

# **TECHNICAL MEMORANDUM**

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TO: Ground-Level Monitoring Committee (GLMC)

Chino Basin Watermaster

FROM: Eric Chiang, PhD

Lauren Salberg

REVIEWED BY: Andy Malone, PG

SUBJECT: Construction and Calibration of One-Dimensional Compaction Models in the Northwest

MZ-1 Area of the Chino Basin (FINAL)

# **BACKGROUND AND OBJECTIVES**

The Chino Basin Watermaster's Subsidence Management Plan (SMP)<sup>1</sup> states that if data from existing monitoring efforts in the Areas of Subsidence Concern indicate the potential for adverse impacts due to subsidence, Watermaster will revise the SMP to avoid those adverse impacts. Watermaster has been monitoring vertical ground motion in Northwest MZ-1 via InSAR since the development of its original SMP (WEI, 2007). Land subsidence in Northwest MZ 1 was first identified as a concern in 2006 in the MZ 1 Summary Report (WEI, 2006). Of particular concern, the subsidence across the San Jose Fault in Northwest MZ 1 has occurred in a pattern of concentrated differential subsidence—the same pattern of differential subsidence that occurred in the Managed Area during the time of ground fissuring. Concerns associated with ground fissuring and differential subsidence include threats to infrastructure and changes to the hydraulic gradient in gravity flow systems.

The issue of differential subsidence, and the potential for ground fissuring in Northwest MZ 1, has been discussed at prior meetings of the Ground Level Monitoring Committee (GLMC), and the subsidence has been documented and described as a concern in Watermaster's State of the Basin Reports, the annual reports of the GLMC, and in the Initial Hydrologic Conceptual Model and Monitoring and Testing Program for the Northwest MZ 1 Area (WEI, 2017). Watermaster increased monitoring efforts in Northwest MZ 1 beginning in Fiscal Year (FY) 2012/13 to include ground elevation surveys and electronic distance measurements (EDM) to monitor ground motion and the potential for fissuring.

In 2015, the Watermaster's Engineer developed the Work Plan to Develop a Subsidence Management Plan for the Northwest MZ-1 Area (Work Plan).<sup>2</sup> The Work Plan is characterized as an ongoing

<sup>1</sup> Wildermuth Environmental, Inc. 2015. Chino Basin Subsidence Management Plan. Prepared for the Chino Basin Watermaster. July 23, 2015.

<sup>&</sup>lt;sup>2</sup> Wildermuth Environmental, Inc. 2015. Work Plan to Develop a Subsidence-Management Plan for Northwest MZ-1. Prepared for the Chino Basin Watermaster. July 23, 2015.

Watermaster effort and includes a description of a multi-year scope of work, a cost estimate, and an implementation schedule. The Work Plan was included in the SMP as Appendix B. Implementation of the Work Plan began in July 2015. On an annual basis, the GLMC analyzes the data and information generated by the implementation of the Work Plan. The results and interpretations generated from the analysis are documented in the annual report of the GLMC and used to prepare recommendations for future activities.

The Work Plan includes various tasks that involve the construction, calibration, and use of one-dimensional aquifer-system compaction models in Northwest MZ-1 (1D Models):

- Tasks 3 and 4 called for the construction and calibration of a single 1D Model at the location of Monte Vista Water District Well 28 (MVWD-28). This 1D Model was used to explore preliminary methods to manage pumping and recharge to avoid the future occurrence of land subsidence in Northwest MZ-1.
- Task 7 called for the construction and calibration of another 1D Model at the location of Pomona Extensometer (PX), which is based on the detailed lithologic information collected at the PX.

The main objective of this technical memorandum is to describe the methods and results for the construction and calibration of both 1D Models. Ancillary objectives are to describe the subsidence mechanisms and the vertical distribution of pre-consolidation head<sup>3</sup> within the aquifer system in Northwest MZ-1.

The knowledge of the subsidence mechanisms and pre-consolidation heads can provide guidance for the Chino Basin parties in the development of "subsidence-management alternatives" (i.e., managed pumping and/or recharge) to avoid the future occurrence of land subsidence in Northwest MZ-1. Subsequent tasks in the Work Plan will utilize the 1D Models described herein to evaluate the effectiveness of the subsidence-management alternatives.

## **METHODS**

This section describes:

- Background information on the modeling tools used to estimate head changes and aquifer system deformation.
- The technical methods that were applied to construct and calibrate the two 1D Models in Northwest MZ-1.

## **Model Codes Used**

The United States Geological Survey (USGS) has developed a wide range of computer models to simulate saturated and unsaturated subsurface flow, solute transport, and chemical reactions in groundwater systems. The most widely used of these models is MODFLOW, which simulates three-dimensional (3D)

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<sup>&</sup>lt;sup>3</sup> The pre-consolidation head is the lowest piezometric level that an aquifer system has ever experienced. When piezometric levels are below the pre-consolidation head, permanent subsidence is caused.

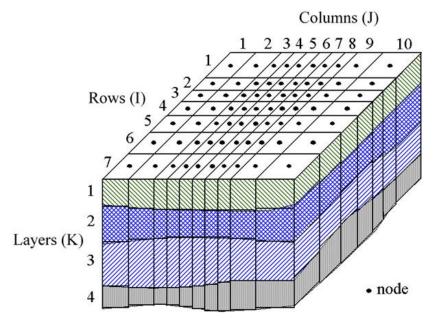
groundwater flow using the finite-difference method. Although it was conceived solely as a groundwater flow model in 1984 and released in 1988 (McDonald et al., 1988), the MODFLOW modular structure has provided a robust framework for the integration of additional simulation capabilities that build on and enhance its original scope. The family of MODFLOW-related models now includes capabilities for simulating coupled groundwater/surface water systems and solute transport.

MODFLOW-NWT (Niswonger et al., 2011) was chosen for this project because: 1) it has extensive publicly available documentation, 2) it has sustained rigorous USGS and academic peer review, 3) it has a long history of development and use, 4) it is widely used around the world in public and private sectors, 5) it can easily operate with additional simulation tools published by others, and 6) it has been used by the Watermaster in the Chino Valley Model (CVM) for the latest Safe Yield Recalculation (WEI, 2020).

The Interbed Storage Package (Leake and others, 1991) of MODFLOW-NWT was chosen to simulate the aquifer-system deformation that is caused by elastic and/or inelastic deformation of the fine-grained interbeds in an aquifer-system due to changes in the effective stress on the soil skeleton because of changing groundwater levels.

## **How MODFLOW Works**

In a MODFLOW model, an aquifer system is represented by a discretized domain consisting of an array of finite difference blocks (model cells) and nodes at the cell centers. The figure below shows the spatial discretization scheme of an aquifer system with a mesh of model cells and nodes at which hydraulic heads are calculated. Hydrostratigraphic units can be represented by one or more model layers and the layer of thickness may vary from cell to cell. The nodal grid forms the framework of a finite-difference numerical model.



To calculate the hydraulic heads at the nodes (i.e., centers of model cells), a water balance equation is

Spatial discretization scheme of MODFLOW

formulated for each model cell:

$$\Sigma Q = S_s \cdot \frac{\Delta h}{\Delta t} \cdot V + S' \cdot \frac{\Delta h}{\Delta t} \tag{1}$$

The left-hand side of the equation ( $\Sigma Q$ ) is the sum of all flows to/from neighboring cells, pumping, and recharge occurring within the model cell. The right-hand side represent the storage change within a time-interval of the length  $\Delta t$ , where Ss is the specific storage (that accounts for compressibility of water), S' is the Skeletal storage coefficient (that accounts for compressibility of soil skeleton) of the model cell, V is the volume of the model cell, and  $\Delta t$  is the head change in the model cell over the time interval  $\Delta t$ . The flows to/from neighboring cells can be expressed with the hydraulic heads of the model cell and its neighbors through the Darcy's law that describes the relationship between the flow, hydraulic conductivity, and hydraulic gradient. In summary, equation (1) can be rewritten to an equation containing unknown hydraulic head values at the cell and its neighboring cells with other aquifer property terms.

MODFLOW formulates such an equation for each of the active model cells (where the heads are unknown and need to be solved). Once all equations are formulated, the system of equations are solved together for the unknown head values. Once the head values are computed, they are used to back-calculate the cell-by-cell flow terms. The calculated head values and flow terms are the basis for water budget calculation, particle tracking simulations, transport models, and visualization, such as flow vectors and water level contours.

# Estimating the vertical aquifer-system deformation in a model cell

The vertical deformation of a model cell ( $\Delta b$ ) over a time interval  $\Delta t$  is calculated as:

$$\Delta \mathbf{b} = \mathbf{S}' \cdot \Delta \mathbf{h} \tag{2}$$

Soil skeleton deformation behavior is non-linear and is dependent on the current hydraulic head and the lowest hydraulic head (i.e., highest effective stress) that has ever been applied to the soil skeleton. To better approximate the non-linear behavior, equation (2) is further refined as follows:

$$\Delta b_e = S_{fe} \cdot \Delta h \qquad if \ h > h_c \tag{3a}$$

$$\Delta b_v = S_{fv} \cdot \Delta h \qquad \text{if } h \le h_c \tag{3b}$$

The variable  $h_c$  is the pre-consolidation head (also referred to as critical head, or the previous lowest hydraulic head) of the model cell;  $\Delta b_e$  is the elastic deformation;  $S_{fe}$  is the elastic storage coefficient;  $\Delta b_v$  is the inelastic deformation; and  $S_{fv}$  is the inelastic storage coefficient. Equation (3a) applies when the hydraulic head is greater than the pre-consolidation head. Equation (3b) applies when the hydraulic head is equal or less than the pre-consolidation head.

If the hydraulic head remains greater than the pre-consolidation head, a further decrease in hydraulic head (i.e., increase in effective stress) causes a small elastic compression in both the coarse- and fine-grained sediments. This compression is recoverable if the head returns to its initial value. If the hydraulic head falls below the pre-consolidation head, the fine-grained sediments can compact inelastically. Inelastic compaction is explained by a physical rearrangement of the sediment grains and is largely permanent (Meade, 1964). Inelastic compaction of coarse-grained sediments is generally negligible compared to that of fine-grained sediments. For the same magnitude of changes in effective stress, inelastic compaction can be one to two orders of magnitude larger than elastic compression (Riley, 1969; Riley 1998).

# **Time Delay of Compaction**

Because of the characteristically low vertical hydraulic conductivity of fine-grained interbeds, the equilibration of hydraulic heads in the interbeds of an aquifer system typically lags the head changes in the bounding aquifers (Hoffmann and others, 2003). In the context of interbed compaction and land subsidence, the time delay caused by slow dissipation of transient overpressures in fine-grained interbed sediments is often given in terms of the time constant  $\tau_0$ .

$$\tau_0 = \left(\frac{b_0}{2}\right)^2 / D' \tag{4}$$

The time constant  $\tau_0$  is the time during which about 93 percent of the ultimate compaction for a given decrease in head occurs (Hoffmann and others, 2003) if the overpressures dissipate vertically in two directions into the bounding aquifers. The variable  $b_0$  is the thickness of the interbed within a model cell and  $D' = S_S'/VK_V'$  is the ratio of the specific storage  $(S_S')$  and the vertical hydraulic conductivity  $(VK_V')$  of the interbed. If the time constant  $\tau_0$  is significantly greater than the model time steps, the process of slow dissipation of the heads in the interbed must be explicitly simulated (Hoffmann and others, 2003). For most regional 3D groundwater models with large interbed thickness within model layers (such as CVM), the time constant  $\tau_0$  is often much greater than the model time steps. The Subsidence and Aquifer Compaction (SUB) Package introduces an approximation method to simulate the slow dissipation of heads in such models, where all interbeds within a model cell (of greater thickness) are lumped together and their root mean square of the thicknesses is used in the simulation. While this method is theoretically sound, it is impractical to accurately collect details of all interbed data for deep aquifers of a 3D model.

To address this challenge, this work used a combination of 3D and 1D models. In this approach, a 3D model is used to simulate regional groundwater head without the skeleton compression (i.e., compaction) terms. A vertical 1D model at a desired location with detailed lithological log is constructed with much higher vertical resolution, where thickness of each model cell is much smaller than the 3D model to obtain a proper time constant  $\tau_0$  for given time step lengths. The simulated heads from the 3D model are then assigned as the prescribed heads for the 1D model cells with coarse-grained sediments, and the 1D model run is executed to calculate the vertical aquifer-system deformation within the model cells of fine-grained sediments. The detailed steps of this approach are given below.

# **Steps to Construct and Calibrate 1D Compaction Models**

In summary, the major steps to construct and calibrate the 1D Models were:

- 1. Construct the 1D Models using the Interbed Storage Package (Leake and others, 1991) of MODFLOW-NWT at areas of maximum historical subsidence. These models are a vertical stack of cells that represent the aquifer system at each location. The thicknesses of the 1D Model cells are chosen to ensure that the time constant  $\tau_0$  is smaller than model time steps. The model cells are categorized into either "Sand" for coarse-grained sediments or "Clay" for fine-grained sediments based on borehole lithologic and geophysical data. Initial aquifer (Sand) and aquitard (Clay) properties were assigned to the 1D Model cells.
- 2. Prepare a time-series of historical heads by aquifer-system layer to serve as input data for the 1D Models over the calibration period. For 1930-1977, these heads are estimated based on the measured groundwater elevations at wells in the vicinity of the 1D Models. For 1977-2018,

these heads are estimated from CVM output data for heads at the 1D Model locations by model layer. The heads are assigned as prescribed heads to the corresponding Sand cells in the 1D Model.

3. Run and calibrate the 1D Models over a historical period by adjusting the aquifer and aquitard properties. The 1D Model simulations were executed to compute a time series of vertical aquifer-system deformation in each 1D Model cell. During calibration, the aquitard properties were adjusted manually to best match historical observations of land subsidence with model-simulated compaction of the aquifer system. The sum of the calculated vertical deformation in all 1D Model cells was assumed to represent the vertical ground motion at the land surface.

# **RESULTS**

This section describes the results and conclusions of the construction and calibration the 1D Models.

## **Location of the 1D Models**

Two 1D Models were constructed and calibrated to simulate the vertical deformation of the aquifer-system sediments at sites in Northwest MZ-1. Figure 1 shows that one model is located at the PX facility and the second model is located at the MVWD-28 well site. Figure 1 also shows the contours of InSAR-estimated vertical ground motion across Northwest MZ-1 used to calibrate the 1D Models and the locations of nearby benchmarks (B-401, B-403, BM 2867, BM 4311, EV3052, EV3054) at which surveyed elevation data are available to validate the 1D Model calibrations.

The PX and MVWD-28 sites were chosen as the 1D Model locations because:

- 1. Both sites are located within the area of greatest subsidence in Northwest MZ-1 as estimated by InSAR from 1992-2021.
- The boreholes were drilled to total depths of 1,290 and 1,317 feet below ground surface (ft-bgs) for PX and MVWD-28, respectively. These depths are deeper than most production wells in the area and penetrate all five model layers as currently conceptualized in the CVM.
- 3. The borehole lithologic descriptions are consistent with the borehole resistivity logs. This is important because the borehole lithology was the primary information used to construct and discretize the 1D Models into "Sand" and "Clay" layers.

# **Data for Calibration and Validation**

Both models were calibrated to match the InSAR estimates of vertical ground motion at the locations of the 1D Models. In addition, ground-level survey data at nearby benchmarks were used to validate the calibration. The table below describes the time range of the available InSAR and ground-level survey data, including data provided by the Los Angeles Department of Public Works (LADPW)<sup>4</sup> and the data acquired by the Chino Basin Watermaster as part of its Ground-Level Monitoring Program.

<sup>&</sup>lt;sup>4</sup> https://dpw.lacounty.gov/sur/BenchMark/

Time Range of Ground-Motion Data Used in 1D Model Calibration and Validation					
Location/Method Time Range					
InSAR at the PX and MVWD-28 locations	1992 to 1999, and 2005 to 2020				
Benchmark 2867 via LADPW leveling surveys	1990 to 2013				
Benchmark 4311 via LADPW leveling surveys	1990 to 2013				
Benchmarks B-401 and B-403 via CBWM leveling surveys	2013 to 2021				

# **Borehole Lithology**

The lithology at PX and MVWD-28 consists of coarse-grained "Sand" layers comprised of silty sands, sands, and gravels, interbedded with fine-grained "Clay" layers comprised of silts, silty clays, and clays. The table below shows the mapping of Unified Soils Classification System (USCS) codes to "Sand" or "Clay" layers.

Mapping of USCS Codes to Sand or Clay Layers				
USCS Code	Cell Type	Description		
SP-SM	Sand	Poorly graded sand with silt		
SP-SC	Sand	Poorly graded sand with clay		
SP	Sand	Poorly graded sand with gravel		
SC	Sand	Clayey sand or Sand with clay		
SM	Sand	Silty sand		
СН	Clay	Fat clay		
ML	Clay	Sandy silt		
CL	Clay	Sandy lean clay or Clay with sand		

# **Spatial Discretization**

Figures 2 and 3 show the generalized borehole lithology at the PX and MVWD-28 sites, short-normal borehole resistivity logs, 1D Model cells (Sand cells are shaded in blue; Clay cells are shaded white), and the corresponding CVM layers. CVM Layer 1 represents the shallow aquifer-system and is generally characterized by unconfined to semi-confined groundwater conditions. CVM Layers 2 to 5 represent the deep aquifer-system and are characterized by confined groundwater conditions, lower permeability sand and gravel layers (compared to Layer 1), and a greater abundance of interbedded fine-grained sediments.

For the PX 1D Model, the borehole lithology was discretized into a stacked column of 529 two-foot-thick cells starting from 234 ft-bgs to 1,292 ft-bgs. The uppermost 234 feet of sediments were not included in

<sup>&</sup>lt;sup>5</sup> The PX2 and MVWD-28 borehole lithologic and geophysical logs are included in Appendix A to this memorandum.

the 1D Model because the sediment was unsaturated throughout the simulation and therefore not subject to deformation caused by changes in head. Each 1D Model cell was mapped to the borehole lithology and identified as either a "Sand" or "Clay" cell based on the mapping shown in the table above.

For the MVWD-28 1D Model, the borehole lithology was discretized into a stacked column of 510 two-foot-thick cells starting from 280 ft-bgs to 1,300 ft-bgs. The uppermost 280 feet of sediments were not included in the 1D Model because the sediment was unsaturated throughout the simulation and therefore not subject to deformation caused by changes in head. Each model cell was mapped to the borehole lithology and identified as either a "Sand" or "Clay" cell based on the mapping shown in the table above.

#### **Time Discretization**

The 1D Models were ran from July 1, 1930 to June 30, 2018 on a monthly time step.

### **Initial Conditions**

The 1D Models require assignment of initial conditions for head, pre-consolidation head, and initial compaction for each model cell. An initial head of 750.5 feet above sea level (ft-amsl) was assigned to all model cells based on measured heads in 1930 at wells located in the vicinity of the 1D Models. The assumption here is that 1930 was a time before significant head declines and compaction of the aquifer-system sediments in Northwest MZ-1. The initial pre-consolidation head was also set at 750.5 ft-amsl. The initial compaction was set to zero for all model cells.

### **Boundary Conditions**

The Sand cells in the 1D Models were modeled as a specified-head boundary with the Flow and Head Boundary Package (Leake and others, 1997). Figures 4 and 5 show the time-series of groundwater elevations by CVM Layer that were used in the 1D Models for the PX and MVWD-28 sites, respectively. Historical measured heads at several wells located in the vicinity of the 1D Models are also shown on Figures 4 and 5.

For the period 1930-1977, the measured heads at nearby wells were used to estimate the time-series of groundwater elevations by CVM Layer. Figure 6 shows that during this period, virtually all pumping wells that existed in Northwest MZ-1 had well screens that penetrated Layer 1 only. Figures 4 and 5 show that during 1930-1977 it was assumed that heads in the deeper CVM Layers equilibrated simultaneously with the head declines that were occurring in Layer 1.

For the period 1977-2018, the CVM-simulated heads at the 1D Model locations were used as the time-series of groundwater elevations by CVM Layer. This period is the calibration period for the 2020 CVM. Figure 6 shows that during this period, deeper pumping wells were constructed in Northwest MZ-1. Figures 4 and 5 show that after about 1977, the deeper pumping caused head declines in the deeper confined CVM Layers, which in turn resulted in downward vertical hydraulic gradients.

### **Initial Aquifer/Aquitard Properties**

Table 1 lists the initial estimates for vertical hydraulic conductivity, specific storage, and the inelastic and elastic storage coefficients that were assigned to all Sand and Clay cells in both 1D Models. These initial estimates were obtained based on literature reviews and were adjusted during calibration.

## **Calibration of the 1D Models**

The calibration of the 1D Models was performed in a manual and iterative manner in the following steps:

- 1. The initial estimates of parameter values for the Sand and Clay cells were assigned to the 1D Models.
- 2. The 1D Models were executed from 1930 to 2018 using the prescribed heads by model layer in Figures 4 and 5 as boundary conditions for the Sand cells in the 1D Models.
- 3. The model-simulated compaction values in the combined Clay cells were compared with the InSAR estimates of vertical ground motion over the period of InSAR records, and the goodness of fit was determined via visual and statistical methods.
- 4. A new set of parameter values for the Clay<sup>6</sup> cells were determined based on the results of step 3, and steps 1 to 3 were repeated for a new calibration iteration.

The iterative calibration process described above was repeated until a good match between model-simulated aquifer-system deformation and the InSAR estimates of vertical ground motion was achieved with parameter values within reasonable bounds. The initial parameter values in Table 1 were used in calibration iteration V1, and then manually adjusted in subsequent calibration iterations.

Table 2 is a list of calibration iterations (V1 to V21) and parameter values for the Clay cells in both 1D Models. Figures 7 and 8 show the time series of the simulated aquifer-system deformation and observed vertical ground motion for all calibration iterations for the PX 1D Model and the MVWD-28 1D Model, respectively. The time-series of vertical ground motion from the benchmark surveys are also displayed on these figures to validate the calibration results. The calibration process was focused on matching model results with the recent InSAR data (i.e., 2005 to 2020), since these are considered the most reliable InSAR data for calibration targets.

For the PX 1D Model, the parameters values for calibration iterations V13 and V21 provided the best match between the simulated and observed values. For the MVWD-28 1D Model, the parameter values for calibration iterations V7 and V21 provided the best match between the simulated and observed values. For both models, V21 matches the InSAR data from 1992 to 1999 better. V21 also results in less total subsidence compared to V7 and V13, which is more consistent with no reported observations of ground fissuring or subsidence-related impacts to overlying infrastructure.

The final calibration results for V21 are displayed in the following figures and tables for both 1D Models:

<sup>&</sup>lt;sup>6</sup> The potential for compaction in the Sand cells was assumed to be negligible, hence, the parameter values for the Sand cells were set to their initial values in Table 1 and were not adjusted during 1D Model calibration.

- Figures 9 and 10 are time series charts that compare simulated versus observed data for calibration iteration V21 for the PX 1D Model and the MVWD-28 1D Model, respectively.
- Figures 11 and 12 are scatter plots that compare simulated versus observed data, which
  quantifies the goodness of fit of the calibration iterations. On these charts, the X-axis represents
  measured ground motion and the Y-axis represents the model-simulated aquifer-system
  deformation. The orange diagonal line represents the line of perfect fit.
- Tables 3 and 4 shows the calibration statistics for all calibration iterations, which indicate that V21 is the best calibration for both 1D Models.

Figures 9 and 10 also display the ground-level survey data from 1990-2020 that validate the model calibration for V21. There are no ground-level survey data near the PX and MVWD-28 sites prior to the 1990s that can be used to validate V21. However, Figure 1 shows that 3.5 feet of subsidence occurred at benchmark EV3052 from 1923-1974 and 1.64 feet of subsidence occurred at benchmark EV3054 from 1968-1978. These early ground-level survey data are consistent with the timing and magnitude of the compaction that was estimated by the 1D Models prior to the 1990s.

In conclusion, the 1D Model parameters of V21 resulted in the best fit between simulated compaction and the observed subsidence data. The final calibrated parameters for both 1D Models are listed below:

Final Calibrated Parameter Values for the Clay Cells in the PX and MVWD-28 1D Models						
Iteration	VK [ft/day]	Ss [1/ft]	Sfv [-]	Sfe [-]		
V21	2.00E-07	1.14E-05	4.50E-04	4.50E-06		

# **Simulation of Historical Subsidence**

Figure 7 shows that the final calibration run (V21) for the PX 1D Model resulted in a total of about 9.6 feet of aquifer-system compaction from 1930 to 2018. Most of the compaction (about 6.4 feet) occurred between 1930 and 1978—the period of gradual and persistent lowering of groundwater levels by about 190 feet in Northwest MZ-1.

Figure 8 shows that the final calibration run (V21) for the MVWD-28 1D Model resulted in a total of about 5.5 feet of aquifer-system compaction from 1930 to 2018. About three feet of compaction occurred between 1930 and 1978—the period of gradual and persistent lowering of groundwater levels by about 190 feet in Northwest MZ-1.

The final calibration run (V21) also generated end-of-calibration (2018) estimates of the compaction and critical head in the 1D Model cells, which are displayed on Figures 13 and 14 for the PX and MVWD-28 1D Models, respectively. The higher critical head and lower compaction in the center of thicker fine-grained sediment layers indicate that the pore pressures there have not yet dissipated and, therefore, these sediment layers are susceptible to compaction should the internal pore pressures continue to decline in the future. As thicker fine-grained layers are primarily located in the deep aquifer-system, this indicates that the potential for future compaction is more likely to occur in the deep aquifer system (Layers 2, 3, 4, and 5) compared to the shallow aquifer-system (Layer 1).

# **Sensitivity Analysis**

In early 2022, the GLMC reviewed the calibration results of the 1D Models described above and recommended an analysis to evaluate the sensitivity of the 1D Model calibrations to the estimates of historical heads. This sensitivity analysis is prudent given the lack of historical data, and hence, uncertainty in knowledge of depth-specific historical heads (i.e., the time series of historical heads in each model layer).

The sensitivity analysis was performed using the following methods:

- 1. Adjust the time series of historical heads shown in Figures 4 and 5 to prepare six additional calibration runs—three for the PX 1D Model and three for the MVWD-28 1D Model:
  - i. Calibration Run V22 for the PX 1D Model. Figure 15 displays a time series of historical heads at the PX site where declines in heads in Layer 5 lag behind the declines in heads in Layers 1 and 3 over the period of 1930-1977. This time series is plausible since there are no records of pumping wells in Northwest MZ-1 with well screens that penetrate Layer 5 during 1930-1973 (see Figure 6).
  - ii. Calibration Run V23 for the PX 1D Model. Figure 16 displays a time series of historical heads at the PX site where: (i) heads in Layer 1 were adjusted upward from 1978-2018 to better match recent heads measured at the PX1-1 piezometer (Layer 1) in 2020 and (ii) heads in Layer 5 were adjusted downward from 1978-2018 to better match recent heads measured at the PX2-3 piezometer (Layer 5) in 2020.
  - iii. **Calibration Run V24 for the PX 1D Model**. Figure 17 displays a time series of historical heads at the PX site where heads were adjusted as described in V22 and V23.
  - iv. Calibration Run V22 for the MVWD-28 1D Model. Figure 18 displays a time series of historical heads at the MVWD-28 site where declines in heads in Layer 5 lag behind the declines in heads in Layers 1 and 3 over the period of 1930-1977. This time series is plausible since there are no records of pumping wells in Northwest MZ-1 with well screens that penetrate Layer 5 during 1930-1973.
  - v. Calibration Run V23 for the MVWD-28 1D Model. Figure 19 displays a time series of historical heads at the MVWD-28 site where: (i) heads in Layer 1 were adjusted upward from 1978-2018 to better match recent heads measured at the PX1-1 piezometer (Layer 1) in 2020 and (ii) heads in Layer 5 were adjusted downward from 1978-2018 to better match recent heads measured at the PX2-3 piezometer (Layer 5) in 2020.
  - vi. **Calibration Run V24 for the MVWD-28 1D Model**. Figure 20 displays a time series of historical heads at the MVWD-28 site where heads were adjusted as described in v22 and V23.
- 2. The 1D Models were executed from 1930 to 2018 using the prescribed heads by model layer in V22, V23, and V24 as boundary conditions for the Sand cells in the 1D Models.
- 3. The model-simulated compaction values in the combined Clay cells were compared with the InSAR estimates of vertical ground motion over the period of InSAR records, and the goodness of fit was determined:

- Figures 21, 22, and 23 are time series charts that compare simulated versus observed data for calibration iterations V22, V23, and V24 for the PX 1D Model.
- Figures 24, 25, and 26 are time series charts that compare simulated versus observed data for calibration iterations V22, V23, and V24 for the MWWD-28 1D Model.
- Tables 3 and 4 shows the calibration statistics for calibration iterations V22, V23, and V24 for PX 1D Model and the MWWD-28 1D Model, respectively.

The main observations and conclusions from the sensitivity analysis are:

- The adjustment in historical heads in the sensitivity analysis did not significantly affect the simulated compaction in the 1D Models. This observation indicates that the 1D Models are not sensitive to minor differences in the assumptions for historical heads. More likely, the 1D Models are most sensitive to the number and thicknesses of the Clay layers and the long-term declining trends in historical heads that drive the delayed drainage and compaction of the Clay layers.
- The 1D Model calibrations with V24 were virtually identical to V21 with no changes to the parameter values for the Clay cells as determined in V21.
- V24 also resulted in less total compaction compared to V21 in both 1D Models, which is more
  consistent with no reported observations of ground fissuring or subsidence related impacts to
  overlying infrastructure. Therefore, V24 replaces V21 as the final calibration iteration, but with
  no changes to the model parameters determined in V21.
- The 1D Models are well calibrated and capable of accurately estimating future aquifer-system compaction under various plans for pumping and recharge. Therefore, the GLMC should proceed with the use of the 1D Models to develop subsidence management strategies for Northwest MZ-1, if necessary.

## **MODEL ERRORS AND LIMITATIONS**

In general, a groundwater model is a simplified mathematical representation of a complex hydrogeologic system. Because of this, there are limits to the accuracy of the model and the use and interpretation of the model results. There are various sources of error and uncertainty. Model error commonly stems from the conceptual model, practical limitations of grid cell size and time discretization, parameter structure, insufficient calibration data, and the effects of processes not simulated by the model. These factors, along with error in observations, result in uncertainty in model results.

The potential errors and limitations associated with the 1D Models and their calibration include:

- The 1D Models were based on the limited resolution, depth, and accuracy of the description of the aquifer-system sediments as documented on the driller's logs of PX and MVWD-28 boreholes.
- The resolution by depth interval of the lithologic descriptions in this log are typically greater than five feet, which may not be a fine enough resolution to characterize any thinner

- interbedding of aquifer and aquitard layers that are an important control on aquifer-system deformation.
- The boreholes did not penetrate the full thickness of the semi-consolidated bedrock formations; there may be deforming sediments at depths below the borehole bottom that are responsible for some of the vertical ground motion estimated by InSAR.
- Most wells in Northwest MZ-1 have well screens that only penetrate the shallow aquifer-system or penetrate both the shallow and deep aquifer-systems. There are no wells in Northwest MZ-1 that existed during the calibration period that are screened only across the deep aquifer-system, meaning that there are no historical measured water-level data for only the deep aquifer-system. As such, there is some uncertainty in the long-term time-series of heads for Layers 2 and 3 that were used as the boundary conditions for the 1D Model calibration, which adds uncertainty to the model results.
- Water-level data at wells is scarce in Northwest MZ-1 prior to the 1930s. This 1D modeling effort
  assumes that the significant lowering of heads in Northwest MZ-1 began after 1930, which may
  not be an accurate assumption. If head declines began before 1930, then this could impact the
  calibration of the 1D models and add uncertainty to the model results.
- The 1D models used InSAR-derived estimates of vertical ground motion as calibration targets for aquifer-system compaction. The limitations of using InSAR-derived estimates as calibration targets are: (1) the InSAR record begins in 1992, which limits the length of the calibration period; (2) there are multiple data gaps in the InSAR record because of satellite malfunctions and satellite replacement; and (3) InSAR produces an aggregate estimate of aquifer-system deformation and therefore provides no depth-specific calibration targets. Due to the lack of depth-specific calibration there is greater uncertainty in the depth-specific estimates for the aquifer and aquitard properties, and hence, the model results.

Continued monitoring and enhanced understanding of hydrogeologic conditions is crucial to minimizing model error and uncertainty, especially the monitoring of the PX in Northwest MZ-1. Future monitoring and data analysis can identify local anomalies associated with geologic complexity that are not currently represented in the model. Model error and uncertainty can be reduced by incorporating new monitoring information into future model updates, if recommended by the GLMC.

### **NEXT STEPS**

Members of the GLMC were asked to review a draft of this technical memorandum and provide comments and suggestions to Andy Malone (<a href="mailto:amalone@westyost.com">amalone@westyost.com</a>) and Edgar Tellez-Foster (<a href="mailto:etellezfoster@cbwm.org">etellezfoster@cbwm.org</a>) by October 21, 2022. Specifically, Watermaster staff and Engineer asked that the GLMC members answer the following question in their comments: Are the 1D Models as described in this technical memorandum sufficiently calibrated to estimate the potential for future subsidence under the Baseline Management Alternative (BMA)? The BMA is a planning scenario that represents the Parties' current plans for pumping and recharge in the Chino Basin.

The comments received from the GLMC, along with the Watermaster Engineer's response to comments, are documented in Appendix B. The majority of GLMC members concurred that the 1D Models are sufficiently calibrated to be used to estimate the potential for future subsidence.

The next steps are as follows:

- 1. The 1D Models are intended to be used to characterize the mechanical response of the aquifer-system to the BMA. A draft technical memorandum will be prepared that summarizes the evaluation of the BMA, particularly, the ability of the BMA to manage piezometric levels in Northwest MZ-1 so that future subsidence is minimized or abated. The draft technical memorandum may also include a recommendation for the Initial Subsidence Management Alternative (ISMA) if the BMA is not successful at managing future subsidence. The assumptions of the ISMA, including the groundwater production and replenishment plans of the Chino Basin parties, will be described in the technical memorandum, and must be reviewed by the GLMC. A GLMC meeting will be held to review the technical memorandum and the recommended ISMA.
- 2. After the recommended ISMA is reviewed by the GLMC, the Watermaster's MODFLOW model will be updated to run the ISMA and will be used to estimate the hydraulic head response to the ISMA at the MVWD-28 and PX locations. The projected hydraulic heads generated from the MODFLOW model using the ISMA will be extracted from the MODFLOW model results at the MVWD-28 and PX locations and will be used as input files for both 1D Models. The 1D Models will then be run to characterize the mechanical response of the aquifer-system to the ISMA at both the MVWD-28 and PX locations to evaluate the effectiveness of the ISMA at managing future subsidence.
- 3. A draft technical memorandum will be prepared that summarizes the evaluation of the ISMA, particularly, the ability of the ISMA to manage hydraulic heads in Northwest MZ-1 so that future subsidence is minimized or abated. The draft technical memorandum may also include a recommendation for a second Subsidence-Management Alternative (SMA-2), if the ISMA is not successful at managing future subsidence. The assumptions of the SMA-2, including the groundwater production and replenishment plans of the Chino Basin parties, will be described, and must be reviewed by the GLMC. A GLMC meeting will be held to review the technical memorandum and the recommended SMA-2.
- 4. If necessary and recommended by the GLMC, additional subsidence management alternative scenarios may be run in FY 2022/23. It is currently envisioned that, based on the results of the 1D Model results, the GLMC may recommend an update to the Watermaster's Subsidence Management Plan in FY 2023/24 to minimize or abate the future occurrence of land subsidence in Northwest MZ-1.

## **REFERENCES**

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- Wildermuth Environmental Inc. (2020). 2020 Safe Yield Recalculation Final Report. Prepared for Chino Basin Watermaster.

Table 1. Initial Estimates of Model Parameters					
Cell Type	Cell Type Model Parameter				
Sand	Vertical hydraulic conductivity VK	5.00E-01 [ft/day]			
Sand	Specific storage Ss	1.83E-06 [1/ft]			
Sand	Inelastic storage coefficient Sfv	1.00E-06 [-]			
Sand Elastic storage coefficient Sfe		1.00E-06 [-]			
Clay	Vertical hydraulic conductivity VK	2.50E-05 [ft/day]			
Clay	Specific storage Ss	1.14E-05 [1/ft]			
Clay	Inelastic storage coefficient Sfv	1.65E-04[-]			
Clay Elastic storage coefficient Sfe 4.50E-06 [-]					



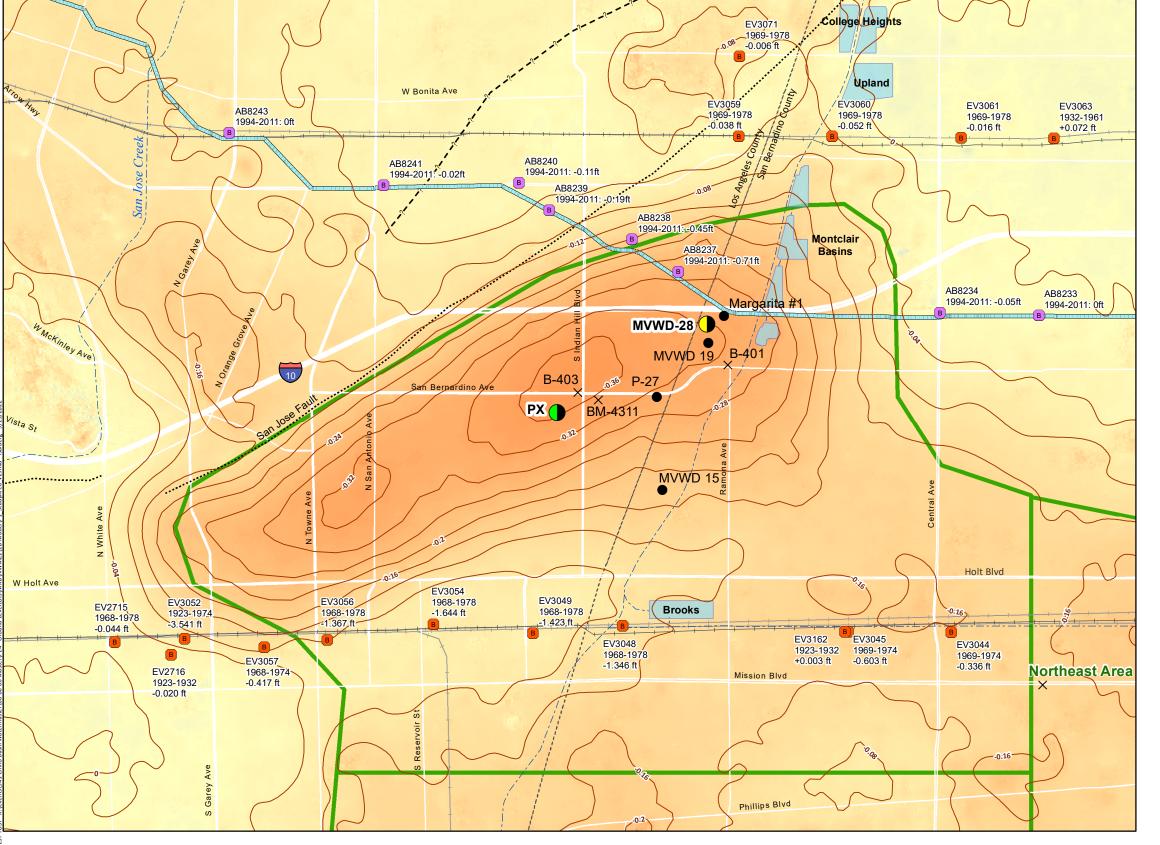
Та	Table 2. Parameter Values for Clay Cells by Calibration Iteration						
Iteration	VK [ft/day]	Ss [1/ft]	Sfv [-]	Sfe [-]			
V1	2.00E-05	1.14E-05	1.65E-04	4.50E-06			
V2	1.00E-05	1.14E-05	1.65E-04	4.50E-06			
V3	1.00E-06	1.14E-05	1.65E-04	4.50E-06			
V3a	1.00E-06	5.00E-06	1.65E-04	4.50E-06			
V3b	1.00E-06	7.00E-06	1.65E-04	4.50E-06			
V4	2.00E-05	1.14E-05	1.00E-04	4.50E-06			
V5	2.00E-05	1.14E-05	2.00E-04	4.50E-06			
V6	1.00E-06	1.14E-05	2.00E-04	4.50E-06			
V7	1.00E-06	1.14E-05	3.00E-04	8.00E-06			
V8	1.00E-06	1.14E-05	5.00E-04	8.00E-06			
V9	1.00E-06	1.14E-05	4.50E-04	4.50E-06			
V10	5.00E-06	1.14E-05	4.50E-04	8.00E-06			
V11	5.00E-06	5.00E-05	4.50E-04	8.00E-06			
V12	2.00E-06	1.14E-05	4.50E-04	4.50E-06			
V13	1.00E-06	1.14E-05	4.00E-04	4.50E-06			
V14	1.00E-06	7.00E-06	4.00E-04	4.50E-06			
V15	6.00E-07	1.14E-05	4.50E-04	4.50E-06			
V16	8.00E-07	1.14E-05	4.50E-04	4.50E-06			
V17	1.00E-06	1.14E-05	3.50E-04	8.00E-06			
V18	1.00E-06	1.14E-05	4.00E-04	2.00E-06			
V19	4.00E-05	1.14E-05	1.00E-04	4.50E-06			
V20	1.00E-06	1.14E-05	3.50E-04	4.50E-06			
V21	2.00E-07	1.14E-05	4.50E-04	4.50E-06			

Table 3. Calibration Statistics for the PX 1D Model

Iteration	Total Subsidence (ft)	Mean of Differences (Observed - Modeled) (ft)	Standard Deviation (ft)	Root Mean Square Deviation (ft)	$R^2$	NSE
V1	9.99	0.29	0.35	0.45	0.91	0.47
V2	9.39	0.32	0.35	0.47	0.94	0.45
V3	6.56	0.37	0.31	0.48	0.96	0.27
V4	6.65	0.37	0.31	0.48	0.93	0.28
V5	6.62	0.37	0.31	0.48	0.97	0.28
V3a	6.19	0.29	0.30	0.41	0.86	0.09
V3b	11.97	0.29	0.38	0.48	0.91	0.57
V6	7.69	0.38	0.33	0.50	0.97	0.37
V7	10.69	0.40	0.39	0.56	0.97	0.55
V8	16.04	0.46	0.52	0.70	0.96	0.67
V9	14.78	0.45	0.49	0.66	0.97	0.65
V10	20.39	0.41	0.59	0.72	0.96	0.71
V11	19.83	0.42	0.58	0.71	0.96	0.71
V12	17.13	0.43	0.53	0.68	0.96	0.68
V13	13.47	0.43	0.46	0.63	0.97	0.62
V14	13.54	0.43	0.46	0.63	0.97	0.63
V15	13.08	0.46	0.47	0.66	0.97	0.62
V16	14.04	0.46	0.48	0.66	0.97	0.64
V17	12.11	0.41	0.42	0.59	0.97	0.60
V18	13.48	0.43	0.46	0.63	0.97	0.62
V19	6.34	0.28	0.30	0.41	0.67	-0.08
V21	9.64	0.03	0.08	0.09	0.99	0.98
V22	9.54	0.03	0.08	0.09	0.99	0.98
V23	9.57	0.05	0.09	0.10	0.99	0.97
V24	9.46	0.04	0.09	0.10	0.99	0.97

Table 4. Calibration Statistics for the MVWD-28 1D Model

Iteration	Total Subsidence (ft)	Mean of Differences (Observed - Modeled) (ft)	Standard Deviation (ft)	Root Mean Square Deviation (ft)	$R^2$	NSE
V1	6.60	0.23	0.22	0.31	0.83	0.46
V2	6.41	0.21	0.20	0.30	0.85	0.49
V3	4.94	0.12	0.13	0.18	0.96	0.82
V4	4.03	0.27	0.23	0.36	0.72	-0.03
V5	7.96	0.20	0.21	0.29	0.87	0.62
V3a	5.02	0.12	0.13	0.18	0.95	0.82
V3b	4.99	0.12	0.13	0.18	0.95	0.82
V6	5.75	0.07	0.11	0.13	0.97	0.92
V7	7.78	-0.05	0.05	0.07	0.99	0.98
V8	11.09	-0.25	0.11	0.27	0.99	0.85
V9	10.33	-0.21	0.09	0.22	0.99	0.89
V10	15.34	-0.20	0.09	0.21	0.99	0.93
V11	14.98	-0.21	0.09	0.23	0.99	0.92
V12	12.75	-0.25	0.10	0.27	0.99	0.88
V13	9.53	-0.16	0.06	0.17	0.99	0.93
V14	9.60	-0.16	0.06	0.17	0.99	0.93
V15	8.59	-0.14	0.06	0.15	0.99	0.93
V16	9.56	-0.18	0.08	0.20	0.99	0.91
V17	8.68	-0.10	0.05	0.11	0.99	0.97
V18	9.54	-0.16	0.06	0.17	0.99	0.93
V19	4.09	0.28	0.24	0.36	0.72	-0.01
V21	5.53	0.00	0.05	0.05	0.99	0.99
V22	5.41	-0.01	0.05	0.05	0.99	0.99
V23	5.59	-0.01	0.05	0.05	0.99	0.99
V24	5.48	-0.02	0.05	0.05	0.99	0.99





PΧ

MVWD-28



# **Land Subsidence Features**

+0.55 ft 0 ft

Relative Change in Land Surface Elevation as Estimated by InSAR (March 2011 to March 2022)

-0.55 ft

- Contours of Relative Change in Land Surface Elevation as Estimated by InSAR (March 2011 to March 2022)
- Benchmark used for 1D Model Calibration
- NGS Benchmarks
- MWD Benchmarks

### Other Features

- Well with Historical Measured Heads
- Recharge Basin
- Northwest MZ-1 Area of Subsidence Concern
- Fault (dotted where concealed; queried where uncertain)
- MWD Upper Feeder
- Railroads

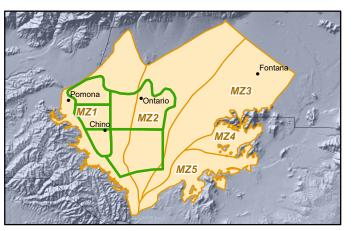


Figure 1

Locations of PX and MVWD-28 1D Models and **Historical Elevation Surveys at Benchmarks** 

**Chino Basin Watermaster** 

**Ground-Level Monitoring Committee** 1D Compaction Models in the Northwest MZ-1 Area





Figure 2. PX Site: CVM Layers, Borehole Lithology, 1D Model Cells, and Resistivity Log

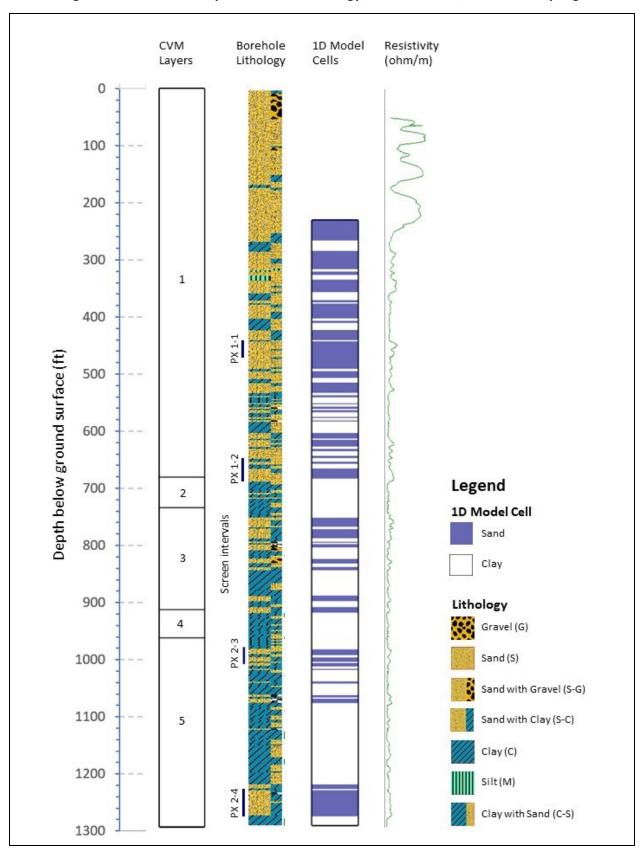


Figure 3. MVWD-28 Site: CVM Layers, Borehole Lithology, 1D Model Cells, and Resistivity Log

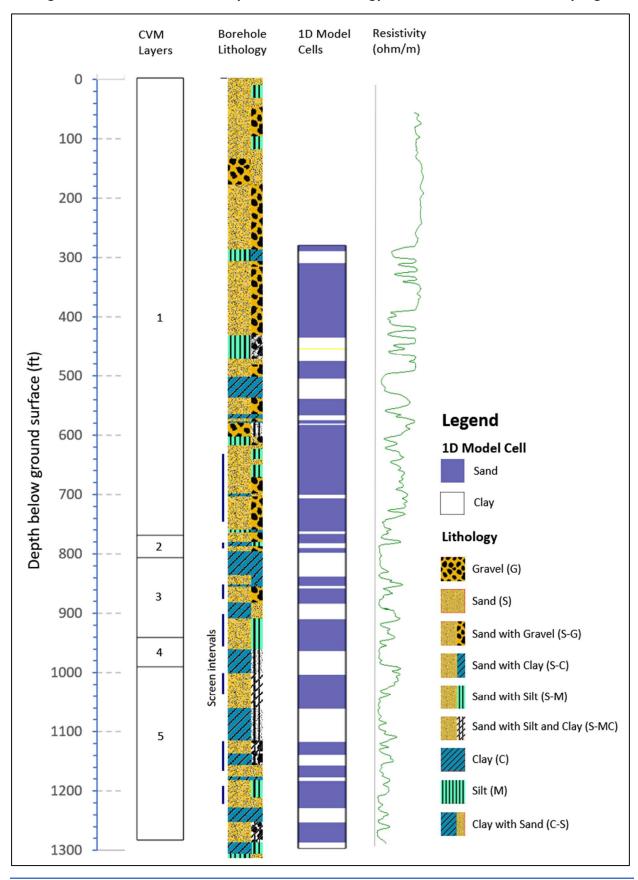


Figure 4. Measured Heads vs. Heads Used in Calibration of PX 1D Model - Calibration Run V21

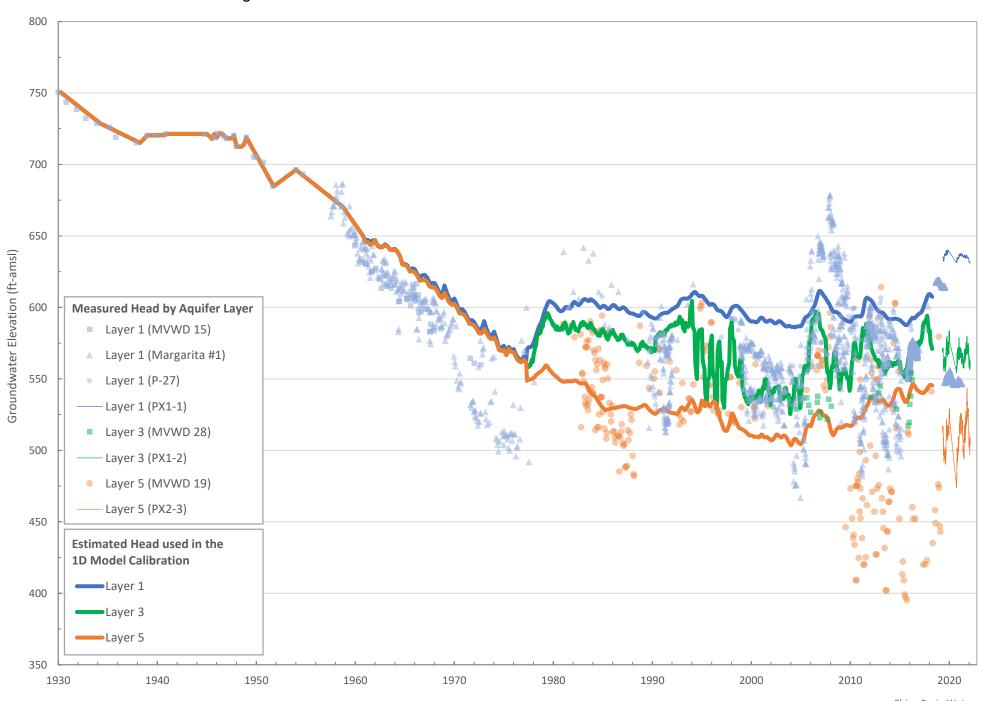
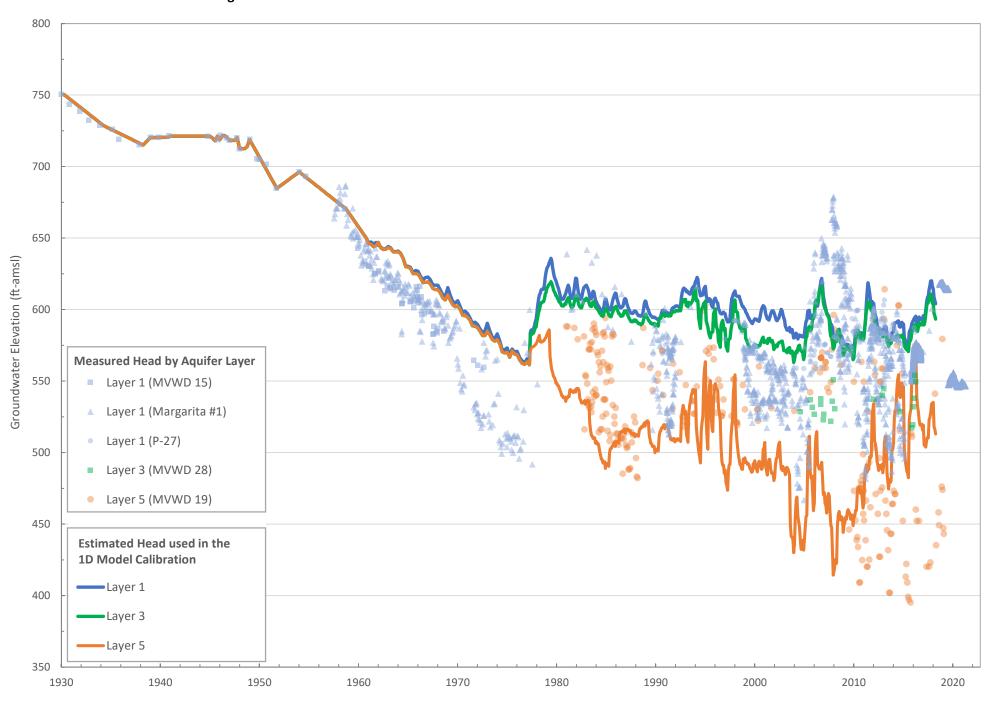
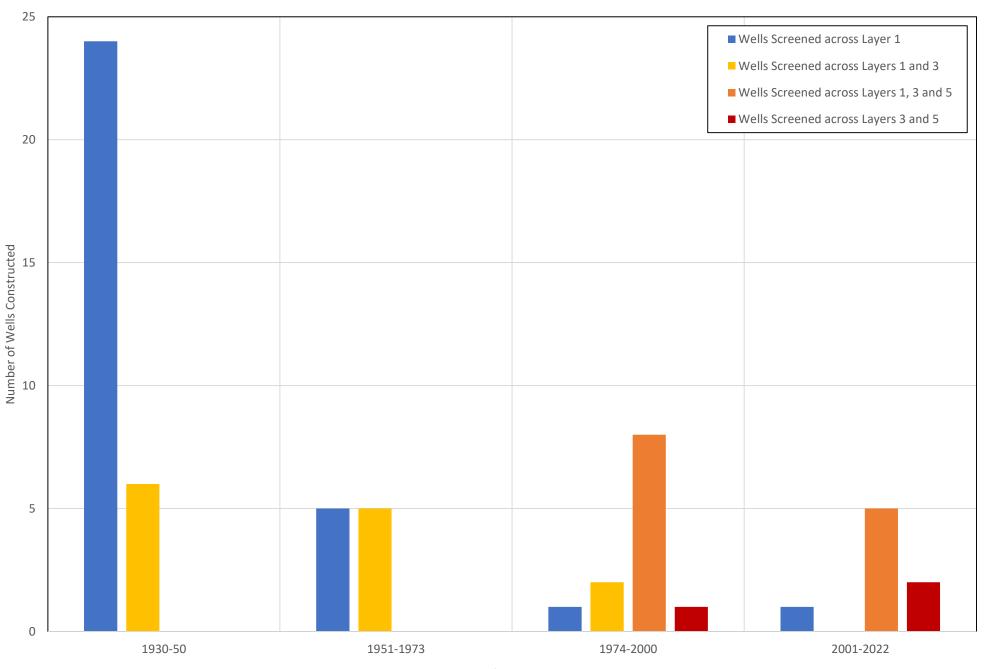


Figure 5. Measured Heads vs. Heads Used in Calibration of MVWD-28 1D Model - Calibration Run V21



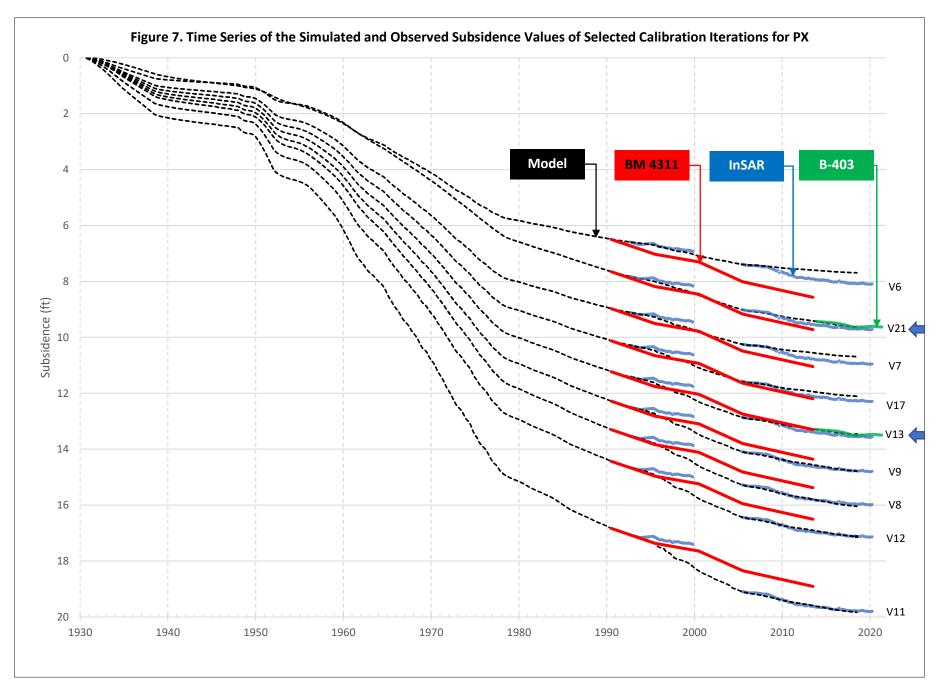
**WEST YOST** 

Figure 6. Wells Constructed in Northwest MZ-1 Over Time by Model Layer



**WEST YOST** 

Time Period of Well Construction



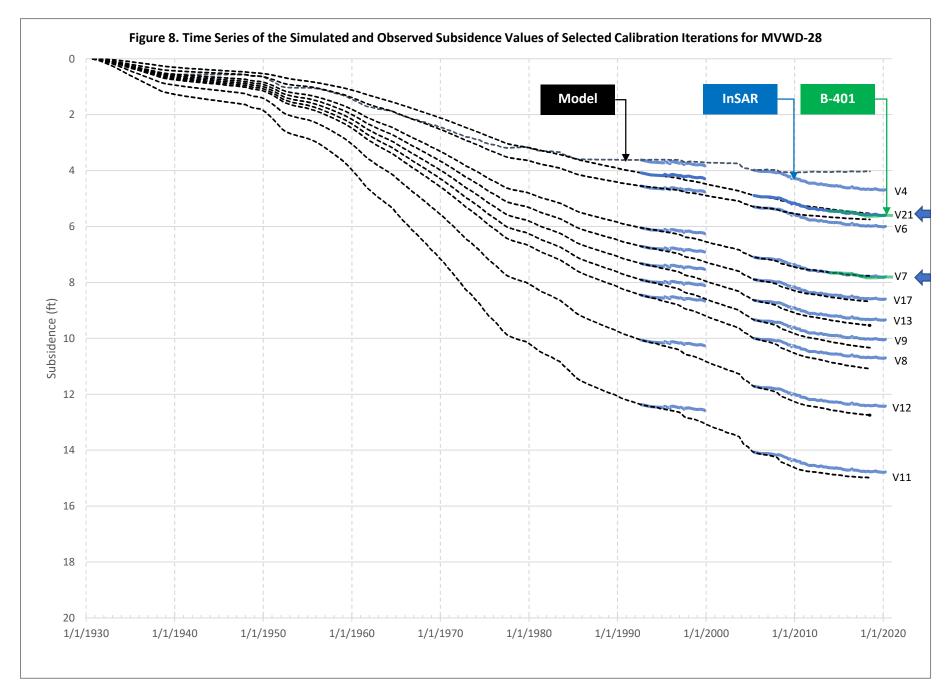


Figure 9. Measured Subsidence vs. Compaction Simulated by PX 1D Model - Calibration Run V21

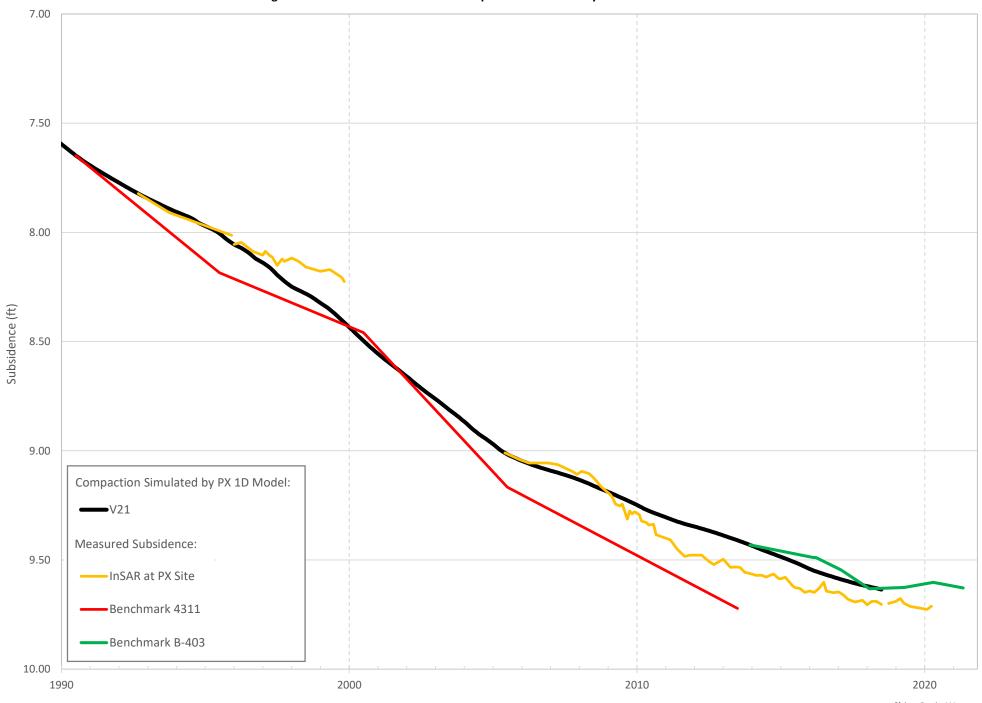


Figure 10. Measured Subsidence vs. Compaction Simulated by MVWD-28 1D Model - Calibration Run V21

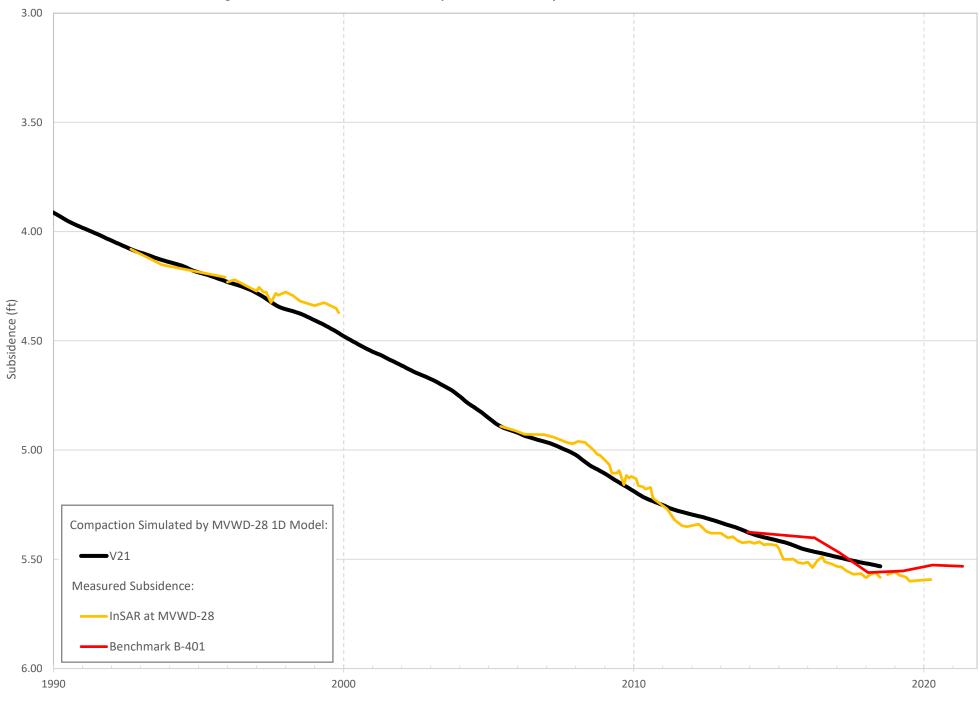


Figure 11. Scatter Plot of the Simulated and Observed Subsidence Values of Calibration Iteration V21 for PX

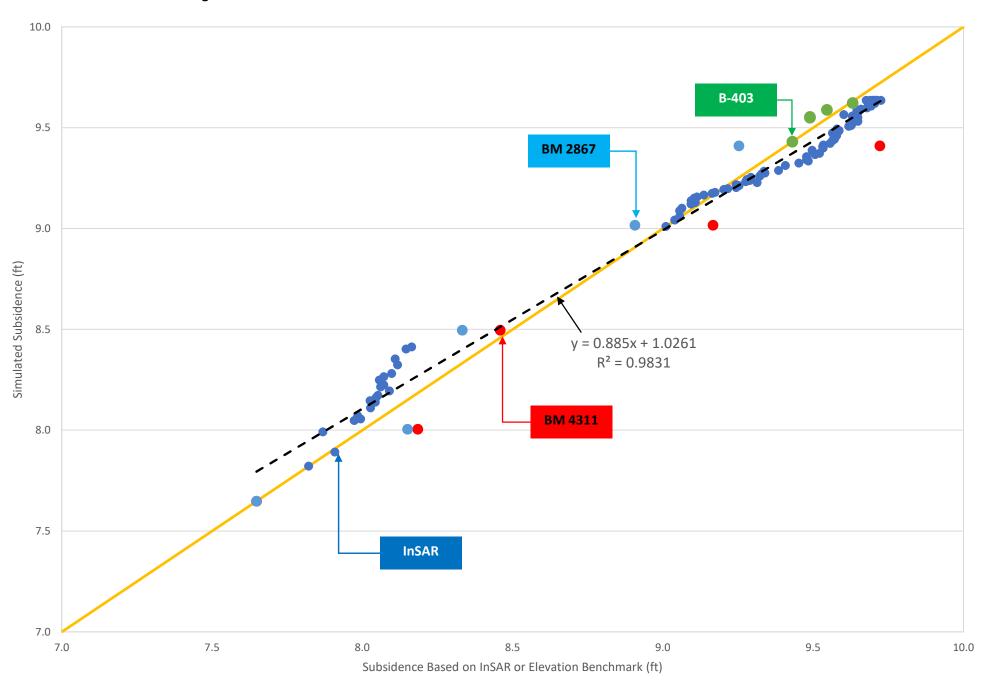


Figure 12. Scatter Plot of the Simulated and Observed Subsidence Values of Calibration Iteration V21 for MVWD-28

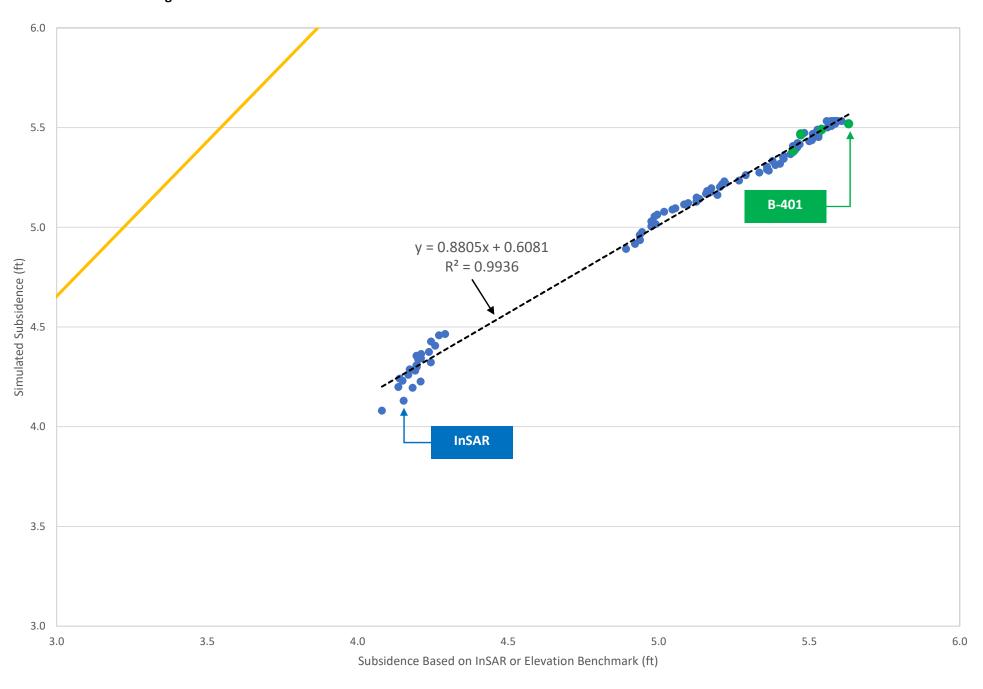


Figure 13. Simulated Compaction and Critical Head on 6/30/2018 for PX

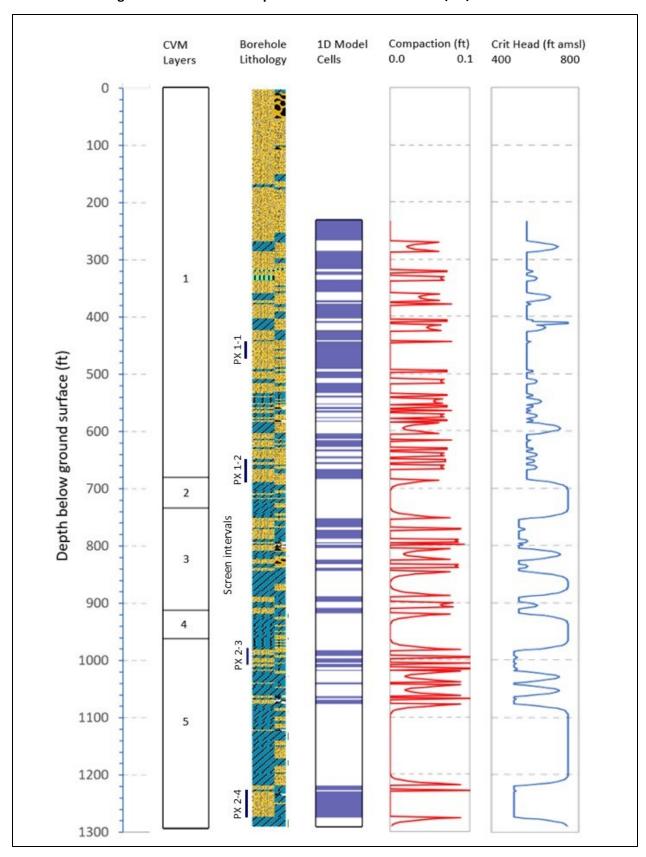


Figure 14. Simulated Compaction and Critical Head on 6/30/2018 for MVWD-28

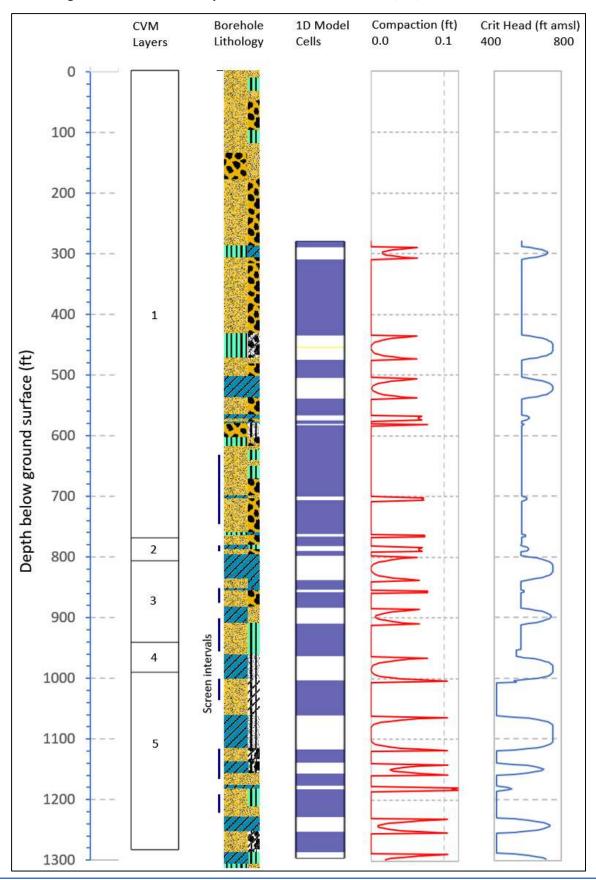


Figure 15. Measured Heads vs. Heads Used in Calibration of PX 1D Model - Calibration Run V22

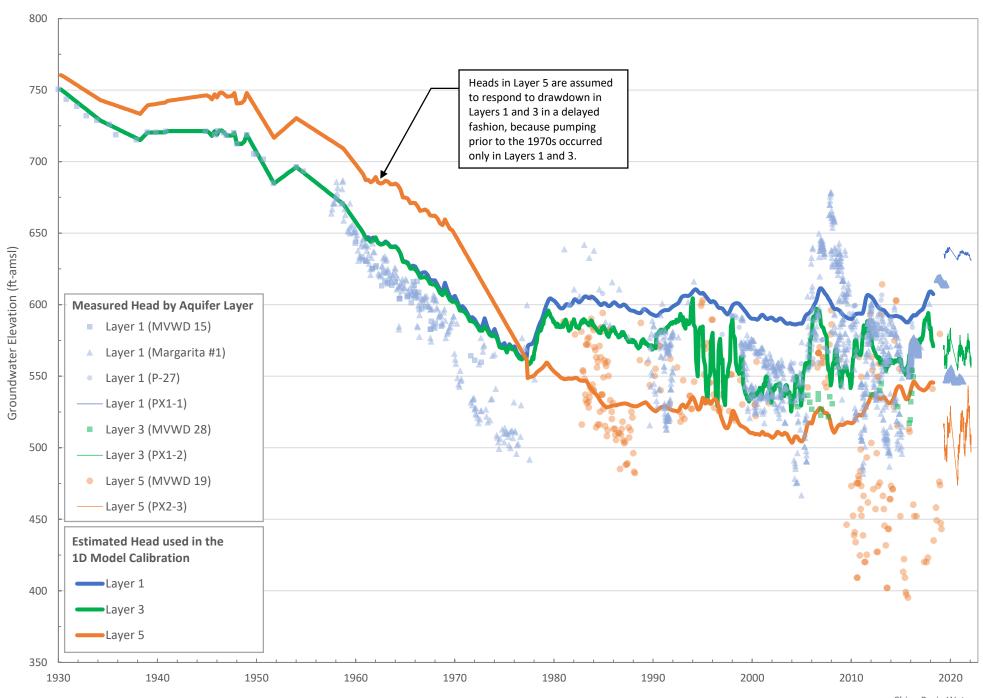


Figure 16. Measured Heads vs. Heads Used in Calibration of PX 1D Model - Calibration Run V23

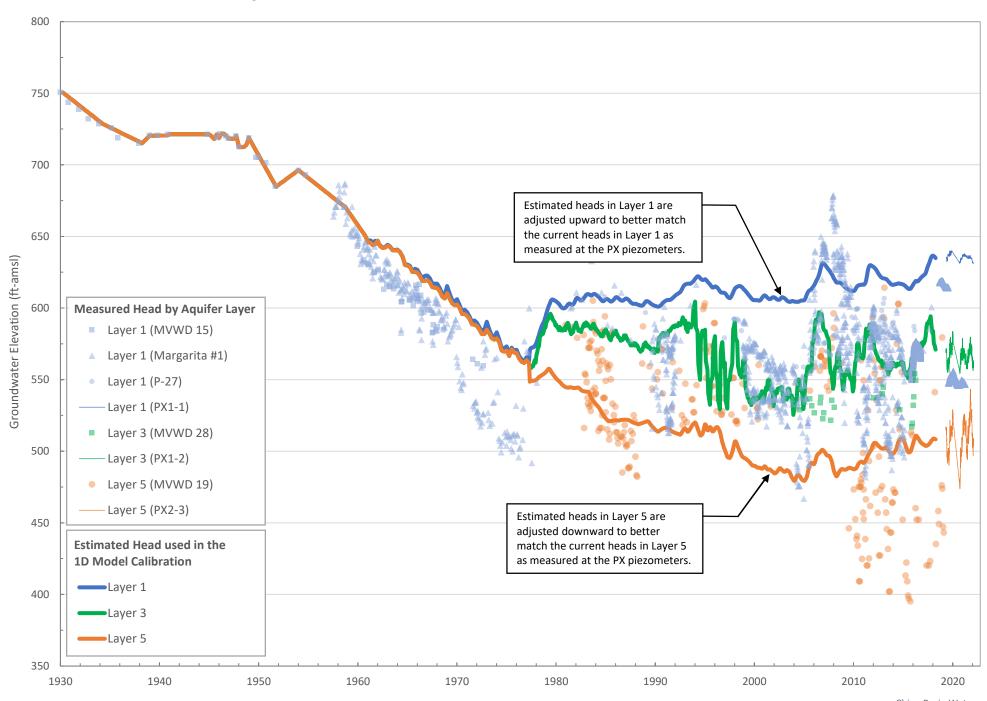


Figure 17. Measured Heads vs. Heads Used in Calibration of PX 1D Model - Calibration Run V24

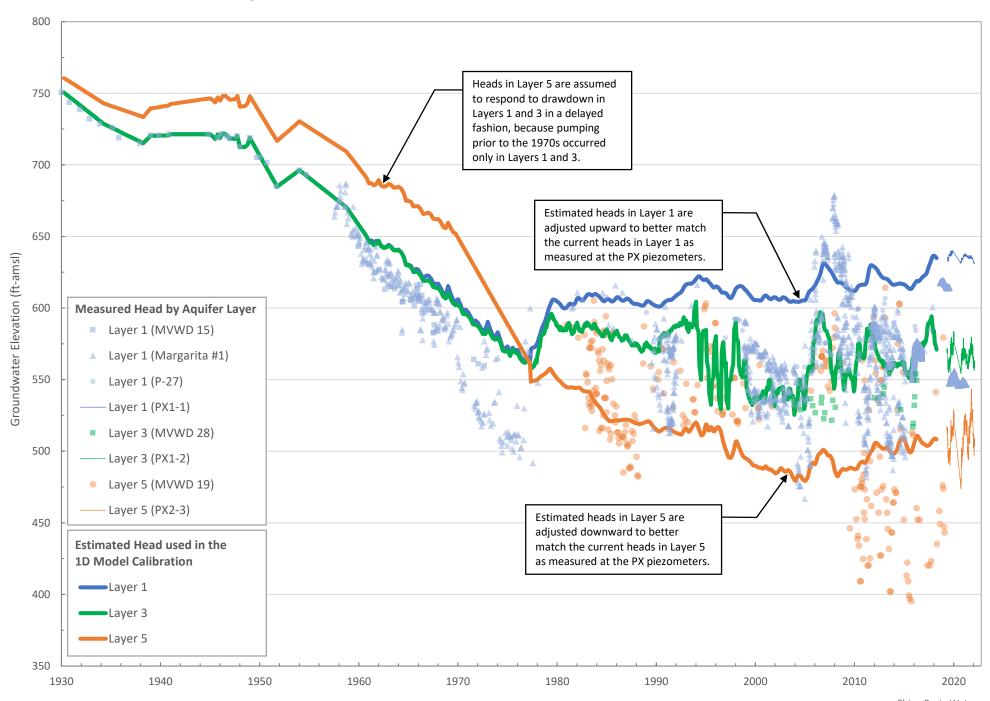
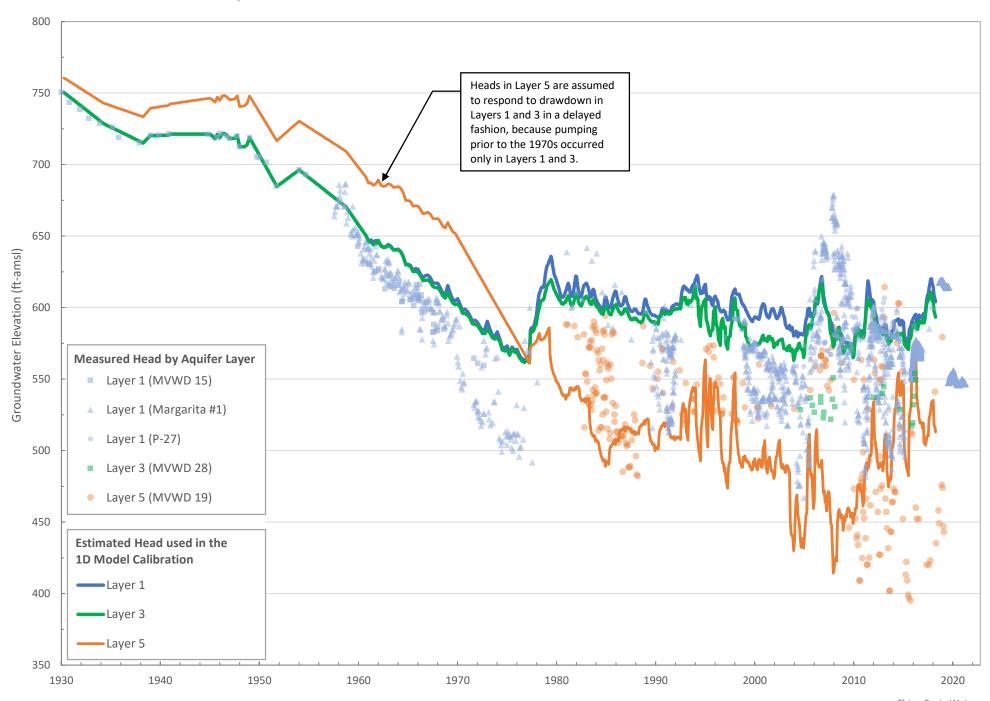


Figure 18. Measured Heads vs. Heads Used in Calibration of MVWD-28 1D Model - Calibration Run V22

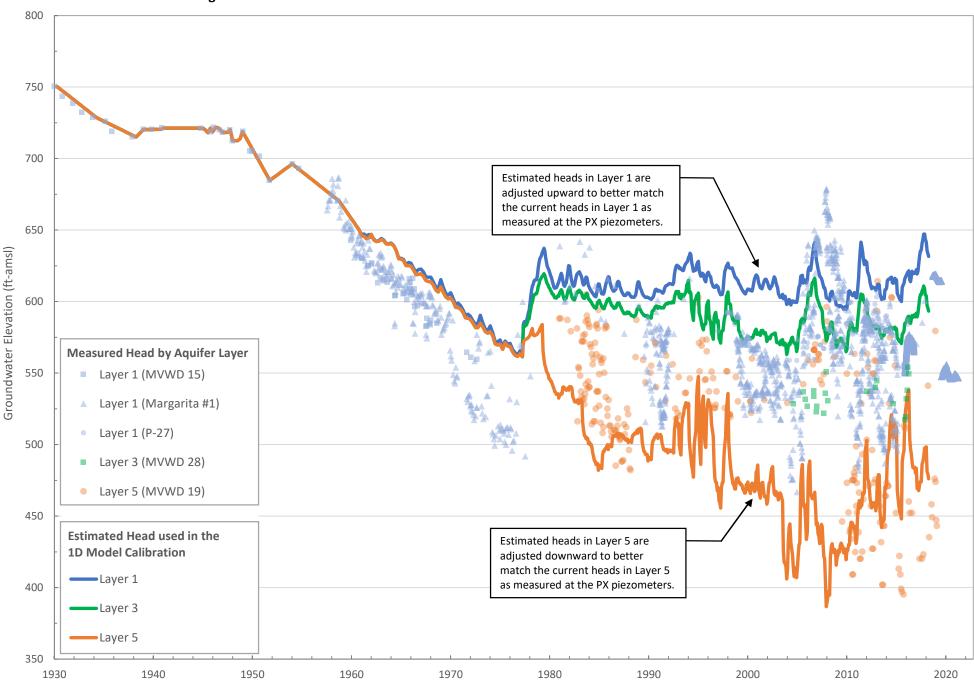


Chino Basin Watermaster

1D Compaction Models in the Northwest MZ-1 Area

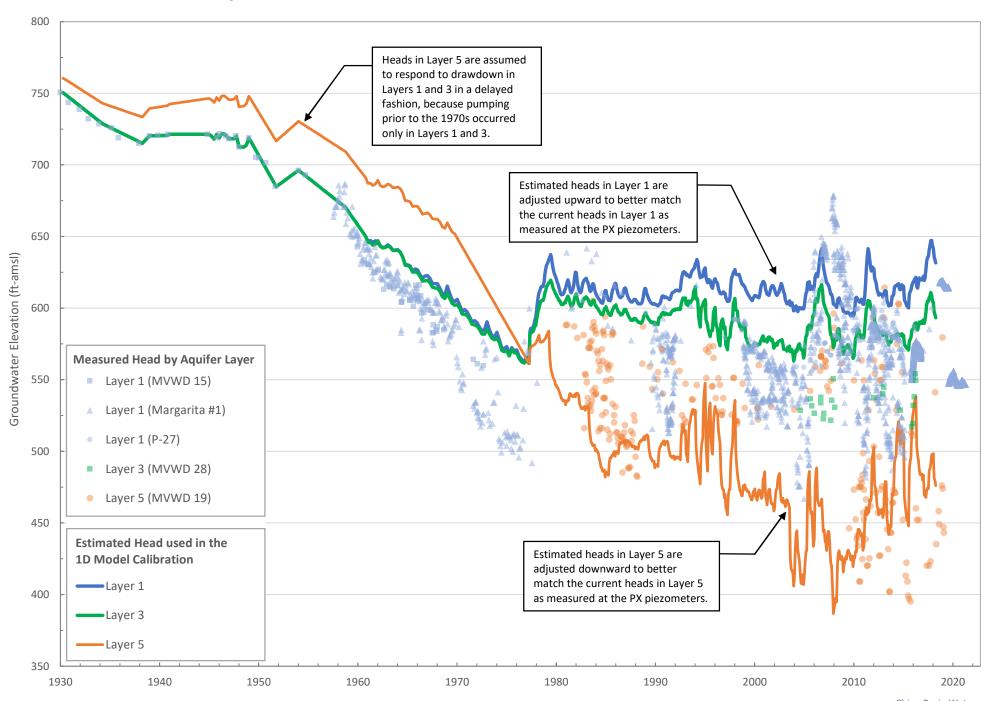
Last Revised: 08-22-2022

Figure 19. Measured Heads vs. Heads Used in Calibration of MVWD-28 1D Model - Calibration Run V23



Chino Basin Watermaster
1D Compaction Models in the Northwest MZ-1 Area
Last Revised: 08-22-2022

Figure 20. Measured Heads vs. Heads Used in Calibration of MVWD-28 1D Model - Calibration Run V24



Chino Basin Watermaster
1D Compaction Models in the Northwest MZ-1 Area
Last Revised: 08-22-2022

7.00 7.50 8.00 Subsidence (ft) 9.00 Compaction Simulated by PX 1D Model: **--**V22 Measured Subsidence: 9.50 InSAR at PX Site Benchmark 4311 Benchmark B-403 10.00 1990 2000 2010 2020

Figure 21. Measured Subsidence vs. Compaction Simulated by PX 1D Model - Calibration Run V22)

#### **WEST YOST**

Figure 22. Measured Subsidence vs. Compaction Simulated by PX 1D Model - Calibration Run V23

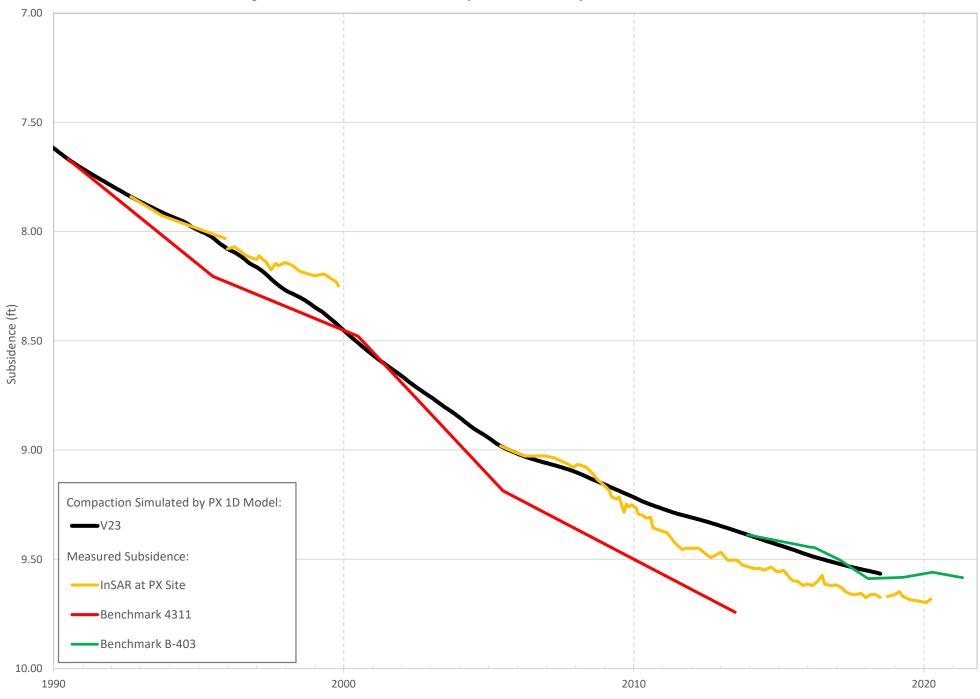


Figure 23. Measured Subsidence vs. Compaction Simulated by PX 1D Model - Calibration Run V24

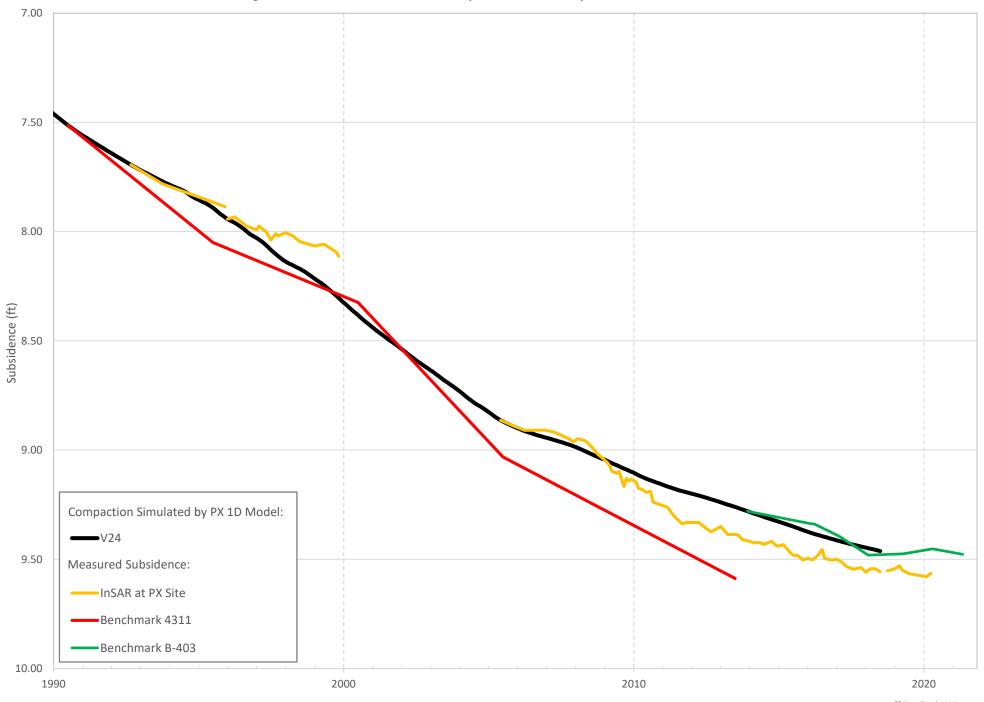


Figure 24. Measured Subsidence vs. Compaction Simulated by MVWD-28 1D Model - Calibration Run V22

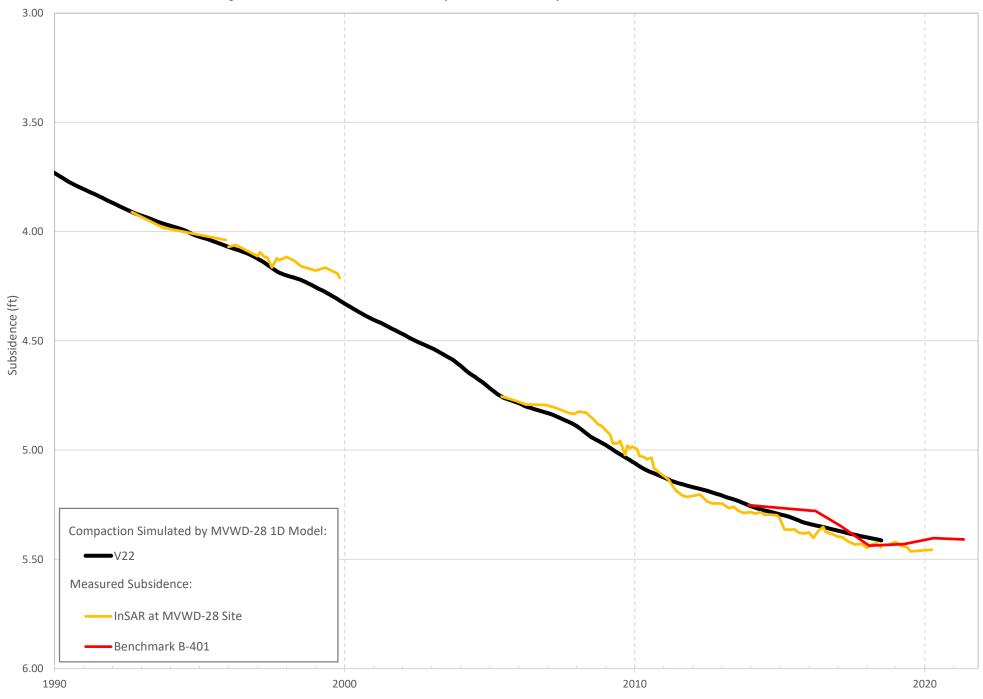


Figure 25. Measured Subsidence vs. Compaction Simulated by MVWD-28 1D Model - Calibration Run V23

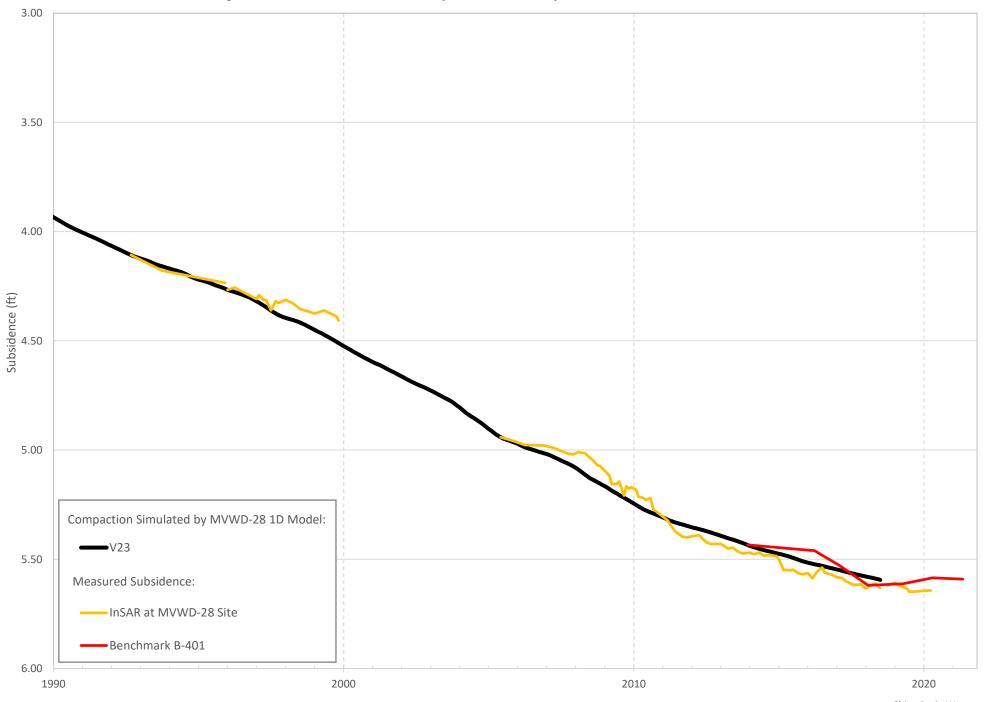
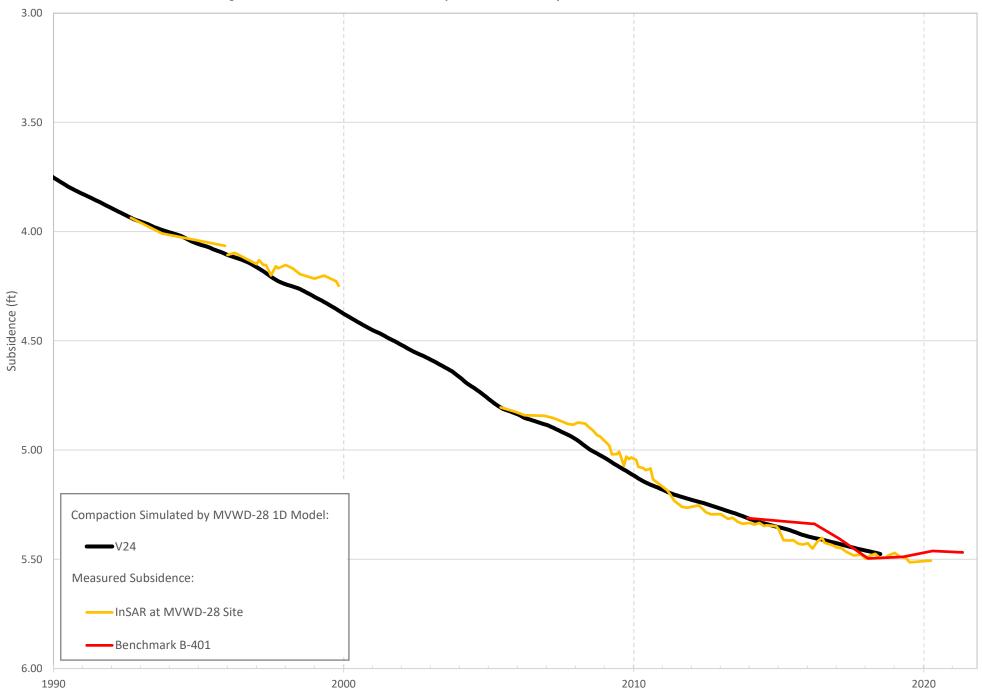


Figure 26. Measured Subsidence vs. Compaction Simulated by MVWD-28 1D Model - Calibration Run V24



# Appendix A

## Driller's Logs of PX and MVWD

Project Name: Pomona Extensometer Facility
Project Location: Montvue Park - Pomona, CA
Project Number: 007-018-762

Client:

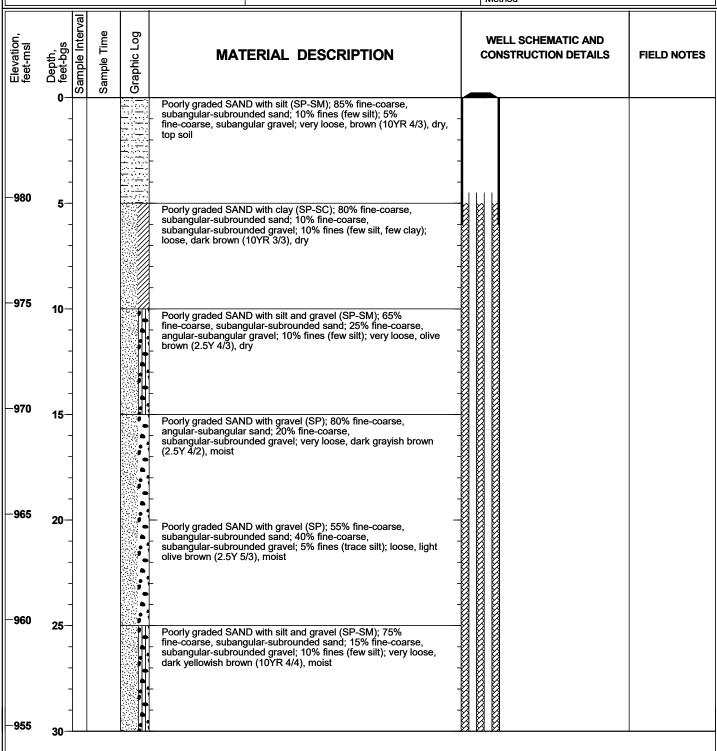
Report: WELL LOG; File: PX.GPJ;

007-018-762 Chino Basin Watermaster

#### **Boring Log / PX2**

Sheet 1 of 38

_					
Date Started 1/4/19	Date 1/29/19	Borehole Depth	1305.0 feet	Drilling Contractor	Cascade
Lat. 34° 4' 28.7934"	Long117° 43' 17.2554	Drill Bit Size/Type	17 1/2 in	Driller	J. Saldera; J. Martinez
Ground Surface 984.7		Screened Interval(s)	980-1,010; 1,235-1,275	Drill Rig Type	Foremost DR-24
Top of Casing Elevation		Depth to Groundwater	N/A	Drilling Method	Flooded Reverse Circulation
Logged By N. Sele	s, PG; R. Thacker	Reviewed By	M. Blazevic, PG, CHG	Sampling Method	Grab



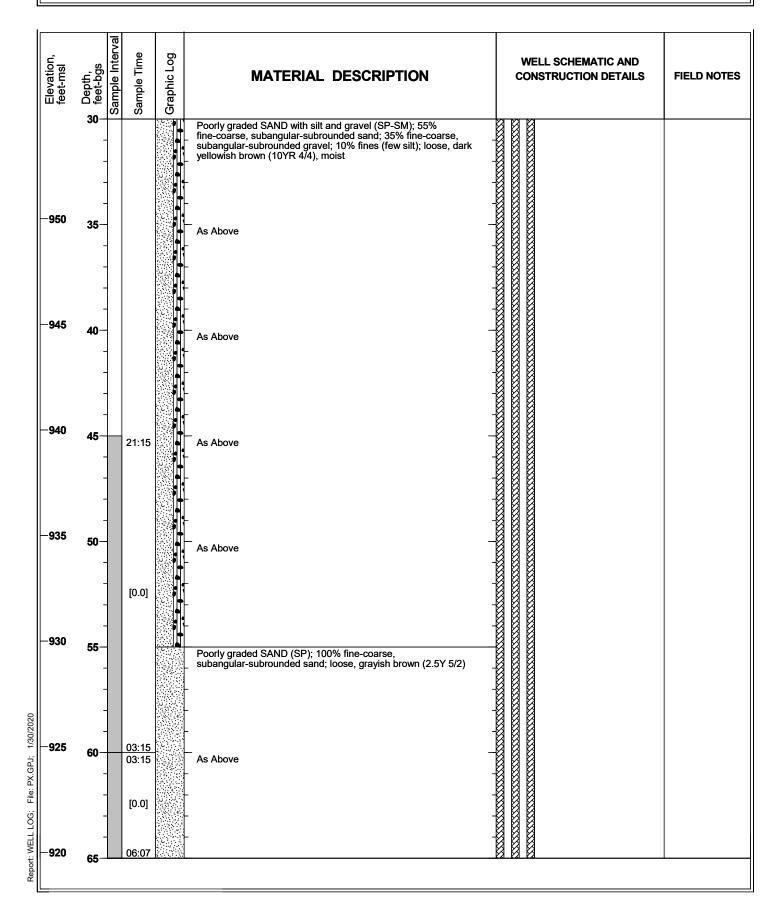
**Project Name: Pomona Extensometer Facility** 

Project Location: Montvue Park - Pomona, CA

**Project Number:** 007-018-762

**Client: Chino Basin Watermaster**  **Boring Log / PX2** 

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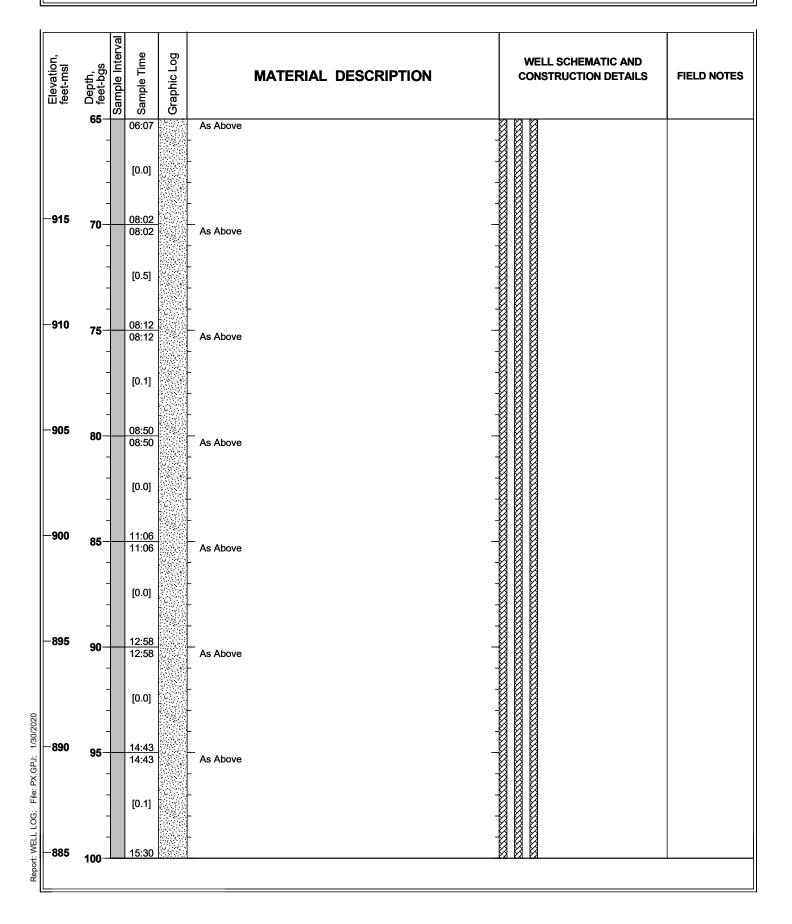
Project Number: 007-018-762

**Client:** 

Chino Basin Watermaster

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**Project Name: Pomona Extensometer Facility** 

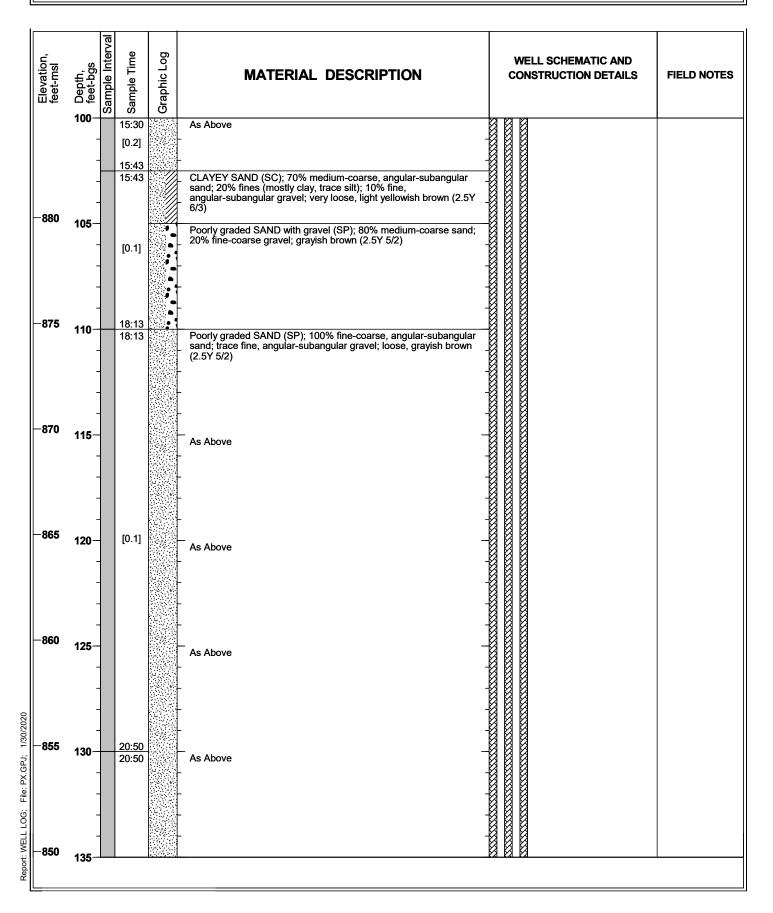
Project Location: Montvue Park - Pomona, CA

**Project Number:** 007-018-762

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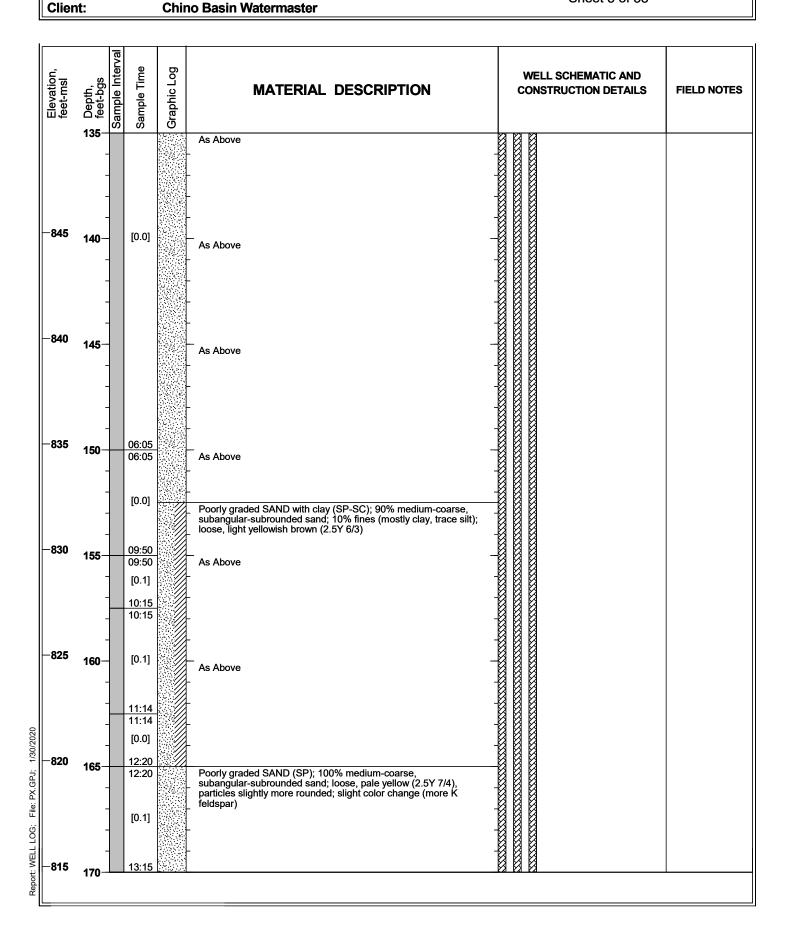


**Project Number:** 007-018-762

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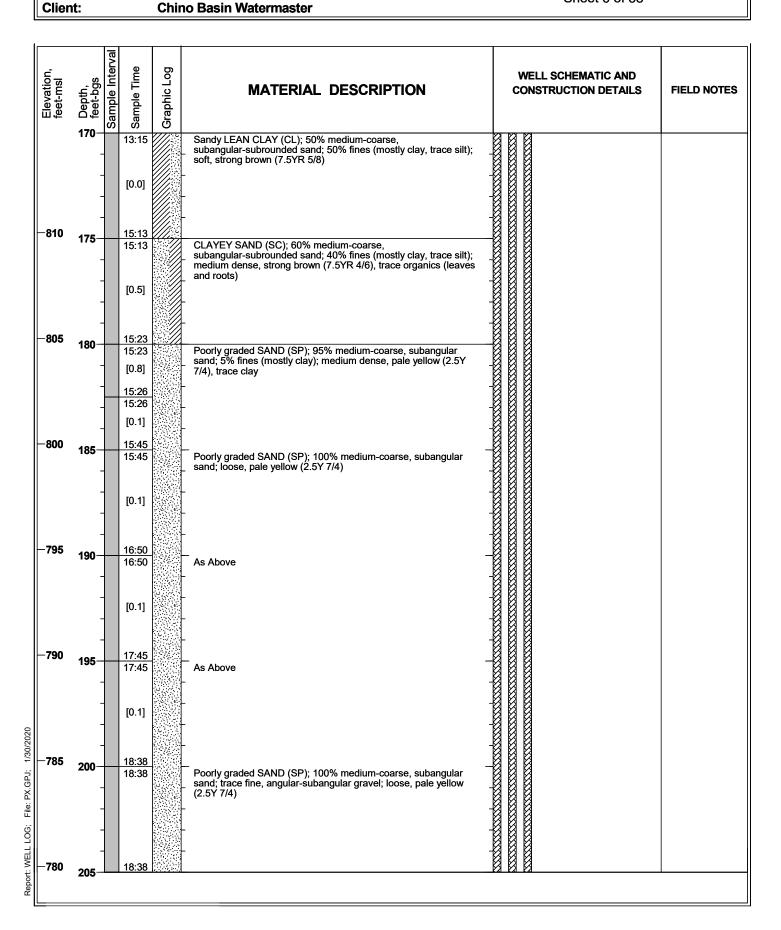


007-018-762 **Project Number:** 

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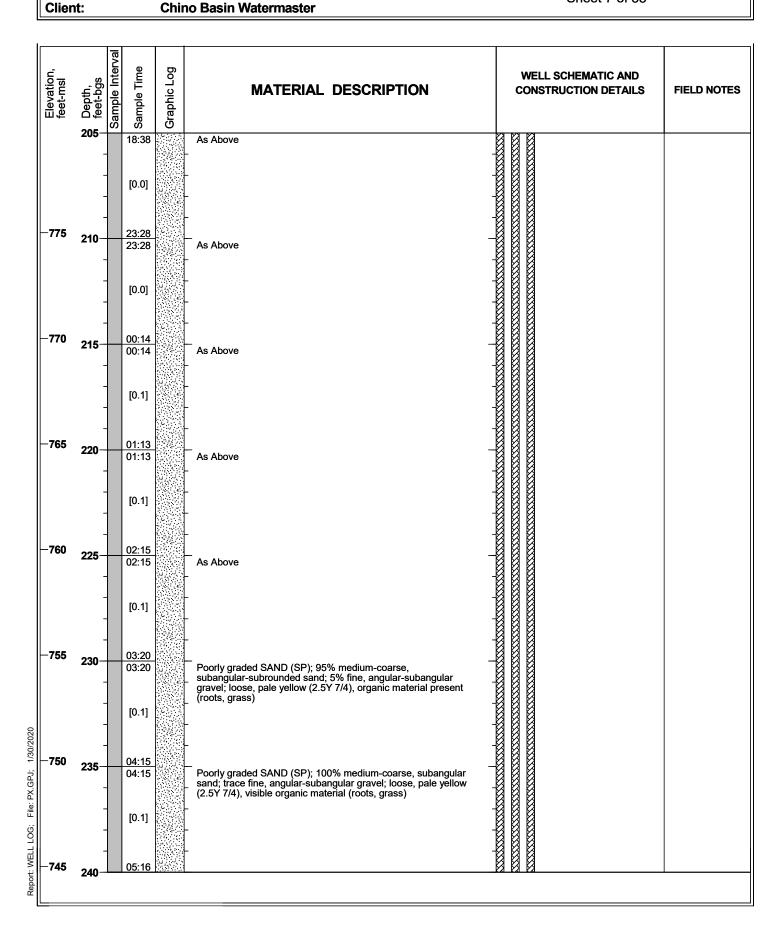


**Project Number:** 007-018-762

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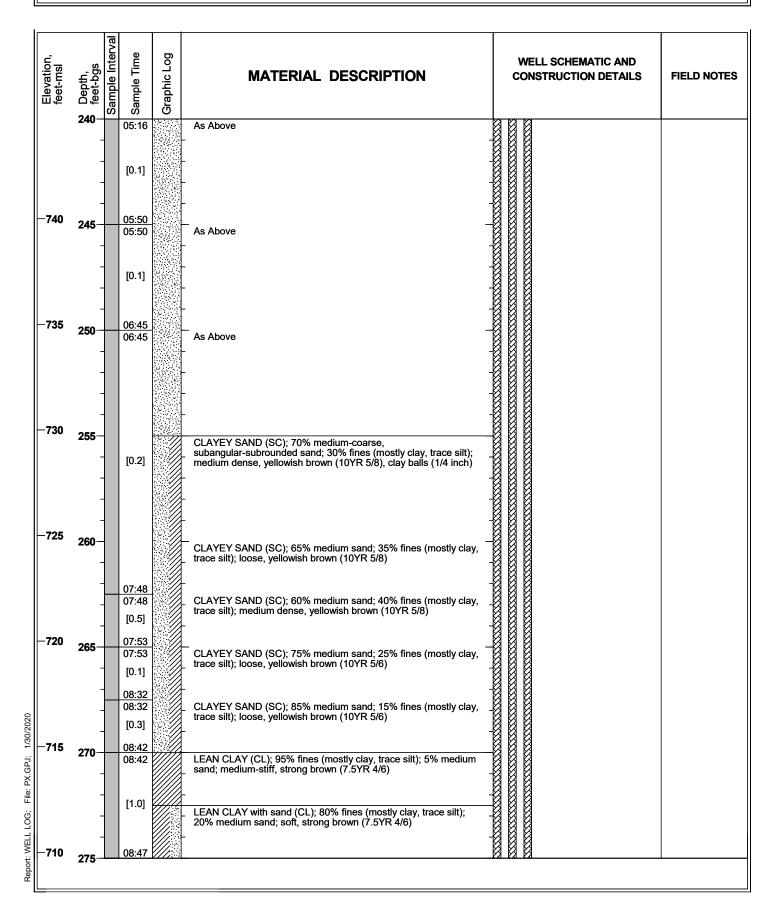


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## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	-	-	[0.3]		As Above  LEAN CLAY with sand (CL); 75% fines (mostly clay, trace silt); 25% medium-coarse, subangular-subrounded sand; soft, strong		
-705	- 280-		09:03 09:03		brown (7.5YR 4/6)  Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40%		
	- - -		[0.2]		medium-coarse, subangular-subrounded sand; soft, dark yellowish brown (10YR 4/6)		
-700	285-	-	09:28 09:28 [0.1]		Sandy LEAN CLAY (CL); 65% fines (mostly clay, trace silt); 35% medium-coarse, subangular-subrounded sand; medium-stiff, dark yellowish brown (10YR 4/6), trace fine gravel		
	-		10:05 10:05 [0.1]		Poorly graded SAND (SP); 100% medium sand; loose, yellow (10YR 7/6), trace organics		
-695	<b>290</b> -		10:30 10:30		Poorly graded SAND (SP); 100% medium-coarse, subangular sand; trace fines; loose, yellow (10YR 7/6), trace organics		
-690	- 295	-	11:26 11:26		Poorly graded SAND (SP); 100% medium sand; loose, yellow (10YR 7/6), trace fine-sand, trace organic material		
	- - -		[0.2]				
685	300-		11:58 11:58 [0.3]		CLAYEY SAND (SC); 85% medium sand; 15% fines (mostly clay, trace silt); loose, yellowish brown (10YR 5/8), trace organics		
680	305—		12:17 12:17 [0.0]		CLAYEY SAND (SC); 70% medium sand; 30% fines (mostly clay, trace silt); loose, yellowish brown (10YR 5/6)		
<b>67</b> F	- -		01:30 01:30 [0.1]		Poorly graded SAND (SP); 95% medium-coarse, subangular-subrounded sand; 5% fine, angular-subangular gravel; loose, light yellowish brown (2.5Y 6/3), trace organics		
675	310-		02:00	<u> </u>		<b>иии</b>	1

## **Boring Log / PX2**

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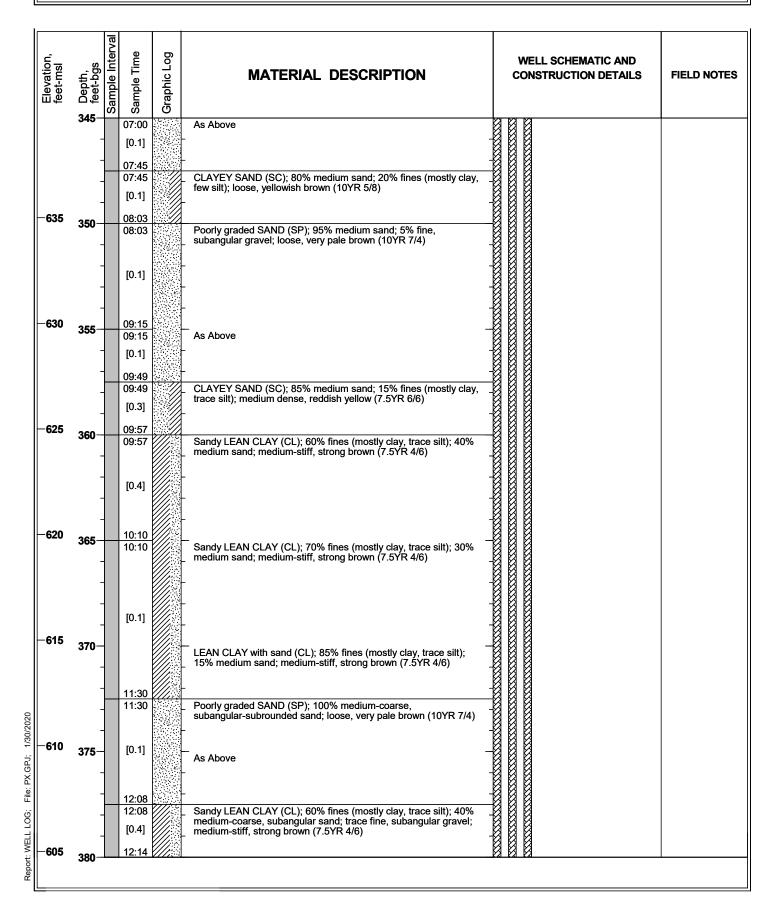
Elevation, feet-msl	<b>018</b> Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	-		[0.1]		As Above -		
-670	- 315—		02:50 02:50 [0.2]		- As Above		
COE	-		03:05 03:05 [0.3]		SILTY SAND (SM); 60% medium-coarse, subangular-subrounded sand; 40% fines (mostly silt, little clay); trace fine, angular-subangular gravel; loose, brown (10YR 4/3)		
-665	<b>320</b> –		03:13 03:13 [0.1] 03:32 03:32		Sandy SILT (ML); 70% fines (mostly silt, little clay); 30% medium-coarse, subangular-subrounded sand; trace fine, angular-subangular gravel; very soft, brown (10YR 4/3)  Poorly graded SAND (SP); 95% medium-coarse,		
-660	325—		[0.1] 03:58 03:58		subangular-subrounded sand; 5% fine, angular-subangular gravel; loose, light yellowish brown (2.5Y 6/3)		
	- -		[0.1]		gravel, loose, light yellowish brown (2.5Y 6/3)		
-655	330— -		04:35 04:35 [0.2] 04:47		SILT with sand (ML); 80% fines (mostly silt, some clay); 20% medium-coarse, subangular-subrounded sand; very soft, yellowish brown (10YR 5/4), trace organics		
-650	- - 335—		04:47 [0.1] 05:05 05:05		yellowish brown (10YR 5/6), trace organics	M M M	
	-		[0.1] 05:28 05:28		Poorly graded SAND (SP); 95% medium-coarse, subangular-subrounded sand; 5% fine, angular-subangular		
645	340—		[0.0] 06:30 06:30 [0.2]		gravel; loose, light yellowish brown (2.5Y 6/3), trace organics  As Above		
	-		06:45 06:45 [0.2]		- - -		
640	345-		07:00	<u> </u>			

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Client: Chino Basin Watermaster

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## **Boring Log / PX2**

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Elevation, feet-msl	SB Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	_		12:14		CLAYEY SAND (SC); 60% medium sand; 40% fines (mostly clay, trace silt); loose, strong brown (7.5YR 5/6)		
	_				-		
	-		[0.2]		-		
	-				-		
-600	385-		12:41 12:41		Poorly graded SAND (SP); 95% medium-coarse,		
	_				subangular-subrounded sand; 5% fines (mostly clay, trace silt); loose, very pale brown (10YR 7/4)		
	_		[0.1]				
	-				-		
-595	-		14:00				
	390-		14:00		Poorly graded SAND (SP); 100% medium-coarse, subangular-subrounded sand; loose, very pale brown (10YR 7/4)		
			[0.1]		, , , , ,		
			14:20 14:20		CLAYEY SAND (SC); 65% medium-coarse,		
	_		[0.1]		subangular-subrounded sand; 35% fines (mostly clay, trace silt); medium dense, very pale brown (10YR 7/4)		
-590	395-		14:38		OLAVEV CAND (CO) COOK madition		
	-		14:38		CLAYEY SAND (SC); 60% medium-coarse, subangular-subrounded sand; 40% fines (mostly clay, trace silt); loose, strong brown (7.5YR 5/6)		
	-		[0.3]		-		
	_		[0.0]		-		
<b>505</b>	_		44.54		-		
-585	400-		14:54 14:54		-		
	-				-		
			[0.2]		As Above		
	_						
-580	405-		15:18				
	-		15:18 [0.2]		LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt); 20% medium sand; medium-stiff, strong brown (7.5YR 5/6)		
	-		15:30		-		
	-		15:30		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% medium sand; medium-stiff, reddish yellow (7.5YR 7/6)		
	-		[0.0]				
575	410-		22:35 22:35		CLAYEY SAND (SC); 60% medium-coarse,		
	-		[0.1]		subangular-subrounded sand; 40% fines (mostly clay, little silt); medium dense, yellowish brown (10YR 5/6)		
	-		23:15 23:15		LEAN CLAY with sand (CL); 75% fines (little silt, trace clay); 25%		
	-		[0.5]		medium-coarse, subangular-subrounded sand; medium-stiff, dark yellowish brown (10YR 4/4), clay balls		
-570	_		23:20				

## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	415		23:20		As Above		
	-		[0.2]		-		
	-		23:35	///	-		
	-		23:35	///	Sandy LEAN CLAY (CL); 60% fines (mostly clay, few silt); 40% medium-coarse, subangular-subrounded sand; soft, yellowish		
	-		[0.2]	///	brown (10YR 5/6), clay balls		
-565	420-		23:50		<del>-</del>		
			23:50		As Above		
			[0.0]				
	_		00:15 00:15		As Above		
	-		[0.1]		AS ADOVE		
	-			///	-		
-560	425-		00:45 00:45		CLAYEY SAND (SC); 70% medium-coarse,		
	-		[0.2]		subangular-subrounded sand; 30% fines (mostly clay, trace silt); trace fine, angular gravel; loose, yellowish brown (10YR 5/4), clay		
	_				balls		
	_		00:56 00:56		As Above		
			[0.1]				
-555	_		01:43		_		
000	430-		01:43		As Above		
	-		[0.2]		<del>-</del>		
	-		01:55		-		
	-		01:55		CLAYEY SAND (SC); 60% medium-coarse, subangular-subrounded sand; 40% fines (mostly clay, trace silt);		
	_		[0.3]		trace fine, angular gravel; loose, yellowish brown (10YR 5/4), clay balls		
-550	435-		02:05				
			02:05		CLAYEY SAND (SC); 70% medium-coarse, subangular-subrounded sand; 30% fines (mostly clay, trace silt);		
	_		[0.3]		trace fine, angular gravel; loose, yellowish brown (10YR 5/4), clays balls		
	_		02:15		An Abour		
	-		02:15		AS ADOVE	ra ra ra	
	-		[0.3]		<del>-</del>		
-545	440-		02:25 02:25		<u> </u>	888	
	-		[0.3]		-		
	-		02:35		-		
	_		02:35		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40%		
	_		[0.1]		medium-coarse, subangular-subrounded sand; soft, yellowish brown (10YR 5/4), clay balls, trace organic material		
-540	445		03:15		·		
	445-		03:15		Poorly graded SAND (SP); 95% medium-coarse, subangular-subrounded sand; 5% fine, angular gravel; loose, light		
	-		[0.0]		yellowish brown (2.5Y 6/3), trace organic material		
	-		04:30		-		
	-		04:30		As Above		
	-		[0.0]		-		
-535	450-		05:50				

## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	-		05:50		As Above		
	-		[0.1]		-		
530	-		06:48		-		
330	455-		06:48		As Above		
	-	-	[0.1]		-		
	-		07:24		-		
	-		07:24 [0.1]		CLAYEY SAND (SC); 70% medium-coarse, subangular-subrounded sand; 30% fines (mostly clay, trace silt); trace fine, angular gravel; loose, yellowish brown (10YR 5/4)		
525	460-		07:49 07:49	- 4	Poorly graded SAND (SP); 100% medium-coarse, subangular		
	_		[0.1]		sand; trace fines; loose, yellow (10YR 7/6)		
	_		08:27 08:27		Poorly graded SAND (SP); 100% medium-coarse, subangular		
	_		[0.1]		sand; trace undefined gravel; trace fines; loose, yellow (10YR 7/6)		
520	465-		09:06				
	405		09:06 [0.0]		Poorly graded SAND (SP); 100% medium-coarse, subangular sand; trace fines; loose, yellow (10YR 7/6)		
	-		10:06		-		
	-	-	10:06		-		
	-	-	[0.2]		-		
515	470-		10:22 10:22		As Above		
	-		[0.1]		-		
	-		10:45		-		
	-		10:45		CLAYEY SAND (SC); 85% medium sand; 15% fines (mostly clay, trace silt); loose, yellowish brown (10YR 5/4), trace fine sand		
	-	-	[0.3]				
510	475-		10:53 10:53		Poorly graded SAND (SP); 95% medium sand; 5% fines (mostly		
	-		. 5.55		clay, trace silt); loose, yellow (10YR 7/6), trace fine sand		
	-		[0.1]		Poorly graded SAND (SP); 100% medium-coarse, subangular sand; trace fines; loose, yellow (10YR 7/6)		
F0-F	-		44.00		-		
505	480-		11:38 11:38	1/	CLAYEY SAND (SC); 70% medium-coarse,		
	-		[0.2] 11:53		subangular-subrounded sand; 30% fines (mostly clay, trace silt); trace fine, angular gravel; loose, yellowish brown (10YR 5/4)		
	-		11:53		CLAYEY SAND (SC); 85% medium sand; 15% fines (mostly clay,		
	_		[0.2]		trace silt); loose, yellowish brown (10YR 5/4)		
500	485-		12:09				

## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	405		12:09 [0.0]		Poorly graded SAND (SP); 95% medium sand; 5% fines (mostly clay, trace silt); loose, yellow (10YR 7/6), trace fine sand		
	-		13:09		-		
	-		13:09		-		
-495	-		[0.1] 13:30		-		
-00	490-		13:30		CLAYEY SAND (SC); 85% medium sand; 15% fines (mostly clay, trace silt); loose, yellow (10YR 7/6), trace fine sand; trace		
	_		[0.1]		organics' -		
	_		14:04 14:04		LEAN CLAY with sand (CL); 85% fines (mostly clay, trace silt); 15% medium sand; medium-stiff, yellowish brown (10YR 5/4)		
	-		[0.4]		15% medium sand; medium-still, yellowish brown (101K 5/4) -		
-490	495-		14:10 14:10		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% medium sand; medium-stiff, brownish yellow (10YR 6/6)		
	-		[0.1]		medium sand; medium-stiff, brownish yellow (10YR 6/6)		
	-		14:30 14:30		- CLAYEY SAND (SC); 70% medium sand; 30% fines (mostly clay,		
	_		[0.1]		trace silt); medium dense, yellow (10YR 7/6)		
485	500-		14:48		D. J.		
	-		14:48		Poorly graded SAND (SP); 95% medium-coarse, subangular sand; 5% fines (mostly clay, trace silt); loose, yellow (10YR 7/6)		
	-		[0.1]		-		
	-				-		
-480	-		15:30		-		
	<b>505</b> —		15:30		As Above		
	-		ro 01		-		
	-		[0.0]		-		
-475	-		47.00		-		
4/5	510-		17:32 17:32		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% medium-coarse, subangular-subrounded sand; soft, dark		
	-		[0.1]		yellowish brown (10YR 4/4), clay balls		
	=		18:15 18:15		As Above		
	-		[0.1]		-		
470	515-		18:36 18:36		As Above		
	-		[0.3]		-		
	-		18:45 18:45		CLAYEY SAND (SC); 70% medium-coarse,		
	-		[0.1]		subangular-subrounded sand; 30% fines (mostly clay, trace silt); loose, yellowish brown (10YR 5/4), clay balls		
465	520-		19:30		· · ·		

## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	520-		19:30		As Above		
	-		[0.1]		·		
	-		19:54		·		
	-		19:54		Poorly graded SAND (SP); 100% medium-coarse, subangular-subrounded sand; trace fine, angular-subangular		
	-	-	[0.1]		gravel, loose, pale brown (10YR 6/3), trace fines		
460	525-		20:15 20:15		Poorly graded SAND (SP); 90% medium-coarse,		
	-		[0.0]		subangular-subangular		
	_				gravel, 5% fines (mostly clay); loose, light yellowish brown (10YR 6/4), very small clay balls, trace fines		
			21:44 21:44		Poorly graded SAND (SP); 95% medium-coarse,		
	-		[0.0]		subangular-subrounded sand; 5% fine, angular-subangular gravel; loose, light yellowish brown (10YR 6/4), trace fines		
455	-		22:39		gravar, recess, light years more provint (1011110), tages miles		
455	530-		22:39		Poorly graded SAND (SP); 90% medium-coarse,		
	-		[0.1]		subangular-subrounded sand; 10% fine, angular-subangular gravel; loose, light yellowish brown (10YR 6/4), trace fines		
	-		22:58		·		
	-	-	22:58		CLAYEY SAND (SC); 60% fine-coarse, subangular-subrounded sand; 40% fines (mostly clay, trace silt); medium dense, olive		
	_		[0.3]		brown (2.5Y 4/4), clay balls		
450	535-		23:08				
	_		23:08		LEAN CLAY (CL); 90% fines (mostly clay, trace silt); 10% fine-coarse, subangular-subrounded sand; medium-stiff, brown		
			[0.2]		(10YR 5/3), clay balls		
	_		23:20 23:20		As Above		
	-		[0.3]				
445	-				<del>-</del>		
445	540-		23:30 23:30		CLAYEY SAND (SC); 65% medium-coarse,		
	-	-	[0.2]		subangular-subrounded sand; 35% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4), clay balls		
	-		23:45		-		
	-		23:45		LEAN CLAY (CL); 90% fines (mostly clay, trace silt); 10% fine-coarse, subangular-subrounded sand; medium-stiff, brown		
	_		[0.2]		(10YR 5/3), clay balls		
440	545-		23:58				
	-		23:58		Sandy LEAN CLAY (CL); 65% fines (mostly clay, trace silt); 35% fine-coarse, subangular-subrounded sand; soft, brown (10YR		
			[0.0]		5/3), clay balls		
			00:05 00:05		LEAN CLAY (CL); 90% fines (mostly clay, trace silt); 10%		
	-		[0.1]		fine-coarse, subangular-subrounded sand; medium-stiff, brown (10YR 5/3), clay balls		
435	-		00:55				
<del>-1</del> JJ	550-		00:55		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40%		
	-	-	[0.1]		fine-coarse, subangùlar-subrounded`sand; soft, brown (10ŶR 5/3), clay balls		
	-		01:34		-		
	-		01:34		CLAYEY SAND (SC); 60% medium-coarse, subangular-subrounded sand; 40% fines (mostly clay, trace silt);		
	-		[0.2]		loose, brown (10YR 5/3), clay balls		
430	555-		01:48				

## **Boring Log / PX2**

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Elevation, feet-msl	<b>99</b> Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	- - -		01:48 [0.4] 01:55 01:55 [0.3]		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% medium-coarse, subangular-subrounded sand; trace fine, angular-subangular gravel; soft, brown (10YR 4/3), clay balls  As Above		
- <b>425</b>	<b>560</b> —		02:05 02:05 [0.3] 02:15		CLAYEY SAND with gravel (SC); 60% medium-coarse, subangular-subrounded sand; 20% fine, angular-subangular gravel; 20% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4), clay balls		
-420	- 565-		02:15 [0.2] 02:30 02:30		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% medium-coarse, subangular-subrounded sand; soft, olive brown (2.5Y 4/4), clay balls  CLAYEY SAND (SC); 60% medium-coarse,		
	- - -		[0.2] 02:44 02:44 [0.0]		subangular-subrounded sand; 40% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4), clay balls  CLAYEY SAND (SC); 70% medium-coarse, subangular-subrounded sand; 30% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4), clay balls		
415	570— -		03:45 03:45 [0.2] 04:00 04:00		LEAN CLAY (CL); 90% fines (mostly clay, trace silt); 10% fine-medium sand; soft, brown (10YR 5/3), clay balls  Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 30%		
410	- 575—		04:53 04:53 [0.1]		fine-coarse, subangular-subrounded sand; soft, brown (10YR 5/3)  As Above		
405	-		05:23 05:23 [0.0]		Poorly graded SAND (SP); 95% fine-coarse, subangular-subrounded sand; 5% fine, angular-subangular gravel; loose, light olive brown (2.5Y 5/3)		
<del>-1</del> UƏ	580— - -		06:58 06:58 [0.1] 07:20 07:20		Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 30% fine-coarse, subangular-subrounded sand; soft, brown (10YR 5/3)  CLAYEY SAND with gravel (SC); 60% medium-coarse,		
400	- 585—		[0.3] 07:28 07:28		subangular-subrounded sand; 20% fine, angular-subangular gravel; 20% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4)  Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 30% fine-coarse, subangular-subrounded sand; soft, brown (10YR 5/3)		
395	-		[0.1] 08:20		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% fine-coarse, subangular-subrounded sand; soft, brown (10YR 5/3)		

## **Boring Log / PX2**

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Elevation, feet-msl	<b>66</b> Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	- - -		[0.3]		Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 30% fine-coarse, subangular-subrounded sand; soft, brown (10YR 5/3), trace fine cobbles		
-390	- <b>595</b>		08:38 08:38		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% medium-coarse, subangular-subrounded sand; trace fine, angular-subangular gravel; soft, brown (10YR 4/3)		
-385	- - 600-		09:00			High-Solids Bentonite	
	- - -		[0.1]		Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 30% fine-medium sand; soft, strong brown (7.5YR 5/8)  -	High-Solids Bentonite Grout	
-380	605— - -		10:15 10:15 [0.2]				
375	610— -		10:40 10:40 [0.3]		CLAYEY SAND (SC); 70% fine-coarse, subangular-subrounded sand; 30% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/3)	High-Solids Bentonite Grout	
370	- 615—		11:00 11:00 [0.1]				
365	- - 620-		11:40 11:40 [0.1] 12:25		CLAYEY SAND (SC); 65% fine-medium sand; 35% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/6)		
	-		12:25 [0.0] 13:26 13:26 [0.1]		CLAYEY SAND (SC); 85% medium-coarse, subangular-subrounded sand; 15% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4)  Poorly graded SAND (SP); 95% fine-medium sand; 5% fines (mostly clay, trace silt); loose, olive gray (5Y 5/2)		
360	625-		13:50				

## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	- - -		[0.1]		CLAYEY SAND (SC); 60% fine-medium sand; 40% fines (mostly clay, trace silt); loose, light yellowish brown (10YR 6/4)  -		
355	630— -		14:30 14:30 [0.1]		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% fine-medium sand; medium-stiff, light yellowish brown (10YR 6/4)		
-350	- 635—		15:15 15:15 [0.1] 15:53 15:53	-	Poorly graded SAND (SP); 95% fine-medium sand; 5% fines (mostly clay, trace silt); loose, olive gray (5Y 5/2)  Poorly graded SAND (SP); 95% fine-coarse,		
	- -		[0.1] 16:30 16:30		subangular-subrounded sand; 5% fine, subrounded gravel; trace fines (mostly clay, trace silt); loose, olive gray (5Y 5/2)  LEAN CLAY (CL); 90% fines (mostly clay, trace silt); 10% fine-medium sand; soft, light olive brown (2.5Y 5/6)		
345	640— -		[0.3] 16:40 16:40 [0.2]		LEAN CLAY (CL); 100% fines (mostly clay, trace silt); trace fine sand; soft, light olive brown (2.5Y 5/6)		
340	-		16:54 16:54 [0.1]		As Above		
340	645— -		17:19 17:19 [0.0] 18:50 18:50		Poorly graded SAND (SP); 95% medium-coarse, subangular-subrounded sand; 5% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4)		
335	650		[0.2] 19:05 19:05		Poorly graded SAND (SP); 95% medium-coarse, subangular-subrounded sand; 5% fine, angular-subangular gravel; loose, light olive brown (2.5Y 5/4)  LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt);		
	- -		[0.1] 19:30 19:30		20% medium-coarse, subangular-subrounded sand; trace fine, angular gravel; soft, brown (10YR 4/3), clay balls  Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 30% fine-coarse, subangular-subrounded sand; soft, light olive brown		
330	- 655—		[0.1] 20:05 20:05		(2.5Y 5/3), clay balls  Poorly graded SAND (SP); 95% medium-coarse, subangular-subrounded sand; 5% fine, angular-subrounded sand; 5% fine, ang		
	<u>-</u>		[0.0]		gravel; trace fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/4), dry, trace clay balls		
325	660-		22:10				

## **Boring Log / PX2**

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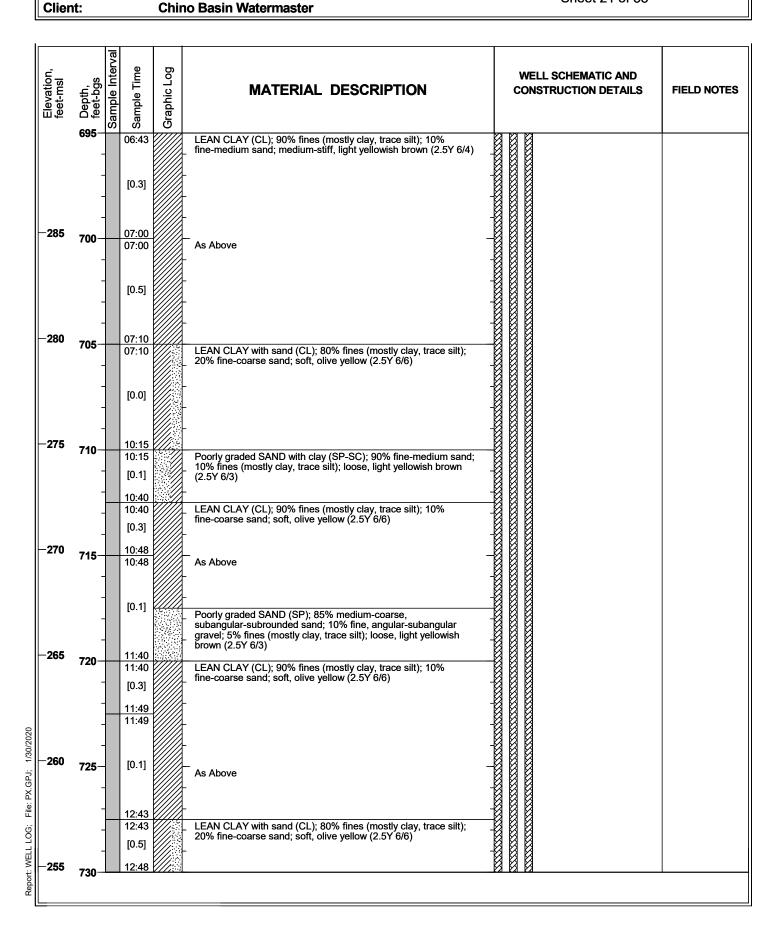
Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	-		22:10 [0.1] 22:30		LEAN CLAY (CL); 95% fines (mostly clay, trace silt); 5% fine-coarse, subangular-subrounded sand; soft, light brownish gray (2.5Y 6/2), clay balls		
220	-		22:30		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% fine-coarse, subangular-subrounded sand; soft, light brownish gray (2.5Y 6/2)		
-320	665-		22:50 22:50 [0.2]		LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt); 20% medium-coarse, subangular-subrounded sand; soft, olive brown (2.5Y 4/3), clay balls		
	_		23:04 23:04		CLAYEY SAND (SC); 60% medium-coarse,		
-315	-		[0.0]		subangular-subrounded sand; 30% fines (mostly clay, trace silt); 10% fine, angular-subangular gravel; loose, light yellowish brown (2.5Y 6/3), trace fine-grained sand.		
JIJ	670 –		00:40		CLAYEY SAND (SC); 75% medium-coarse, subangular-subrounded sand; 15% fines (mostly clay, trace silt); 10% fine, angular-subangular gravel; loose, light yellowish brown (2.5Y 6/3)		
	-		[0.1]		As Above		
-310	675-		01:55	//_	Dearly graded CAND (CD), 000/ medium accura		
	-		[0.1]		Poorly graded SAND (SP); 90% medium-coarse, subangular-subrounded sand; 10% fine, angular-subangular gravel; trace fines (mostly clay, trace silt); loose, light yellowish brown (2.5Y 6/3)		
-305	_		03:27		- -		
303	680 –		03:27		Poorly graded SAND (SP); 85% medium-coarse, subangular-subrounded sand; 10% fine, angular-subangular gravel; 5% fines (mostly clay, trace silt); loose, light yellowish brown (2.5Y 6/3)		
	-		[0.0]		- -	M M M	
-300	685-		05:10		_		
	-		05:10 [0.1]		As Above -		
-295	- - 690		06:30		- -		
	-		06:30		LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt); 20% fine-coarse sand; soft, olive yellow (2.5Y 6/6)		
	-		[0.4]		- -		
290	695-		06:43	///:		<u> </u>	

007-018-762 **Project Number:** 

**Chino Basin Watermaster** 

#### **Boring Log / PX2**

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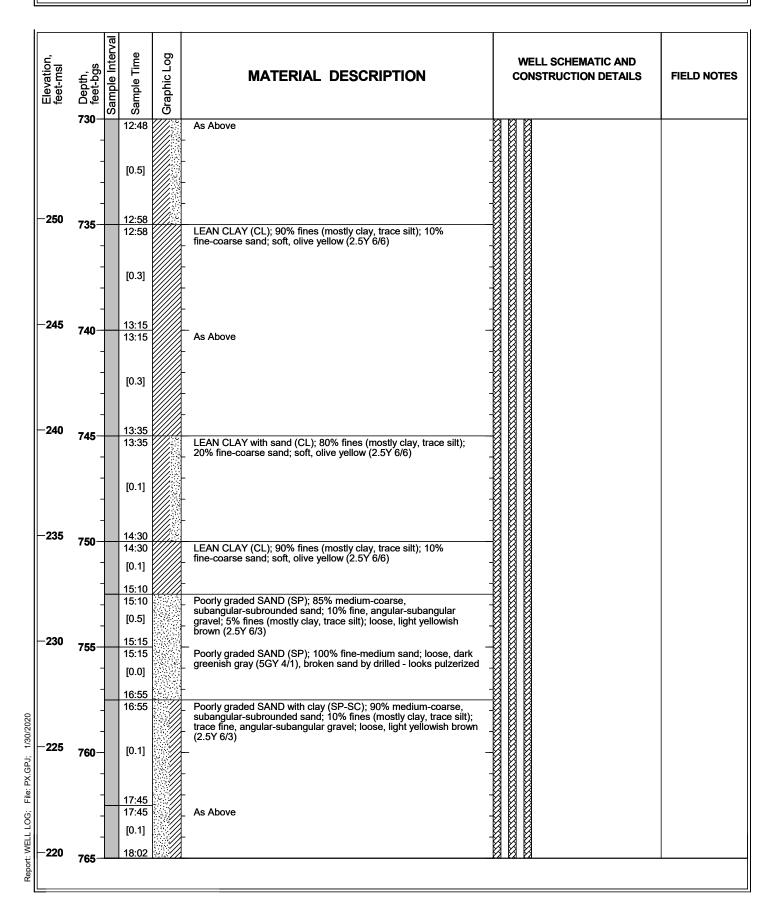


**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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## **Boring Log / PX2**

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Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	-	-	18:02 [0.1] 18:47		CLAYEY SAND (SC); 60% medium-coarse, subangular-subrounded sand; 40% fines (mostly clay, trace silt); loose, light olive brown (2.5Y 5/3)		
-215	-		18:47 [0.8] 18:50		Poorly graded SAND (SP); 100% medium-coarse, subangular-subrounded sand; trace fine, angular-subangular gravel; trace fines (mostly clay, trace silt); very loose, light yellowish brown (2.5Y 6/3)		
210	770- - -	-	18:50 [0.2]		LEAN CLAY (CL); 100% fines (mostly clay, trace silt); trace medium-coarse sand; medium-stiff, olive brown (2.5Y 4/4), clay balls		
-210	-		19:05 [0.2]		CLAYEY SAND (SC); 65% medium-coarse, subangular-subrounded sand; 30% fines (mostly clay, trace silt); 5% fine, angular-subangular gravel; very loose, light yellowish brown (2.5Y 6/4)		
	775-		19:20 19:20 [0.1]		Poorly graded SAND with clay (SP-SC); 80% medium-coarse, subangular-subrounded sand; 10% fine, subangular-subrounded gravel; 10% fines (mostly clay, trace silt); very loose, light yellowish brown (2.5Y 6/3)		
-200	-	-	19:38 19:38 [0.4]		CLAYEY SAND (SC); 70% medium-coarse, subangular-subrounded sand; 30% fines (mostly clay); trace fine, angular-subangular gravel; loose, olive brown (2.5Y 4/4)		
	<b>780</b> -	-	19:45 19:45		CLAYEY SAND (SC); 75% medium-coarse, subangular-subrounded sand; 15% fines (mostly clay, trace silt); 10% fine, angular-subangular gravel; very loose, light yellowish brown (2.5Y 6/3)		
	-		20:10		As Above		
-195	785- - -		20:10		As Above -		
	-		[0.1]		As Above .		
	<b>790</b> -		21:30 21:30		FAT CLAY (CH); 100% fines (mostly clay); medium-stiff, olive brown (2.5Y 4/3)		
400	-		[0.1]				
-190	795- - -		22:06 22:06 [0.2]		CLAYEY SAND with gravel (SC); 60% medium-coarse, subangular-subrounded sand; 25% fine, angular-subangular gravel; 15% fines (mostly clay, trace silt); very loose, light olive brown (2.5Y 5/3)		
40=	-		22:20 22:20		Sandy LEAN CLAY (CL); 70% fines (mostly clay, trace silt); 25% medium-coarse, subangular-subrounded sand; 5% fine, angular gravel; medium-stiff, light olive brown (2.5Y 5/3)		
-185	800-			///:		888	

## **Boring Log / PX2**

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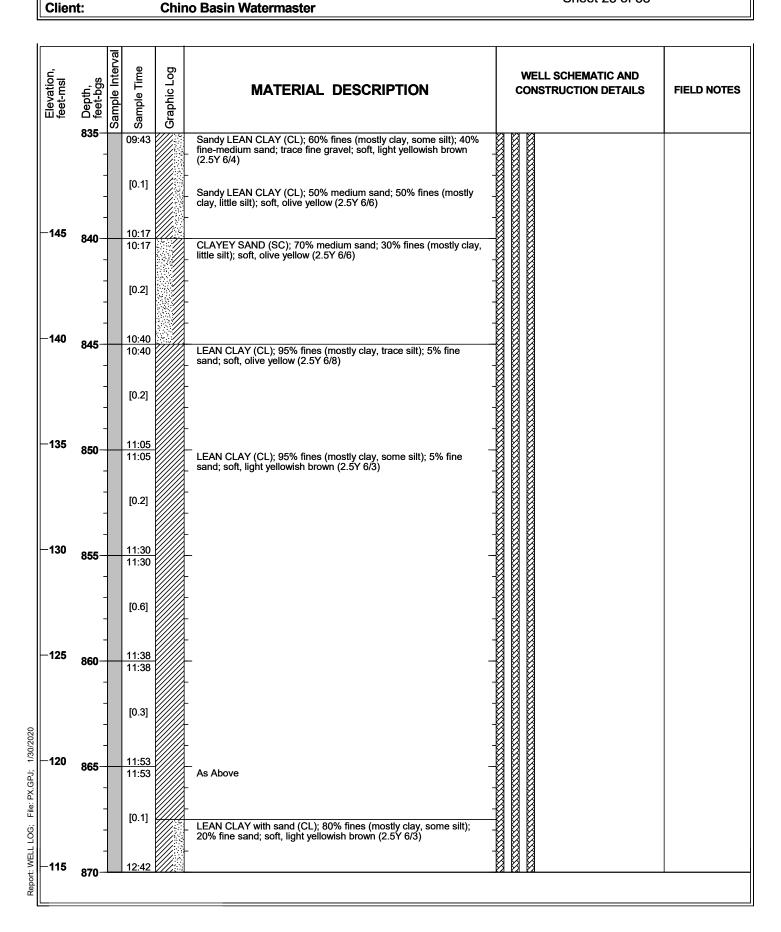
Elevation, feet-msl	<b>608</b> Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	- - -		[0.1]		Poorly graded SAND with clay and gravel (SP-SC); 70% medium-coarse, subangular-subrounded sand; 20% fine, angular-subangular gravel; 10% fines (mostly clay, trace silt); very loose, light yellowish brown (2.5Y 6/3)		
−18 <b>0</b>	805-		23:11 23:11 [0.0] 03:26		FAT CLAY (CH); 100% fines (mostly clay); trace medium-coarse, subangular-subrounded sand; medium-stiff, olive brown (2.5Y 4/3)		
-175	- 810-		03:26 [0.2] 03:38		LEAN CLAY (CL); 90% fines (mostly clay); 10% medium-coarse, subangular-subrounded sand; medium-stiff, olive brown (2.5Y 4/3)		
	- -		03:38 [0.1] 03:56 03:56		LEAN CLAY with sand (CL); 80% fines (mostly clay); 20% fine-medium sand; medium-stiff, olive brown (2.5Y 4/3)  FAT CLAY (CH); 100% fines (mostly clay); medium-stiff, olive brown (2.5Y 4/3)		
-170	- 815—		[0.3] 04:05 04:05 [0.3]		LEAN CLAY (CL); 100% fines (mostly clay); trace medium-coarse, subangular-subrounded sand; medium-stiff, olive brown (2.5Y 4/3)		
	- -		04:13 04:13 [0.2]		As Above		
-165	820- -		04:24 04:24 [0.1]		LEAN CLAY with sand (CL); 80% fines (mostly clay); 20% fine-medium sand; medium-stiff, olive brown (2.5Y 4/3)		
-160	- 825-		04:41 04:41 [0.1] 05:07		Sandy LEAN CLAY (CL); 65% fines (mostly clay); 35% fine-medium sand; medium-stiff, olive brown (2.5Y 4/3)		
	-		[0.0]		Poorly graded SAND with gravel (SP); 80% medium-coarse, subangular-subrounded sand; 15% fine, angular-subangular gravel; 5% fines (mostly clay, trace silt); very loose, light yellowish brown (2.5Y 6/4)		
-155	830— - -		09:19 09:19 [0.1]				
-150	- 835—		09:39 [0.6] 09:43		Sandy LEAN CLAY (CL); 65% fines (mostly clay, some silt); 35% fine-medium sand; trace fine gravel; medium-stiff, light yellowish brown (2.5Y 6/4)		

**Project Number:** 007-018-762

**Chino Basin Watermaster** 

#### **Boring Log / PX2**

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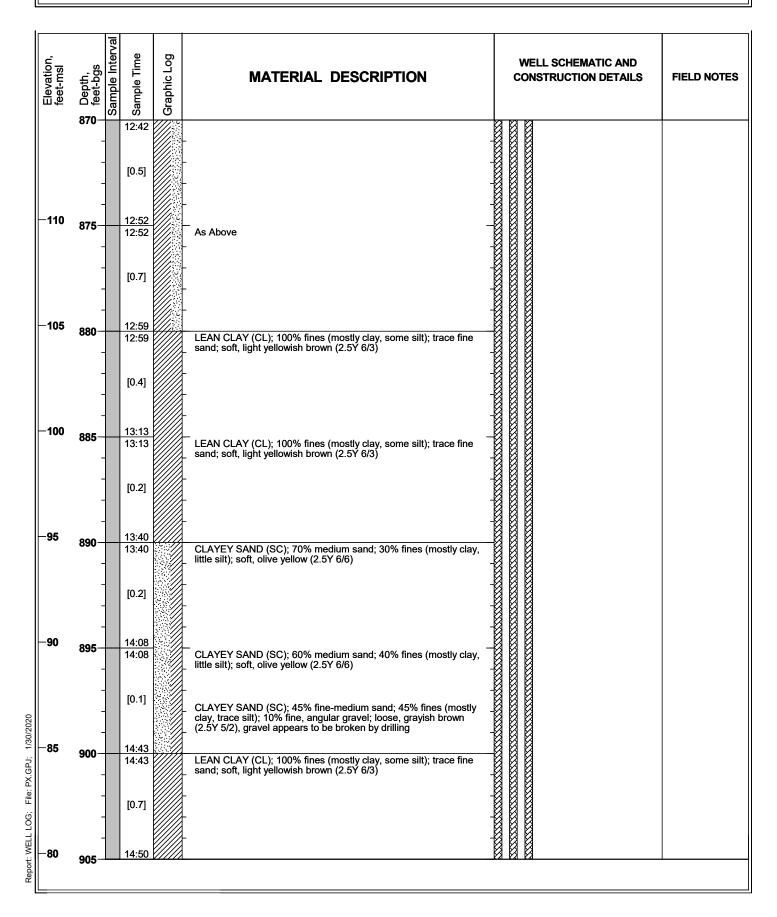


**Project Number:** 007-018-762 **Client:** 

**Chino Basin Watermaster** 

#### **Boring Log / PX2**

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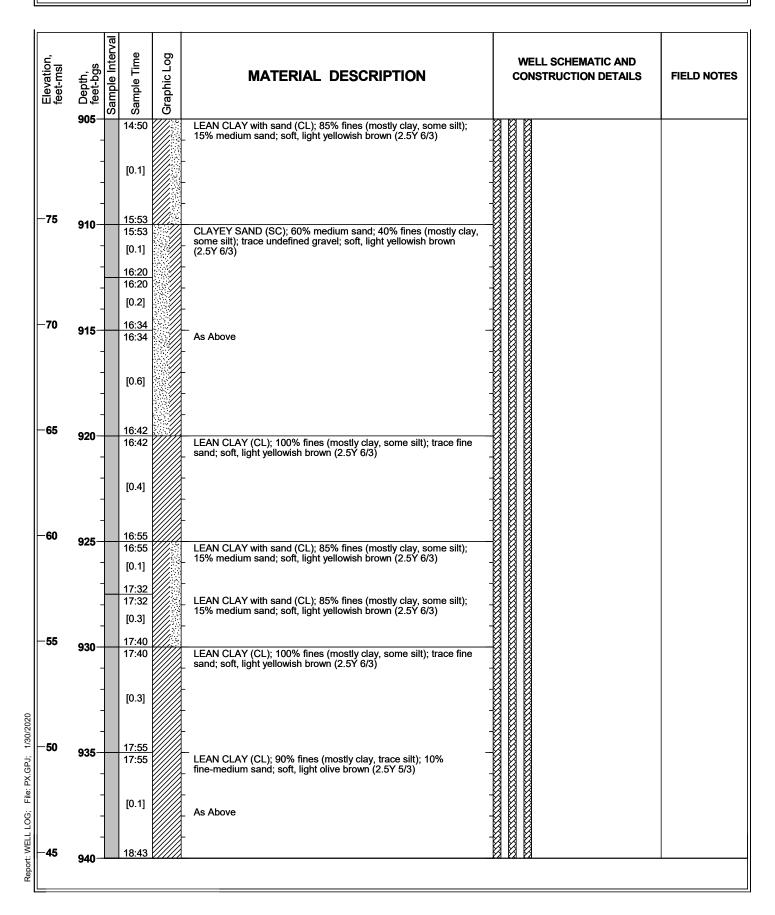


**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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Project Name:
Project Location:
Project Number:
Client:

Pomona Extensometer Facility
Montvue Park - Pomona, CA
007-018-762
Chino Basin Watermaster

## **Boring Log / PX2**

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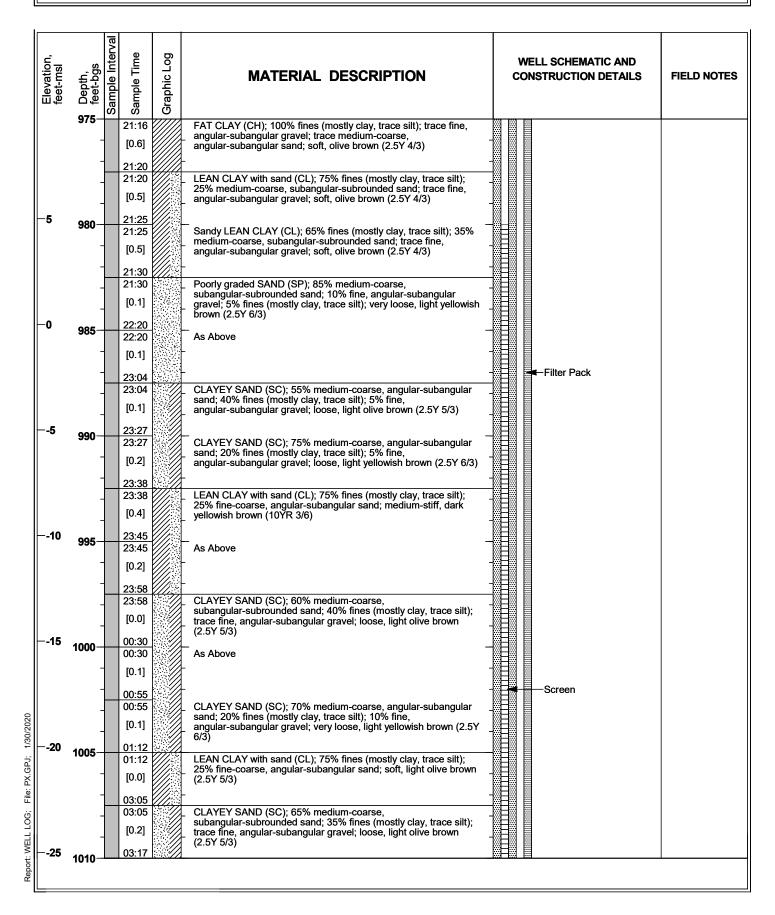
Elevation, feet-msl	Depth, feet-bgs	Sample Interval	Sample Time	Graphic Log	MATERIAL DESCRIPTION	WELL SCHEMATIC AND CONSTRUCTION DETAILS	FIELD NOTES
	- -		18:43 [0.4] 18:50		Sandy LEAN CLAY (CL); 60% fines (mostly clay, trace silt); 40% fine-coarse, subangular-subrounded sand; soft, light olive brown (2.5Y 5/3)		
-40	-		18:50 [0.3] 18:58		FAT CLAY (CH); 100% fines (mostly clay); soft, light olive brown (2.5Y 5/3)		
40	945— - -		18:58 [0.1]		LEAN CLAY (CL); 100% fines (mostly clay); trace medium-coarse sand; soft, light olive brown (2.5Y 5/3)		
	-		19:20 19:20 [0.3]		LEAN CLAY (CL); 90% fines (mostly clay); 10% fine-medium sand; soft, light olive brown (2.5Y 5/3)		
-35	950— - -		19:29 19:29 [0.2]		LEAN CLAY with sand (CL); 80% fines (mostly clay); 20% fine-medium sand; medium-stiff, light olive brown (2.5Y 5/3)		
	-		19:40 19:40 [0.3]		LEAN CLAY (CL); 95% fines (mostly clay); 5% fine-medium sand; _medium-stiff, light olive brown (2.5Y 5/3)		
-30	955— -		19:48 19:48 [0.3]		As Above		
	-		19:58 19:58 [0.1]		LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt); 20% fine-medium sand; medium-stiff, light olive brown (2.5Y 5/3), contains think pockets of fine-grained sand		
-25	960-		20:16 20:16 [0.2]		As Above		
	-		20:28 20:28 [0.3]		LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt); 20% fine-coarse, subangular-subrounded sand; medium-stiff, olive brown (2.5Y 4/3)		
-20	965— -		20:36 20:36 [0.1]		LEAN CLAY (CL); 90% fines (mostly clay, trace silt); 10% fine-coarse, subangular-subrounded sand; stiff, olive brown (2.5Y _4/3)	■ Transition Bentonite Seal	
	-		20:53 20:53 [0.4]		LEAN CLAY with sand (CL); 80% fines (mostly clay, trace silt); 20% fine-coarse, subangular-subrounded sand; medium-stiff, olive brown (2.5Y 4/3)		
15	970— -		21:00 21:00 [0.5]		fine-medium sand; soft, light olive brown (2.5Y 5/3)		
	-		21:05 21:05 [0.2]		LEAN CLAY with sand (CL); 75% fines (mostly clay, trace silt); 25% medium-coarse, subangular-subrounded sand; trace fine, angular-subangular gravel; soft, olive brown (2.5Y 4/3)	■ Transition Sand Seal	
-10	975-		21:16				

**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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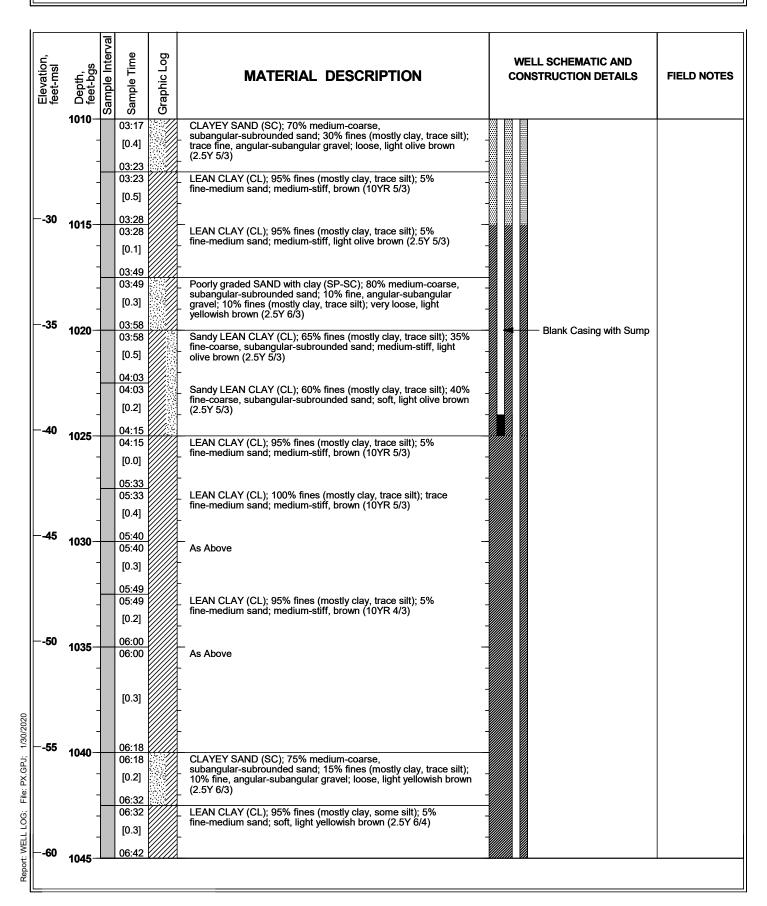


**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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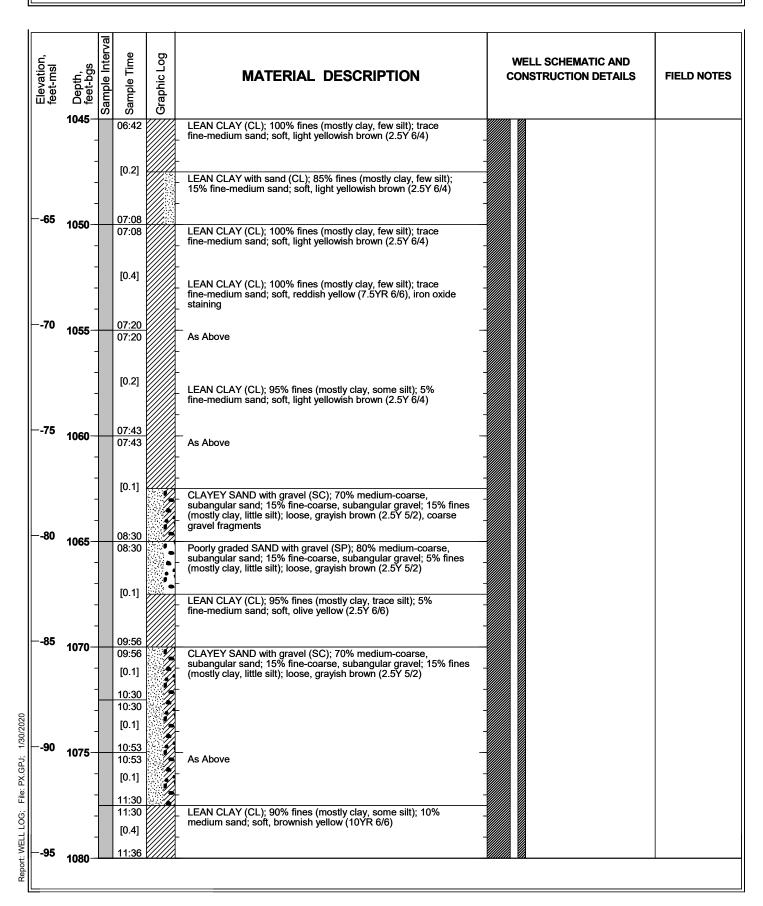


**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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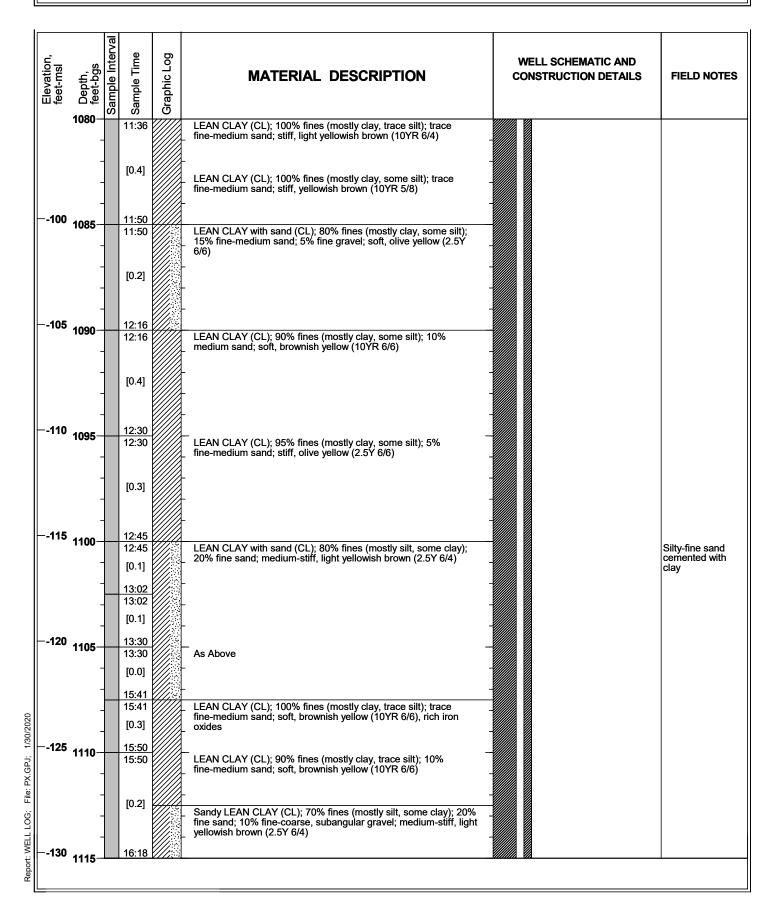


**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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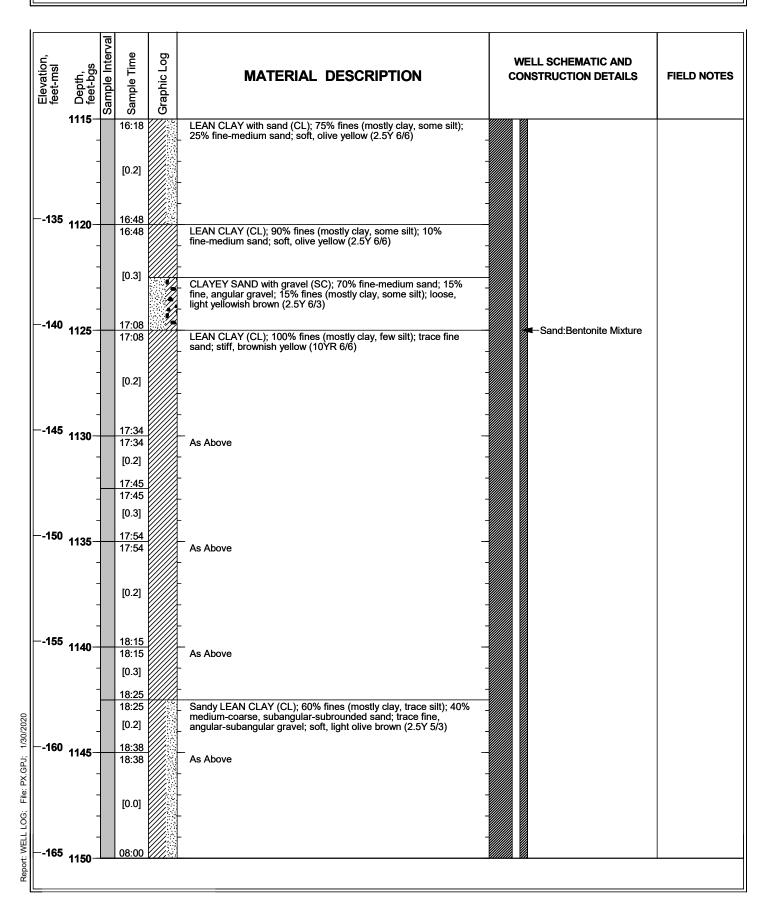


Project Location: Montvue Park - Pomona, Project Number: 007-018-762

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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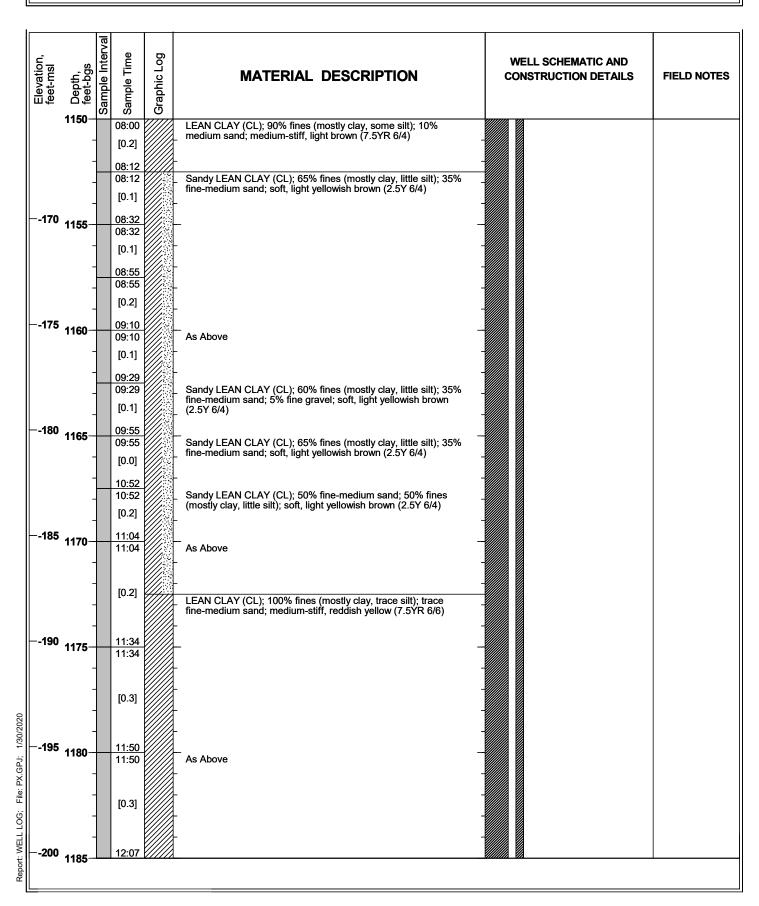


Project Location: Montvue Park - Pomona, Project Number: 007-018-762

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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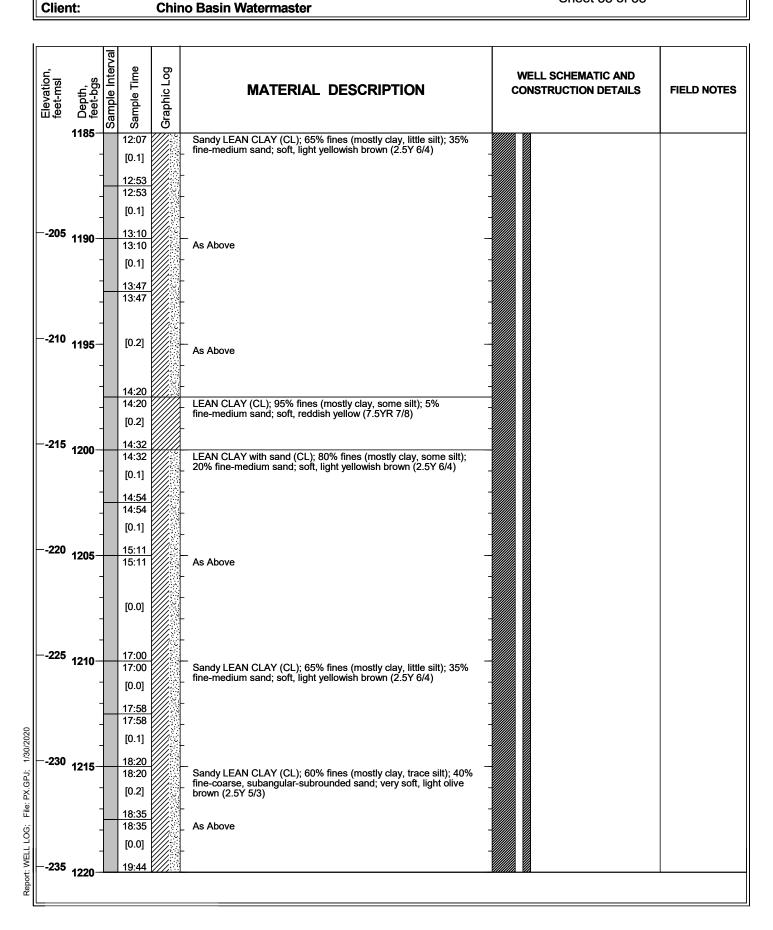


**Project Number:** 007-018-762

**Chino Basin Watermaster** 

#### **Boring Log / PX2**

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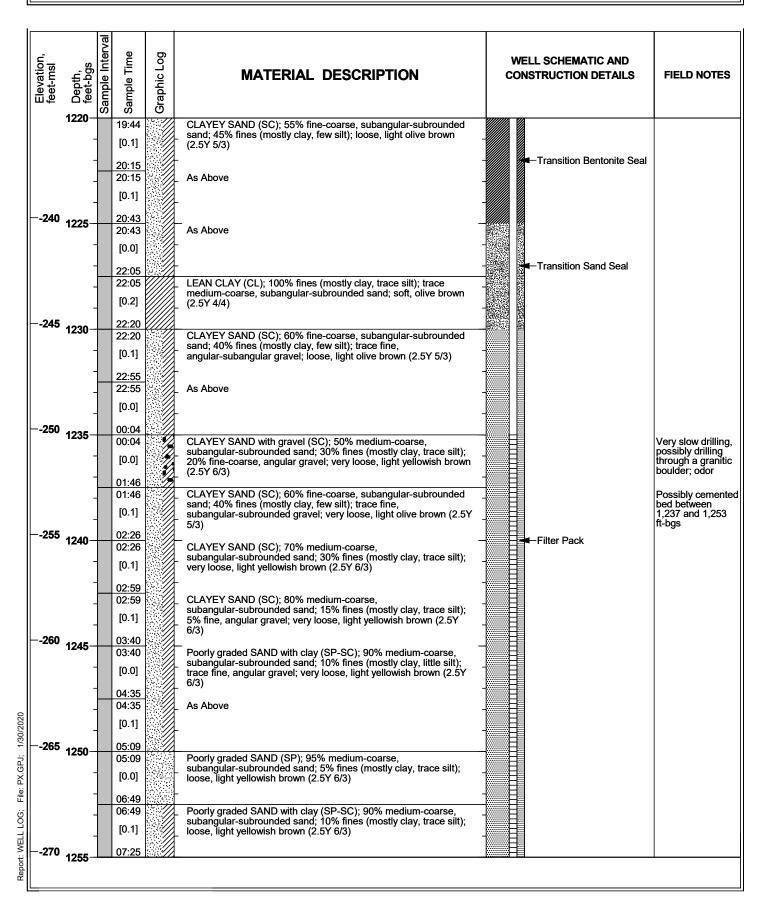


**Project Number: 007-018-762** 

Client: Chino Basin Watermaster

#### **Boring Log / PX2**

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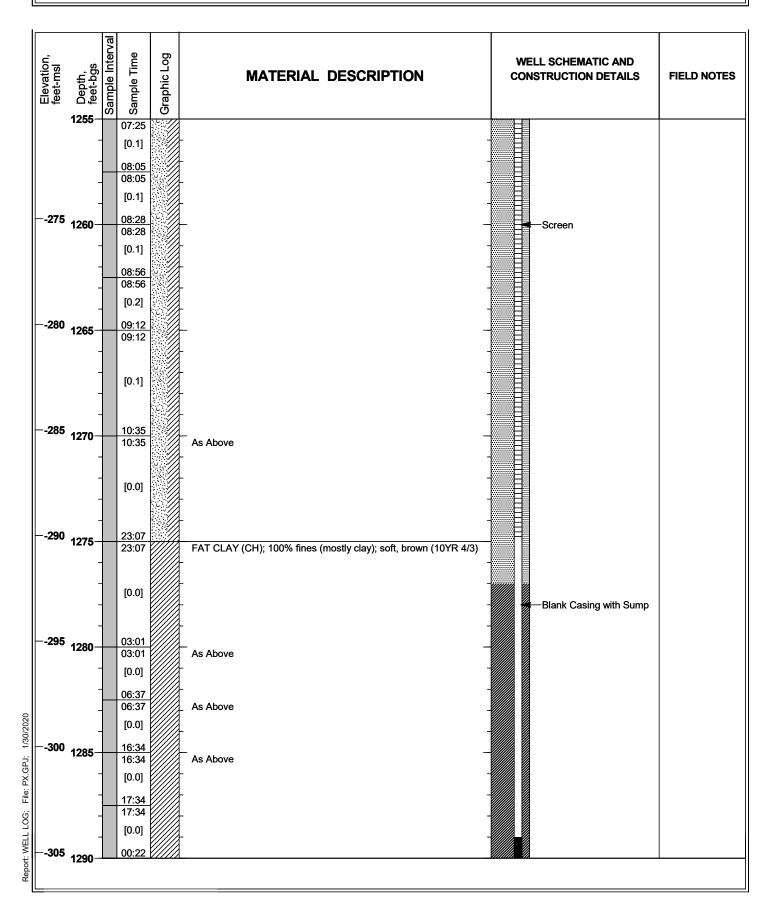


Project Location: Montvue Park - Pomona, CA Project Number: 007-018-762

Client: Chino Basin Watermaster

## **Boring Log / PX2**

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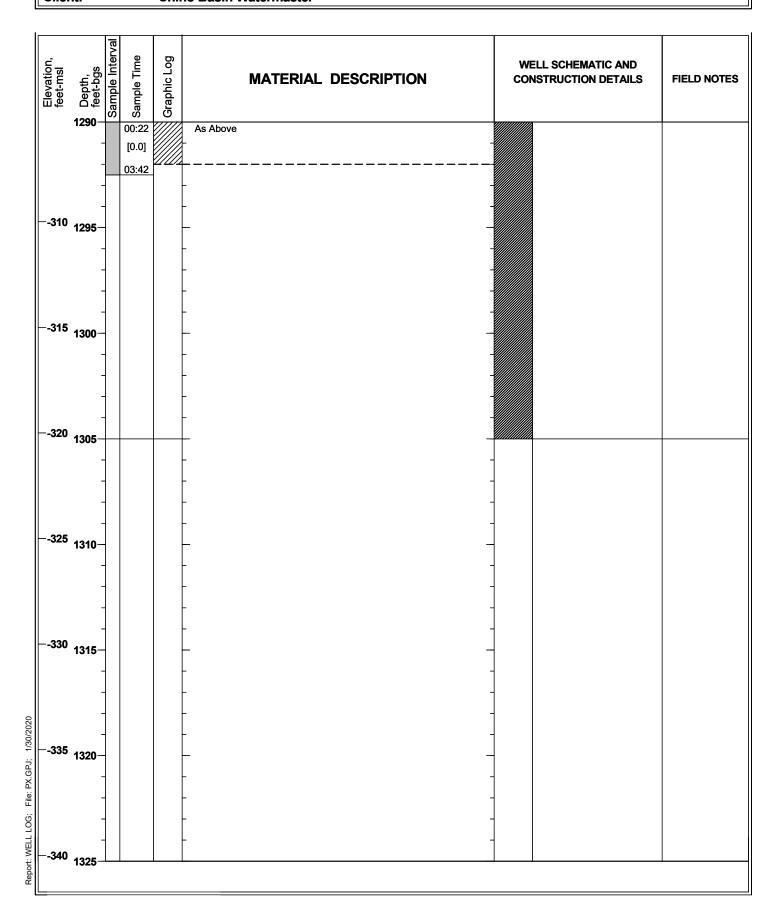
Project Name: Pomona Extensometer Facili Project Location: Montvue Park - Pomona, CA Pomona Extensometer Facility

007-018-762

**Project Number:** Client: **Chino Basin Watermaster** 

## **Boring Log / PX2**

Sheet 38 of 38



# CDM

Camp Dresser & McKee, Inc. 18881 Von Karman Avenue, Suite 650 Irvine, CA 92612 (949) 752-5452

## **BORING/WELL CONSTRUCTION LOG**

PAGE 1 OF 39

PROJ LOCA DRILL SAME GROU TOP ( LOGG REMA	ECT NATION LING MIPLING M JND EL DF CAS GED BY ARKS	Moi	Montclair FON Hoffn	nte , CA leve Gra	0-2196 Vista W	6-WEL /ater D culation	istrict n William	illLL	BORING/WELL NUMBER Well #3  DATE DRILLED 1/25/01-2/23/01  CASING TYPE/DIAMETER 3/8" C  SCREEN TYPE/SLOT Ful Flo Shi  GRAVEL PACK TYPE Colorado S  GROUT TYPE/QUANTITY 10.3-9  DEPTH TO WATER (feet bgs) 540  GROUND WATER ELEVATION	EB Steel utter/0.07 Silica 6 x sack slur	70" 16 ny / 55 yds³
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHO	LOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
			V			SM		poorly graded sand, f sphericity; 20% silt in to coarse, subangula 10% cobbles, 12-inch	ark grayish brown (10YR3/2); 60% ine, angular to rounded, low to high matrix; 10% well graded gravel, fine to subrounded, moderate sphericity; maximum diameter, subangular to	0.5	
					5	SP		POORLY GRADED S fine to medium, trace to moderate sphericit coarse, subangular to sphericity: 10% cobbl	e sphericity; slightly moist.  AND: brown (10YR4/3); 80% sand, coarse, angular to subrounded, low y; 10% well graded gravel, fine to subrounded, low to moderate es, 12-inch maximum diameter, nded, moderate sphericity; slightly		18" x 3/8" CB Steel Blank (0 584.77 ft bgs)
					 15  	SM		poorly graded sand, f moderate sphericity;	ellowish brown (10YR4/4); 70% ine, subangular to subrounded, 20% silt in matrix; 10% cobbles, meter, subangular to subrounded, slightly moist.	_ 13.0	
					-20-  			SII TV SANDI, dark v	ellowish brown (10YR4/4); 70%	23.0	10.3-sack sar slurry (2 - 530 bgs)
					 -25-  	SM		poorly graded sand, f moderate sphericity; 12-inch maximum dia moderate sphericity;	ine, subangular to subrounded, 20% silt in matrix; 10% cobbles, Imeter, subangular to subrounded,		



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

								Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WE	ELL DIAGRAM
						SM		SILTY SAND: dark yellowish brown (10YR4/4); 70% poorly graded sand, fine, subangular to subrounded, moderate sphericity; 20% silt in matrix; 10% cobbles, 12-inch maximum diameter, subangular to subrounded, moderate sphericity; slightly moist.  POORLY GRADED SAND: brown (7.5YR4/4); 80% sand, fine to medium, trace coarse, subangular to subrounded, moderate sphericity; 20% cobbles, 12-inch maximum diameter, subangular to subrounded, low to moderate sphericity; trace poorly graded gravel, fine, 1/2-inch maximum diameter, angular to subrounded, low sphericity; slightly moist.	33.0		18" x 3/8" CB Steel Blank (0 584.77 ft bgs)
					 -45-  	SP		POORLY GRADED SAND: brown (7.5YR4/4); 80% sand, fine to medium, trace coarse, subangular to subrounded, moderate sphericity; 20% cobbles, 12-inch maximum diameter, subangular to subrounded, low to moderate sphericity; trace poorly graded gravel, fine, 1/2-inch maximum diameter, angular to subrounded, low sphericity; slightly moist.	45.0		-10.3-sack san slurry (2 - 530 bgs)
					50   55	SP	0 0	POORLY GRADED SAND WITH GRAVEL: brown (10YR5/4); 90% sand, fine to medium; 10% poorly graded gravel, fine, trace coarse, angular to subangular; trace silt.	51.0		-34" Mild Stee Conductor (0-51 ft bgs)
					  - 60 		0 0 0 0 0	POORLY GRADED SAND WITH GRAVEL: brown (10YR5/4); 90% sand, fine to medium; 10% poorly graded gravel, fine, trace coarse, angular to subangular; trace silt.	60.0		



## **BORING/WELL CONSTRUCTION LOG**

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
ā.	-0	RE ()	SA	ш	-65-   	SP	© 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	POORLY GRADED SAND WITH GRAVEL: brown	70.0	18" x 3/8" CB Steel Blank (
					   75 	SP	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(10YR5/4); 90% sand, fine to medium; 10% poorly graded gravel, fine, trace coarse, angular to subangular; trace silt.		584.77 ft bgs
						SW	0 2 3 4 4 9	WELL GRADED SAND WITH GRAVEL: brown (10YR5/4); 80% sand, fine to coarse, 20% well graded gravel, fine to coarse.	_ 80.0	10.3-sack sa slurry (2 - 53 bgs)
						SW	0	WELL GRADED SAND WITH GRAVEL: brown (10YR5/4); 80% sand, fine to coarse, 20% well graded gravel, fine to coarse.	90.0	



#### **BORING/WELL CONSTRUCTION LOG**

10490-21966-WELL28.DRILL

Monte Vista Water District

**BORING/WELL NUMBER** 

Well #28

DATE DRILLED 1/25/01-2/23/01

**PROJECT NAME** Continued from Previous Page RECOVERY (inches) SAMPLE ID. PID (ppm) GRAPHIC LOG CONTACT BLOW EXTENT DEPTH (ft. BGL) U.S.C.S. LITHOLOGIC DESCRIPTION WELL DIAGRAM 100.0 SILTY SAND: yellowish brown (10YR5/6); 85% sand, fine to medium; 15% silt; trace poorly graded gravel, fine, subangular to subrounded. 18" x 3/8" CB Steel Blank (0 SM 584.77 ft bgs) 110.0 SILTY SAND: yellowish brown (10YR5/6); 85% sand, fine to medium; 15% silt; trace poorly graded gravel, fine, subangular to subrounded. 10.3-sack sand SM slurry (2 - 530 ft bgs) 120.0 120 SILTY SAND: yellowish brown (10YR5/6); 85% sand, fine to medium; 15% silt; trace poorly graded gravel, fine, subangular to subrounded. SM 123.0 POORLY GRADED SAND: yellowish brown (10YR5/6); 90% sand fine to medium; 5% poorly graded gravel, fine, subangular to subrounded; 5% silt. 125 NEWGINT MVWD.GPJ NEWGINT.GDT 4/3/01 SP 130 Continued Next Page PAGE 4 OF 39



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

DATE DRILLED 1/25/01-2/23/01

				,				Continued from Previous Page	1		
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEL	L DIAGRAM
					 - 135- 	SP		POORLY GRADED SAND: yellowish brown (10YR5/6); 90% sand fine to medium; 5% poorly graded gravel, fine, subangular to subrounded; 5% silt.	133.0		
					  -140 	sw		WELL GRADED SAND WITH GRAVEL: brown (10YR5/4); 90% sand, fine to coarse, 10% well graded gravel, fine to coarse; subangular to subrounded.	137.0		─18" x 3/8" CB Steel Blank (0 584.77 ft bgs)
					145-    -150-	gw		WELL GRADED GRAVEL WITH SAND: grayish brown (10YR5/2); 60% gravel, fine to coarse, subrounded; 40% poorly graded sand, medium to coarse.			<b>4</b> -10.3-sack sar slurry (2 - 530 bgs)
					  -15 <del>5 -</del> 	GW		WELL GRADED GRAVEL WITH SAND: grayish brown (10YR5/2); 60% gravel, fine to coarse, subrounded; 40% poorly graded sand, medium to coarse.	154.0		
					-160    -165		30000000000000000000000000000000000000	WELL GRADED GRAVEL WITH SAND: grayish brown (10YR5/2); 60% gravel, fine to coarse, subrounded; 40% poorly graded sand, medium to coarse.	164.0		



#### **BORING/WELL CONSTRUCTION LOG**

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

		, 1						Continued from Previous Page	T		
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WE	LL DIAGRAM
					 170  	GW			174.0		
						GW		WELL GRADED GRAVEL WITH SAND: grayish brown (10YR5/2); 60% gravel, fine to coarse, subrounded; 40% poorly graded sand, medium to coarse.			18" x 3/8" CB Steel Blank (0 584.77 ft bgs)
					   -185- 	SP		POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 90% sand, fine to medium, some coarse; 10% poorly graded gravel, coarse, subangular to subrounded.	_ 181.0		-10.3-sack sar slurry (2 - 530 bgs)
					 190-  		0	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 90% sand, fine to medium, some coarse (increasing downward); 10% poorly graded gravel, coarse, subangular to subrounded.	190.0		
					-195-    -200-	SP	0 0 0	POORLY GRADED SAND WITH GRAVEL: pale brown (10YR6/3); 90% sand, medium to coarse; 10% well	200.0		



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER Well #28

							, ,	Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELI	L DIAGRAM
						SP SP SM		POORLY GRADED SAND WITH SILT AND GRAVEL: dark yellowish brown (10YR4/4); 80% sand, fine to medium; 10% well graded gravel, fine to coarse, subrounded; 10% silt as oxidized balls with gravel.	210.0		–18" x 3/8" CB Steel Blank (i 584.77 ft bgs
						SP		POORLY GRADED SAND WITH GRAVEL: light yellowish brown (10YR6/4); 80% sand, medium to coarse; 15% well graded gravel, fine to coarse; 5% silt.	220.0		€10.3-sack sa slurry (2 - 53 bgs)
						SP	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	POORLY GRADED SAND WITH SILT AND GRAVEL: dark yellowish brown (10YR4/4); 80% sand, fine to medium; 10% well graded gravel, fine to coarse, subrounded; 10% silt as oxidized balls with gravel.	230.0		



## **BORING/WELL CONSTRUCTION LOG**

	JECT N	UMBER AME	-		0-21966 /ista W		L28.DRI	BORING/WELL NUMBER   Well #	28		
								Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	W	ELL DIAGRAM
						SM	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WELL GRADED SAND WITH GRAVEL: pale brown (10YR6/3); 80% sand, fine to coarse, 20% well graded gravel, fine to coarse; subangular to subrounded; trace cobbles.	240.0		18" x 3/8" CE Steel Blank ( 584.77 ft bgs
						sw	В. () () () () () () () () () ()	WELL GRADED SAND WITH GRAVEL: pale brown (10YR6/3); 80% sand, fine to coarse, 20% well graded gravel, fine to coarse; subangular to subrounded; trace cobbles; coarsening downward.	249.0		-10.3-sack sa
					-255  260 		5	WELL GRADED SAND WITH GRAVEL: pale brown (10YR6/3); 80% sand, fine to coarse, 20% well graded gravel, fine to coarse; subangular to subrounded.	260.0		10.3-sack sa slurry (2 - 53 bgs)
					_265 _	SW		Continued Next Page	270.0		PAGE 8 OF



## **BORING/WELL CONSTRUCTION LOG**

10490-21966-WELL28.DRILL

**BORING/WELL NUMBER** 

Well #28

DATE DRILLED Monte Vista Water District 1/25/01-2/23/01 **PROJECT NAME** Continued from Previous Page RECOVERY (inches) SAMPLE ID. GRAPHIC LOG CONTACT BLOW PID (ppm) EXTENT DEPTH (ft. BGL) U.S.C.S. WELL DIAGRAM LITHOLOGIC DESCRIPTION WELL GRADED SAND WITH GRAVEL: pale brown (10YR6/3); 80% sand, fine to coarse, 20% well graded gravel, fine to coarse; subangular to subrounded. SW 280.0 18" x 3/8" CB 280 WELL GRADED SAND WITH SILT AND GRAVEL: Steel Blank (0 yellowish brown (10YR5/4); 70% sand, fine to coarse; 584.77 ft bgs) 20% well graded gravel, fine to coarse; 10% silt; trace 285 SW SM 290.0 10.3-sack sand slurry (2 - 530 ft 290 CLAYEY SILT: strong brown (7.5YR5/6); 70% silt, inelastic, soft; 20% clay, nonplastic, soft; 10% poorly bgs) graded sand, fine to medium. 295 ML NEWGINT MVWD.GPJ NEWGINT.GDT 300.0 300 SANDY SILT WITH CLAY: yellowish brown (10YR5/8); 60% silt, inelastic, soft; 30% poorly graded sand, medium; 10% clay, nonplastic, soft. Continued Next Page PAGE 9 OF 39



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER 10490-21966-WELL28.DRILL

BORING/WELL NUMBER

								Continued from Previous Page	-		
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WE	LL DIAGRAM
Δ.		ar a	<b>VS</b>		305 	ML SW		WELL GRADED SAND WITH GRAVEL: light yellowish brown 910YR6/4); 70% sand, fine to coarse; 25% poorly graded gravel, fine, trace coarse, subrounded; 5% silt.  SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/6); 75% sand, fine to coarse; 15% silt; 10% well graded gravel, fine to coarse, subangular to subrounded; trace clay.  SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/6); 75% sand, fine to coarse; 15% silt; 10% well graded gravel, fine to coarse, subangular to subrounded; trace clay.	310.0		18" x 3/8" CB Steel Blank (0 584.77 ft bgs)



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER Well #28

DATE DRILLED 1/25/01-2/23/01

								Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	W	ELL DIAGRAM
						SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/6); 75% sand, fine to coarse; 15% silt; 10% well graded gravel, fine to coarse, subangular to subrounded; trace clay.	340.0		-18" x 3/8" CB Steel Blank (0
						SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/6); 80% sand, fine to coarse; 10% silt; 10% well graded gravel, fine to coarse, subangular to subrounded; trace clay.	350.0		584.77 ft bgs)
		*						WELL GRADED SAND WITH SILT AND GRAVEL: brownish yellow (10YR6/6); 75% sand, fine to coarse; 15% well graded gravel, fine to coarse, subangular to subrounded; 10% silt; trace clay.	360.0		slurry (2 - 530 bgs)
					365   - 370 	SW		WELL GRADED SAND WITH GRAVEL: pale brown (10YR6/3); 80% sand, fine to coarse; 20% well graded gravel, fine to coarse, subangular to subrounded.  Continued Next Page	_ 370.0		



## **BORING/WELL CONSTRUCTION LOG**

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PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

**PROJECT NAME** 

Monte Vista Water District DATE DRILLED 1/25/01-2/23/01 Continued from Previous Page RECOVERY (inches) SAMPLE ID. PID (ppm) GRAPHIC CONTACT BLOW U.S.C.S. EXTENT DEPTH (ft. BGL) LITHOLOGIC DESCRIPTION WELL DIAGRAM SW 380.0 18" x 3/8" CB 380 WELL GRADED SAND WITH GRAVEL: pale brown Steel Blank (0 (10YR6/3); 80% sand, fine to coarse; 20% well graded 584.77 ft bgs) gravel, fine to coarse, subangular to subrounded. SW 390.0 10.3-sack sand WELL GRADED SAND WITH SILT AND GRAVEL: light yellowish brown (10YR6/4); 70% sand, fine to coarse; slurry (2 - 530 ft bgs) 20% well graded gravel, fine to coarse; 10% silt as balls, yellowish brown; trace clay. SW SM 395 400.0 400 SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/6); 50% sand, fine to coarse; 35% silt, inelastic; 10% poorly graded gravel, subrounded; 5% clay. SM Continued Next Page



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

							, ,	Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WE	LL DIAGRAM
					 - 410    	SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/8); 50% sand, fine to coarse; 35% silt, inelastic; 10% poorly graded gravel, subrounded; 5% clay.	410.0		18" x 3/8" CB Steel Blank (0
						SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/8); 50% sand, fine to coarse; 35% silt, inelastic; 10% poorly graded gravel, subrounded; 5% clay.	420.0		584.77 ft bgs)
					   - 430 	SM	9 9 9 1 1 1	SILTY SAND WITH GRAVEL: brownish yellow (10YR 6/8); 50% sand, fine to coarse; 35% silt, inelastic; 10% poorly graded gravel, subrounded; 5% clay.	430.0		slurry (2 - 530 bgs)
					435    440			CLAYEY SILT WITH SAND: yellowish red (5YR5/6); 70% silt, moderately elastic, medium stiffness; 20% poorly graded sand, fine to medium; 10% clay, moderately plastic, medium stiffness.	436.0		



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER 10490-21966-WELL28.DRILL

BORING/WELL NUMBER

-			, ,			Continued from Previous Page	-	
PID (ppm) BLOW COUNTS	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
				445 - 445 - 450 - 455 - 460 - 465 - 470 - 475	ML ML	CLAYEY SILT WITH SAND AND GRAVEL: yellow (5YR4/6); 60% silt, dark reddish brown (5YR3/4), or 20% poorly graded sand, fine to medium; 15% poor graded gravel, fine, subrounded; 5% clay.  CLAYEY SILT WITH SAND AND GRAVEL: yellow (5YR4/6); 60% silt, dark reddish brown (5YR3/4), or 20% poorly graded sand, fine to medium; 15% poor graded gravel, fine, subrounded; 5% clay.  CLAYEY SILT WITH SAND: yellowish brown (10Y 70% silt, inelastic, soft; 20% poorly graded sand, m subrounded; 10% clay, nonplastic, soft.	458.0 dized; y 458.0 dized; y 465.0 dium, 474.0	18" x 3/8" CE Steel Blank ( 584.77 ft bgs 10.3-sack sa slurry (2 - 53) bgs)



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

DATE DRILLED 1/25/01-2/23/01



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

Monte Vista Water District

BORING/WELL NUMBER Well #28

DATE DRILLED 1/25/01-2/23/01

PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEI	L DIAGRAM
					  - 515- 	CL		CLAY: yellowish brown (10YR5/8); 100% clay, nonplastic, soft to medium stiff; trace sand.	516.0		—18" x 3/8" CB Steel Blank (0 584.77 ft bgs)
						CL		CLAY: yellowish brown (10YR5/8); 90% clay, nonplastic, very soft to soft; 10% sand.	523.0		-10.3-sack sand slurry (2 - 530 bgs)
					 -530-   -535- 	CL		CLAY: yellowish brown (10YR5/8); 95% clay, nonplastic, stiff to very stiff; 5% sand.	533.0		Colorado Silica 6 x 16 Gravel Pack (530 - 1265 ft bgs)
					540 	SM		SILTY SAND: yellowish brown (10YR5/8); 80% well graded sand, fine to coarse, angular to subrounded, low sphericity; 20% silt.	_ 540.0	¥	4-4" CB Steel, Permanent Gravel Feed Tube (0-540 ft bgs)



#### **BORING/WELL CONSTRUCTION LOG**

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

PROJECT NAME	Monte Vista Water District	DATE DRILLED 1/25/01-2/23/01	
		Continued from Previous Page	
PID (ppm) BLOW COUNTS RECOVERY (inches)	SAMPLE ID.  EXTENT DEPTH (ft. BGL) U.S.C.S. GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT OEPTH MEND DIAGRAM
	-545 SM 2	SILTY SAND WITH GRAVEL: yellowish brown (10YR5/8); 60% sand, coarse, angular to subrounded, low sphericity; 20% silt; 20% gravel, angular to subrounded, low sphericity.	545.0  18" x 3/8" CF Steel Blank ( 584.77 ft bgs
	-555 GM	SILTY GRAVEL WITH SAND: yellowish brown (10YR5/8); 50% poorly graded gravel, fine, angular to subrounded, low sphericity; 30% poorly graded sand, coarse, angular to subrounded, low sphericity; 20% silt.	_ 553.0 584.77 it ugs
	-560	SILTY SAND WITH GRAVEL: yellowish brown (10YR5/8); 60% poorly graded sand, coarse, angular to subrounded, low sphericity; 20% silt; 20% gravel, angular to subrounded, low sphericity.	557.0 Colorado Sil 6 x 16 Grave Pack (530 - 1265 ft bgs)
	CL	CLAY: yellowish brown (10YR5/8); 95% clay, nonplastic, stiff to very stiff; 5% sand.	_ 568.0
	; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	SILTY SAND WITH GRAVEL: yellowish brown (10YR5/8); 65% poorly graded sand, coarse, angular to subrounded, low sphericity; 20% silt; 15% gravel, angular to subrounded, low sphericity.  Continued Next Page	_ 576.0



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER 10490-21966-WELL28.DRILL BORING/WELL NUMBER

PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
		Œ.	0)		580-	SM	o			18" x 3/8" CB
						CL		CLAY: brownish yellow (10YR6/8); 85% clay; 10% poorly graded sand, medium to coarse; 5% poorly graded gravel, fine, subangular to subrounded.	581.0	584.77 ft bgs
					 -585 			WELL GRADED GRAVEL WITH SAND AND SILT: brownish yellow (10YR6/6); 60% gravel, fine to coarse, angular to subrounded; 30% poorly graded sand, medium to coarse; 10% silt.	_ 584.0	
					 -590- 	GW GM				18" x 3/8" CE Steel Blank V 2" Sounding Tube Splice (584.77 - 622.92 ft bgs
				-	 -595  			WELL GRADED GRAVEL WITH SAND: brownish yellow (10YR6/6); 60% gravel, fine to coarse, angular to subrounded; 30% poorly graded sand, medium to coarse; 5% silt.	_ 594.0	
					 -600-  					Colorado Silli 6 x 16 Grave Pack (530 - 1265 ft bgs)
					-605  	ML		SILT WITH SAND AND GRAVEL: yellowish brown (10YR5/6); 50% silt; 25% well graded gravel and rock fragments, fine to coarse, angular to subrounded; 25% poorly graded sand, medium to coarse, angular to subrounded.	_ 606.0	
					610-	SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR6/6); 60% poorly graded sand, medium to coarse; 20% well graded gravel and rock fragments, fine to coarse; 20% silt.  SILT WITH SAND: yellowish brown (10YR5/4); 85% silt	611.0	



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER Well #28

			Continued from Previous Page					
		T	Continued from Previous Page					
PID (ppm) BLOW COUNTS HECOVERY (inches)	SAMPLE ID. EXTENT DEPTH (ft. BGL)	U.S.C.S. GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM			
		ML	POORLY GRADED SAND: yellowish brown (10YR5/4); 100% sand, medium to coarse, some fine, angular to subangular, low sphericity.	621.0	18" x 3/8" CB Steel Blank W 2" Sounding Tube Splice (584.77 - 622.92 ft bgs)  Splice Openir (616.12 - 619.22 ft bgs)			
		SP SP SM	POORLY GRADED SAND WITH SILT: yellowish brown (10YR5/4); 90% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff, sand in matrix.	_ 628.0	Mechanical Coupling (622.92 - 625.02 ft bgs  18" x 5/16" 3 SS Blank (625.02 - 635 bgs)			
	 - 635- 	ML	SANDY SILT: yellowish brown (10YR5/4); 70% silt as balls, inelastic, soft to medium stiff; 30% poorly graded sand, medium to coarse, angular to subangular.	634.0	18" x 5/16" 3 SS, 0.070" Ful-Flo (635 750.15 ft bgs			
	 -640  	SM	SILTY SAND: yellowish brown (10YR5/4); 80% poorly graded sand, medium to coarse, angular to subangular; 20% silt as balls, inelastic, soft to medium stiff.	_ 640.0				
	 -645- 		POORLY GRADED SAND: yellowish brown (10YR5/4); 90% poorly graded sand, medium to coarse, angular to subangular; 5% silt as balls, inelastic, soft to medium stiff; 5% poorly graded gravel, fine, 3/4-inch maximum diameter, angular to subrounded, low sphericity.	644.0	6 x 16 Grave Pack (530 - 1265 ft bgs)			



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

								Continued from Previous Page	_		
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAG	GRAM
						SP		POORLY GRADED SAND WITH SILT: yellowish brown (10YR5/4); 90% poorly graded sand, medium to coarse, angular to subangular; 10% silt as balls, inelastic, soft to medium stiff.	654.0	SS, Ful-I	k 5/16" 3 0.070" 15 (635 - 15 ft bgs
					-660   -665 	SM		POORLY GRADED SAND WITH SILT: yellowish brown (10YR5/4); 85% poorly graded sand, medium to coarse, angular to subangular; 10% silt as balls, inelastic, soft to medium stiff; 5% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subrounded, low sphericity.	664.0	6 x 1	orado Sili 6 Grave k (530 - 5 ft bgs)
					-670-    -675-	SM		POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 85% sand, medium to coarse; 10% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	_ 674.0		
					  -680	SP	0.0.0				



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								Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELI	_ DIAGRAM
						SP		POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 80% sand, medium to coarse; 15% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	686.0		–18" x 5/16" 3 SS, 0.070" Ful-Flo (635 750.15 ft bgs
						SP	000000000000000000000000000000000000000	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 80% sand, medium to coarse; 15% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	696.0		►Colorado Sil 6 x 16 Grave Pack (530 -
					   -705-	CL	0	CLAY WITH SAND: yellowish brown (10YR5/4); 85% clay as balls, nonplastic, soft to medium stiff; 15% well graded sand, fine to coarse, angular to subangular, low sphericity.	702.0		1265 ft bgs)
					 710-   715-	SP	0 0 0	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 80% sand, medium to coarse; 15% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	_ 707.0		
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10490-21966-WELL28.DRILL

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PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAN	М
					   - 720- 	SP	0. 9. 0. 0.	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 80% sand, medium to coarse; 15% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	717.0		
					725   730 	SP	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/4); 80% sand, medium to coarse; 15% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	727.0	18" x 5/16 SS, 0.070 Ful-Flo (6 750.15 ft	0" 535 -
						SP		POORLY GRADED SAND WITH GRAVEL: light yellowish brown (10YR6/4); 70% sand, medium to coarse, angular to subangular, low sphericity; 25% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	735.0	Colorado 6 x 16 Gr Pack (530 1265 ft bo	ravel 0 -
								POORLY GRADED SAND WITH GRAVEL: light yellowish brown (10YR6/4); 60% sand, medium to coarse, angular to subangular, low sphericity; 30% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls.	745.0		
					<del>-7</del> 50-	SP		Continued Next Page			



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

		, 1						Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEL	L DIAGRAM
						SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR6/6); 40% poorly graded sand, fine to medium, angular to subangular; 40% silt as balls; 20% poorly graded gravel, fine, subrounded.	754.0		18" x 5/16" ; SS Blank (750.15 - 784.95 ft bgs
					 -765- 	ML		SILT WITH CLAY: yellowish brown (10YR5/4); 80% silt, moderately elastic, medium stiff; 15% clay, moderately plastic, medium stiff; 5% poorly graded sand, fine to medium.			
				-		SM		SILTY SAND WITH GRAVEL: yellowish brown (10YR5/6); 40% poorly graded sand, fine to medium, angular to subangular; 40% silt as balls, moderate to highly inelastic, medium stiff; 20% poorly graded gravel, fine, angular to subangular.	_ 768.0		Colorado Sil 6 x 16 Grave Pack (530 - 1265 ft bgs)
					   -780 	SM		SILTY SAND WITH GRAVEL: brownish yellow (10YR6/6); 60% poorly graded sand, fine to medium, angular to subangular; 30% silt as balls; 10% poorly graded gravel and rock fragments, fine, 1/4-inch maximum diameter, angular.	778.0		
				-	-	ML	18	CLAYEY SILT WITH SAND: light brownish yellow (10YR6/4); 60% silt as balls, inelastic, soft; 20% clay as Continued Next Page	783.0		



#### **BORING/WELL CONSTRUCTION LOG**

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PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

Monte Vista Water District DATE DRILLED 1/25/01-2/23/01 **PROJECT NAME** Continued from Previous Page RECOVERY (inches) SAMPLE ID. GRAPHIC CONTACT PID (ppm) BLOW EXTENT U.S.C.S. DEPTH (ft. BGL) LITHOLOGIC DESCRIPTION WELL DIAGRAM balls, nonplastic soft; 20% poorly graded sand, fine, some 785.0 medium.
SILTY CLAY: yellowish brown (10YR5/8); 60% clay, 785 moderately plastic, medium stiff; 35% silt, moderately elastic, medium stiff; 5% poorly graded sand, medium, some coarse, angular to subangular. 18" x 5/16" 304 790 SS, 0.070" 791.0 Ful-Flo (784.95 POORLY GRADED SAND WITH GRAVEL: light olive - 794.91 ft bgs) brown (2.5Y5/3); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 15% poorly graded gravel and rock fragments, fine, 1/2-inch maximum 0 diameter, angular to subangular, low sphericity. :0 795 SP .0. o 799.0 CLAY: yellowish brown (10YR5/8); 100% clay as balls, nonplastic, soft; trace poorly graded sand, medium to Colorado Silica 800 coarse, angular to subangular, low sphericity; trace silt in 6 x 16 Gravel clay matrix. Pack (530 -1265 ft bgs) CL 805 809.0 CLAY: light olive brown (2.5Y5/3); 90% clay as balls, nonplastic, soft; 10% well graded sand, fine to coarse, 18" x 5/16" 304 810 angular to subangular, low sphericity; trace silt in clay SS Blank (794.91 -854.91 ft bgs) NEWGINT MVWD.GPJ NEWGINT.GDT CL 815 Continued Next Page



# **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

PROJECT NAME

Monte Vista Water District

BORING/WELL NUMBER

Well #28

DATE DRILLED 1/25/01-2/23/01

	7							Continued from Previous Page	1	
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
					 -820- 			CLAY: light olive brown (2.5Y5/3); 90% clay as balls, nonplastic, soft; 10% well graded sand, fine to coarse, angular to subangular, low sphericity; trace silt in clay matrix.	819.0	
					 -825 	CL				18" x 5/16" 3 SS Blank (794.91 - 854.91 ft bgs)
					 -830- 			CLAY: light olive brown (2.5Y5/3); 90% clay as balls, nonplastic, soft; 10% well graded sand, fine to coarse, angular to subangular, low sphericity; trace silt in clay matrix.	829.0	
					 -835  	CL				Colorado Silli 6 x 16 Grave Pack (530 - 1265 ft bgs)
								CLAYEY SAND: yellowish brown (10YR5/8); 60% poorly graded sand, medium to coarse, some fine, angular to subangular, low sphericity; 35% clay as balls and coating gravel, nonplastic, soft to medium stiff; 5% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity.	_ 839.0	
					 -845  	sc				
					 -850- 	sc		CLAYEY SAND: yellowish brown (10YR5/8); 75% poorly graded sand, medium to coarse, some fine, angular to subangular, low sphericity; 20% clay as balls and coating gravel, nonplastic, stiff to very stiff; 5% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subangular, low sphericity.	849.0	
							111	Continued Next Page	4	1.1 1.1



# **BORING/WELL CONSTRUCTION LOG**

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Monte Vista Water District

BORING/WELL NUMBER

Well #28

DATE DRILLED 1/25/01-2/23/01

				П				Continued from Previous Page	T		
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEL	L DIAGRAM
					855   	CL		CLAY: light olive brown (2.5Y5/3); 90% clay as balls, nonplastic, soft; 10% well graded sand, fine to coarse, angular to subangular, low sphericity; trace silt in clay matrix.  POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/8); 85% sand, medium to coarse, angular to who provide the proportion of the provided graded gravely.	_ 855.0 _ 859.0		
					  - 865 	SP	0 0 0 0 0 0	to subangular, low sphericity; 10% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, soft.	960.0		—18" x 5/16" 3 SS, 0.070" Ful-Flo (854.
					 -870- 	SP	0 0	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/8); 85% sand, medium to coarse, angular to subangular, low sphericity; 10% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, soft.	869.0		- 879.87 ft b
					 - 875	CL		CLAY: light yellowish brown (7.5YR5/6); 90% silty clay as balls, nonplastic, soft to medium stiff; 10% well graded sand, fine to coarse, angular to subangular, low sphericity.	876.0		Colorado Sil
		=			  		0 , o	POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/8); 85% sand, medium to coarse, angular to subangular, low sphericity; 10% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, soft.	_   0.00		Pack (530 - 1265 ft bgs)
					  	SP	0.000				—18" x 5/16" 3 SS Blank (879.87 - 904.87 ft bgs
					-		0	CLAY: light yellowish brown (7.5YR5/6); 90% silty clay as	_ 886.0		
						-	IIIn.	Continued Next Page		्रिय दिव	1.776



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

PROJECT NAME

Monte Vista Water District

BORING/WELL NUMBER

Well #28

DATE DRILLED 1/25/01-2/23/01

					-			Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL	. DIAGRAM
					  -890-	CL		balls, nonplastic, soft to medium stiff; 10% well graded sand, fine to coarse, angular to subangular, low sphericity.	892.0		-18" x 5/16" 3 SS Blank (879.87 - 904.87 ft bgs
					- /	SP		POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/8); 85% sand, medium to coarse, angular to subangular, low sphericity; 10% poorly graded gravel	893.0		
					 -895- 	CL		and rock fragments, fine, 1/2-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, soft.  SANDY CLAY: light yellowish brown (7.5YR5/6); 70% clay as balls, nonplastic, soft to medium stiff; 25% poorly graded sand, medium to coarse, angular to subangular, low sphericity; poorly graded gravel with rock fragments, fine, 1/4-inch maximum diameter, angular to subangular,	897.0		
					  -900-  	CL		low sphericity. CLAY: light yellowish brown (7.5YR5/6); 90% silty clay as balls, nonplastic, soft to medium stiff; 10% well graded sand, fine to coarse, angular to subangular, low sphericity.			- Colorado Sil 6 x 16 Grave Pack (530 - 1265 ft bgs)
					-905  	CL		CLAY: yellowish brown (10YR5/8); 100% clay as balls, nonplastic, soft to medium stiff; trace poorly graded sand, fine to medium, angular to subangular, low sphericity; trace silt in matrix.	906.0		
					-910 			POORLY GRADED SAND WITH GRAVEL: yellowish brown (10YR5/8); 85% sand, medium to coarse, angular to subangular, low sphericity; 10% poorly graded gravel	912.0		-18" x 5/16" 3 SS, 0.070" Ful-Flo (904 - 959.79 ft b
					 -915- 	SP	0 0 0 0 0 0	and rock fragments, fine, 1/2-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, soft.			
					 920	SP	0 5 6 0	POORLY GRADED SAND WITH GRAVEL AND SILT: brownish yellow (10YR6/6); 75% poorly graded sand, medium to coarse, angular to subangular, low sphericity; 15% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter, angular to subrounded; 10% silt as balls, soft.	918.0		



#### **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER 10490-21966-WELL28.DRILL

BORING/WELL NUMBER Well #28

DATE DRILLED 1/25/01-2/23/01 **PROJECT NAME** Monte Vista Water District Continued from Previous Page RECOVERY (inches) SAMPLE ID. GRAPHIC LOG BLOW PID (ppm) DEPTH (ft. BGL) U.S.C.S. EXTENT LITHOLOGIC DESCRIPTION WELL DIAGRAM SM 924.0 POORLY GRADED SAND: brown (10YR5/3); 100% sand, medium to coarse, angular to subangular, low SP 925 sphericity, clean; trace silt. 926.0 POORLY GRADED SAND WITH GRAVEL AND SILT: yellowish brown (10YR5/4); 75% poorly graded sand, medium to coarse, angular to subangular, low sphericity; 15% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter, angular to subrounded; 10% 18" x 5/16" 304 930 SS, 0.070" Ful-Flo (904.87 SP - 959.79 ft bgs) SM 935 936.0 SILTY CLAY: dark yellowish brown (10YR4/6); 100% silty clay, moderately to highly plastic, medium stiff to stiff. CL 940.0 ·Colorado Silica SILTY SAND: brownish yellow (10YR6/6); 80% poorly 6 x 16 Gravel graded sand, fine to medium, angular to subangular, low Pack (530 sphericity; 20% silt as balls. 1265 ft bgs) SM NEWGINT MVWD.GPJ NEWGINT.GDT 4/3/01 950.0 950 SILTY SAND: brownish yellow (10YR6/6); 80% poorly graded sand, fine to medium, angular to subangular, low sphericity; 20% silt as balls. SM 953.0 SILTY SAND: brownish yellow (10YR6/6); 80% poorly graded sand, fine to medium, angular to subangular, low sphericity; 20% silt as balls. 955 Continued Next Page PAGE 28 OF 39



# **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

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PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELI	_ DIAGRAM
					    960- 	SM					-18" x 5/16" 3( SS, 0.070" Su-Fio (904.0 - 959.79 ft bg
					 -965 	SM		SILTY SAND: brownish yellow (10YR6/6); 80% poorly graded sand, fine to medium, angular to subangular, low sphericity; 20% silt as balls.  CLAY WITH SAND: brownish yellow (10YR6/6); 60% clay, moderately plastic, medium stiff to stiff; 20% poorly graded sand, medium, subangular to subrounded; 20% silt.	963.0		►Colorado Sili 6 x 16 Grave Pack (530 -
					 -970-  	CL		POORLY GRADED SAND: pale brown (10YR6/3); 100%	_ 973.0		1265 ft bgs)
					975	SP		sand, medium, some fine, subangular to subrounded; trace silt in balls.	976.0		
					   - 980- 	CL		SILTY CLAY WITH SAND: yellowish brown (10YR5/6); 60% clay, moderately plastic, medium stiff; 25% silt; 15% poorly graded sand, fine to medium, subangular to subrounded.			-18" x 5/16" 3 SS Blank (959.79 - 1004.73 ft bg
					 -985  			SILTY CLAY WITH SAND: yellowish brown (10YR5/6); 60% clay, moderately plastic, medium stiff; 25% silt; 15% poorly graded sand, fine to medium, subangular to subrounded.	986.0		
					- -990-	CL		Continued Next Page			



# **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

SAMPLE ID.  EXTENT  DEPTH  (ft. BGL)  U.S.C.S.	LITHOLOGIC DESCRIPTION	CONTACT OF PART OF PAR
995 CL SM :	SILTY CLAY WITH SAND: dark yellowish brown (10YR4/6); 60% clay, moderately plastic, medium stiff; 25% silt; 15% poorly graded sand, fine to medium, subangular to subrounded.  SILTY SAND: light yellowish brown (10YR6/4); 60% poorly graded sand, fine to medium, trace coarse, subangular to subrounded, low sphericity; 40% silt.  SILTY CLAY WITH SAND: yellowish brown (10YR5/6); 60% clay, moderately to highly plastic, very stiff; 25% silt; 15% poorly graded sand, fine to medium, subangular to subrounded.	993.0
CL	POORLY GRADED SAND WITH SILT: light yellowish brown (10YR4/6); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	1005.0
CL CL 	CLAY: yellowish brown (10YR5/6); 100% clay, nonplastic, medium stiff.  POORLY GRADED SAND WITH SILT: light yellowish brown (10YR4/6); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	1015.018" x 5/16" 3
	-1000- CL CL 	poorly graded sand, fine to medium, trace coarse, subangular to subrounded, low sphericity; 40% silt.  SILTY CLAY WITH SAND: yellowish brown (10YR5/6); 60% clay, moderately to highly plastic, very stiff; 25% silt; 15% poorly graded sand, fine to medium, subangular to subrounded.  POORLY GRADED SAND WITH SILT: light yellowish brown (10YR4/6); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.  CLAY: yellowish brown (10YR5/6); 100% clay, nonplastic, medium stiff.  POORLY GRADED SAND WITH SILT: light yellowish brown (10YR4/6); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.



#### **BORING/WELL CONSTRUCTION LOG**

 PROJECT NUMBER
 10490-21966-WELL28.DRILL
 BORING/WELL NUMBER
 Well #28

 PROJECT NAME
 Monte Vista Water District
 DATE DRILLED
 1/25/01-2/23/01

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PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL	. DIAGRAM
					+1025-  - +1030-   	SP		POORLY GRADED SAND: light yellowish brown (10YR4/6); 90% sand, medium to coarse, some fine, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	_ 1027.0		-18" x 5/16" 30 SS, 0.070" Ful-Flo (1004.73 - 1039.62 ft bgs
						SP SM		POORLY GRADED SAND WITH SILT: light yellowish brown (10YR4/6); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	_ 1037./		-Colorado Silio 6 x 16 Gravel Pack (530 - 1265 ft bgs)
					   	CL		CLAY: yellowish brown (10YR5/4); 100% clay, nonplastic, medium stiff.	_ 1050.	\$ 1	-18" x 5/16" 3 SS Blank (1039.62 - 1119.74 ft bg
					 -1055  			SILTY SAND: light yellowish brown (10YR4/6); 80% poorly graded sand, medium to coarse, some fine, angular to subangular, low sphericity; 15% silt as balls, inelastic, medium stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	_ 1055.	G	



## **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER Well #28

								Continued from Previous Page		
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
						SM		CLAY AND SILT: 50% clay as balls, dark yellowish brown (10YR4/6), nonplastic, soft; 50% silt as balls, yellowish brown (10YR5/6), inelastic, medium stiff.	_ 1064.0	18" x 5/16" 3 SS Blank (1039.62 - 1119.74 ft bgs
					  - <del>1</del> 07 <del>5</del> - 	CL		CLAY: yellowish brown (10YR5/6); 100% clay, nonplastic, medium stiff; trace well graded sand, fine to coarse, angular to subangular, low sphericity.	1074.0	Colorado Silic 6 x 16 Gravel Pack (530 - 1265 ft bgs)
					 - <del>1</del> 08 <del>0</del> - 			CLAY: yellowish brown (10YR5/4); 100% clay, plastic, medium stiff.	1080.0	
					 - <del>1</del> 08 <del>5</del> - 	CH		CLAY: yellowish brown (10YR5/6); 100% clay, nonplastic, medium stiff; trace well graded sand, fine to coarse, angular to subangular, low sphericity.	1086.0	<b>G</b>
					- <del>1</del> 09 <del>0</del> 	CL		SILTY SAND: light yellowish brown (10YR4/6); 80%  Continued Next Page	_ 1092.	<b>c</b>



#### **BORING/WELL CONSTRUCTION LOG**

								Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEL	L DIAGRAM
					  -1095	SM		poorly graded sand, medium to coarse, some fine, angular to subangular, low sphericity; 15% silt as balls, inelastic, medium stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	1096.0		
								CLAY: yellowish brown (10YR5/6); 100% clay, nonplastic, medium stiff; trace well graded sand, fine to coarse, angular to subangular, low sphericity.			1011 15/1011
					<del>-1</del> 10 <del>0</del> -  	CL			1104.0		
					- - <del>1</del> 105 -	SP SM		POORLY GRADED SAND WITH SILT: light yellowish brown (10YR4/6); 85% sand, medium to coarse, some fine, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	1106.0		
					 	SP		POORLY GRADED SAND: light yellowish brown (10YR4/6); 90% sand, medium to coarse, some fine, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	1109.0		
					 			CLAY WITH SAND: brownish yellow (10YR6/6); 85% clay, nonplastic, medium stiff; 15% poorly graded sand, medium to coarse; trace rock fragments, 1/2-inch maximum diameter, angular to subangular low sphericity.			6 x 16 Grave Pack (530 - 1265 ft bgs)
					 <del>-1</del> 115- 	CL					
					  <del>-1</del> 12 <del>0</del> -			SILTY SAND: light yellowish brown (10YR4/6); 80% poorly graded sand, medium to coarse, some fine, angular to subangular, low sphericity; 15% silt as balls, inelastic, medium stiff; 5% poorly graded gravel and rock fragments,	1119.0		
						SM		fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.  SILTY SAND: light yellowish brown (10YR4/6); 70% poorly graded sand, medium to coarse, some fine, angular	1123.0		
					 -1125 	SM		to subangular, low sphericity; 25% silt as balls, inelastic, medium stiff; 5% poorly graded gravel and rock fragments, fine, 1/4-inch maximum diameter; angular to subangular, low sphericity.  CLAY: yellowish brown (10YR5/6); 100% clay, nonplastic,	1125.0 1126.0		



#### **BORING/WELL CONSTRUCTION LOG**

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

			_				Continued from Previous Page			
PID (ppm) BLOW COUNTS	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEL	L DIAGRAM
	RE.	SAI		1130 	SM SP CL SP		medium stiff to stiff; trace well graded sand, fine to coarse, angular to subangular, low sphericity.  SILTY SAND: light yellowish brown (10YR4/6); 80% poorly graded sand, medium to coarse, some fine, angular to subangular, low sphericity; 15% silt as balls, inelastic, soft to medium stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.  POORLY GRADED SAND: light yellowish brown (10YR4/6); 90% sand, medium to coarse, some fine, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff to stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.  SILT WITH SAND: dark yellowish brown (10YR4/6); 75% silt; 15% well graded sand, fine to coarse, subrounded to rounded; 10% poorly graded gravel, fine, 3/4-inch maximum diameter.  POORLY GRADED SAND WITH GRAVEL: dark grayish brown (10YR4/2); 75% sand, fine to medium, subrounded to rounded; 20% well graded gravel and rock fragments, fine to coarse, 1-inch maximum diameter, subrounded to rounded; 5% silt.  SILTY CLAY: yellowish brown (10YR5/8); 100% silty clay; trace fine sand.  POORLY GRADED SAND WITH GRAVEL: dark grayish brown (10YR4/2); 75% sand, fine to medium, subrounded to rounded; 5% silt.  SILTY CLAY: yellowish brown (10YR5/8); 100% silty clay; trace fine sand.	1128.0 1128.0 1137.0 1141.0		-18" x 5/16" 3 SS, 0.070" Ful-Flo (1119.74 - 1169.74 ft bg 6 x 16 Grave Pack (530 - 1265 ft bgs)
			-	  <del>1</del> 160	CL		POORLY GRADED SAND: yellowish brown (10YR5/4); 90% sand, medium to coarse, angular to subangular, low	1160.0		



#### **BORING/WELL CONSTRUCTION LOG**

PAGE 35 OF 39

Well #28

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

1/25/01-2/23/01 **PROJECT NAME** Monte Vista Water District DATE DRILLED Continued from Previous Page RECOVERY (inches) GRAPHIC LOG SAMPLE ID. PID (ppm) BLOW CONTACT EXTENT DEPTH (ft. BGL) U.S.C.S. LITHOLOGIC DESCRIPTION WELL DIAGRAM sphericity; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff. 18" x 5/16" 304 SP 1165 SS, 0.070" Ful-Flo (1119.74 -1169.74 ft bgs) 1170.d POORLY GRADED SAND: yellowish brown (10YR5/4); 90% sand, medium to coarse, angular to subangular, low sphericity; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff. SP Colorado Silica 6 x 16 Gravel Pack (530 -1265 ft bgs) 1179.0 CLAY: brownish yellow (10YR6/6); 100% clay, nonplastic, 1180 CL 1185.d 18" x 5/16" 304 SILTY SAND: yellowish brown (10YR5/4); 60% poorly graded sand, medium to coarse, angular to subangular, SS Blank (1169.74 low sphericity; 35% silt as balls, inelastic, soft; 5% poorly 1194.68 ft bgs) graded gravel and rock fragments, fine, 3/4-inch maximum diameter; angular to subangular, low sphericity. NEWGINT MVWD.GPJ NEWGINT.GDT 4/3/01 SM 1195.d POORLY GRADED SAND WITH SILT: yellowish brown Continued Next Page



# **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER

10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

HUJ	IECT N	AIVIE	_ IVIO	mite '	Vista W	ater D	nstrict	DATE DRILLED 1/25/01-2/23/01			
							1 1	Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WEL	L DIAGRAM
						SP SM		(10YR5/4); 85% poorly graded sand, medium to coarse, angular to subangular, low sphericity; 10% silt as balls, inelastic, soft; 5% poorly graded gravel and rock fragments, fine, 3/4-inch maximum diameter; angular to subangular, low sphericity.			
					+205    +210-	SP		POORLY GRADED SAND: yellowish brown (10YR5/4); 90% sand, medium to coarse, angular to subangular, low sphericity; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff.	_ 1205.0		-18" x 5/16"; SS, 0.070" Ful-Flo (1194.68 - 1224.67 ft b
					  	SM		SILTY SAND: yellowish brown (10YR5/4); 60% poorly graded sand, medium to coarse, angular to subangular, low sphericity; 35% silt as balls, inelastic, soft to medium stiff; 5% poorly graded gravel and rock fragments, fine, 1/2-inch maximum diameter; angular to subangular, low sphericity.	1212.0		-Colorado S 6 x 16 Grav
					   - 122 <del>0</del> - 	SP		POORLY GRADED SAND: yellowish brown (10YR5/4); 90% sand, medium to coarse, angular to subangular, low sphericity; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff.	_ 1216.0		Pack (530 - 1265 ft bgs)
						SP		POORLY GRADED SAND: yellowish brown (10YR5/4); 90% sand, medium to coarse, angular to subangular, low sphericity; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity; 5% silt as balls, inelastic, medium stiff.	1226.0		18" x 5/16" SS Blank W Shoe (1224 1244.79 ft b
					<del>-1</del> 23 <del>0</del> -			Continued Next Page			PAGE 36 OF



# **BORING/WELL CONSTRUCTION LOG**

								Continued from Previous Page			
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAG	RAM
					  -1235-  	CL		CLAY: light reddish brown (5YR6/4); 100% clay, nonplastic, stiff to very stiff; trace well graded sand, fine to coarse, angular to subangular, low sphericity.	1232.0	18" x ss Bl	5/16" 3( ank W/ (1224.6) 79 ft bgs
					   -1245-  	CL		CLAY: brownish yellow (10YR6/6); 100% clay, nonplastic, soft to medium stiff; trace poorly graded sand, medium to coarse, angular to subangular, low sphericity.	1242.0		
					125 <del>0</del>	CL		CLAY: brownish yellow (10YR6/6); 100% clay, nonplastic, soft to medium stiff; trace poorly graded sand, medium to coarse, angular to subangular, low sphericity.	1252.0	Pack ( 1265 f	Gravel (530 -
					  1260- 	SP SM		POORLY GRADED SAND WITH SILT: yellowish brown (10YR5/4); 85% sand, medium to coarse, angular to subangular, low sphericity; 10% silt as balls, inelastic, medium stiff; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity.	_ 1256.C		



#### **BORING/WELL CONSTRUCTION LOG**

PAGE 38 OF 39

PROJECT NUMBER 10490-21966-WELL28.DRILL

BORING/WELL NUMBER Well #28

PROJ	ECT NA	AME	_ Mo	nte	Vista W	Vater D	District	DATE DRILLED 1/25/01-2/23/01  Continued from Previous Page		
		>						Commuea nom Frevious Page	1	
PID (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	DEPTH (ft. BGL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL DIAGRAM
					-1265    -1270 	SP SM		POORLY GRADED SAND WITH SILT: yellowish brown (10YR5/4); 80% sand, medium to coarse, angular to subangular, low sphericity; 15% silt as balls, inelastic, medium stiff; 5% poorly graded gravel and rock fragments; fine, 3/4-inch maximum diameter, angular to subangular, low sphericity.	1266.0	# Sluff (1265 1317 ft bgs
					 - <del>1</del> 275-  	ML		CLAYEY SILT: yellowish red (5YR4/6); 90% clayey silt, inelastic to moderately elastic, soft; 10% poorly graded sand, fine, trace medium, subangular to subrounded.	_ 1274.0	
					-1280   - 1285   - 1290	SM		SILTY SAND WITH GRAVEL: light yellowish brown (10YR6/4); 40% poorly graded sand, medium to coarse, subangular to subrounded; 30% silt; 20% well graded gravel and rock fragments, fine to coarse, 1-inch maximum diameter, subangular to subrounded; 10% clay, nonplastic, soft.	_ 1280.0	
					  - 1295- 	CL		SILTY CLAY: yellowish brown (10YR5/8); 50% clay, moderately plastic, medium stiff; 45% silt; 5% poorly graded sand, coarse, angular to subangular.	1291.0	



# **BORING/WELL CONSTRUCTION LOG**

PROJECT NUMBER 10490-21966-WELL28.DRILL

BORING/WELL NUMBER

Well #28

rio (ppm)	BLOW	RECOVERY (inches)	SAMPLE ID.	EXTENT	oTH 3GL)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT	WELL	. DIAGRAM
<u>a</u>	SOU	RECO (incl	SAMP	EXT	DEPTH (ft. BGL)	U.S.	GRA	LITHOLOGIC DESCRIPTION	CON	VVEC	DIAGNAM
					 -1300 			SILTY CLAY: dark yellowish brown (10YR4/6); 50% clay, moderately plastic, medium stiff; 45% silt; 5% poorly graded sand, coarse, angular to subangular.	1301.0		
					 -1305-  	CL					-Sluff (1265 1317 ft bgs
					- 1310    - 1315-	ML		SANDY SILT: brownish yellow (10YR6/6); 50% silt; 45% poorly graded sand, medium, trace coarse, subangular to subrounded; 5% clay.	_  1310.0		
								Total Depth of Borehole is 1,317 feet bgs.	1317.0		

# PACIFIC SURVEYS

File No.

Sec.

# **ELECTRIC LOG** LATEROLOG 3 **GAMMA-RAY**

Job No. CASCADE DRILLING Company 25150

> Well **IEUA PX2**

Field **POMONA** 

LOS ANGELES CA County State

Other Services: Location:

WEST SIDE OF MONTVUE PARK: 1634 CORDOVA ST GPS: 34.0747462 -117.214596

Twp.

LL3 SONIC **CALIPER** 

TMP

DEVIATION Rge.

Elevation G.L. Permanent Datum Elevation K.B. D.F. G.L. G.L. 0' above perm. datum Log Measured From G.L. Drilling Measured From 01-17-2019 Date Run Number ONE Depth Driller 1295' Depth Logger 1295' **Bottom Logged Interval** 1295.6' Top Log Interval 40' Casing Driller 20" @ 50' 50' Casing Logger Bit Size 17.5" Type Fluid in Hole **BENTONITE** Density / Viscosity 9.2 / 37 pH / Fluid Loss -- / 7 Source of Sample MUD TANK Rm @ Meas. Temp 6.2 @ 71.2 F 5.96 @ 71.2 F Rmf @ Meas. Temp Rmc @ Meas. Temp N/A Source of Rmf / Rmc **MEASURED** Rm @ BHT N/A Time Circulation Stopped 0745 Time Logger on Bottom 1230 Max. Recorded Temperature 72.69 F **Equipment Number** PS-5 Location **VENTURA** Recorded By **CALEB VILLALOBOS** Witnessed By ROBERT THACKER

s and we cannot and do not guarantee the accuracy or correctness or our part, be liable or responsible for any loss, costs, damages, or of our officers, agents or employees. These interpretations are also in our current Price Schedule. opinions based on inferences from electrical or other measurements and we shall not, except in the case of gross or willful negligence on r sustained by anyone resulting from any interpretation made by any subject to our general terms and conditions set out it All interpretations are op any interpretation, ar expenses incurred or s

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Comments

o

Calibration Report

25150.db ELOG Thu Jan 17 12:51:01 2019

Dataset Pathname Dataset Creation Database File

Report Calibration 90 Serial: D4 Model: DTQ

Shop Calibration Performed: Before Survey Verification Performed: After Survey Verification Performed: Fri Jun 01 15:42:16 2018 Thu Nov 16 12:27:34 2017 Thu Nov 16 12:28:17 2017

#### Shop Calibration

	Readings		Readings			References			Results	
	Zero	Cal		Zero	Cal		Gain	Offset		
Short	0.417	44.861		0.500	50.000	Ohm-m	1.114	0.036		
Long	3.373	181.647		2.000	200.000	Ohm-m	1.111	-1.746		
IEE	99.060	25586.141	counts	0.108	28.001	Α				
VSN	15.160	0.000	counts	0.289	0.000	V				
VLN	161.020	136.420	counts	3.071	2.602	V				

#### Before Survey Verification

	Read	ings		Refere	nces		Resu	ults
	Zero	Cal		Zero	Cal		Gain	Offset
Short	0.000	101.105		0.000	101.038	Ohm-m	0.999	0.000
Long	0.000	102.475		0.000	102.112	Ohm-m	0.996	0.000
IEE	0.000	3225.740	counts	0.000	3.530	Α		
VSN	86.120	3664.180	counts	1.643	69.890	V		
VLN	76.720	928.460	counts	1.463	17.709	V		

#### After Survey Verification

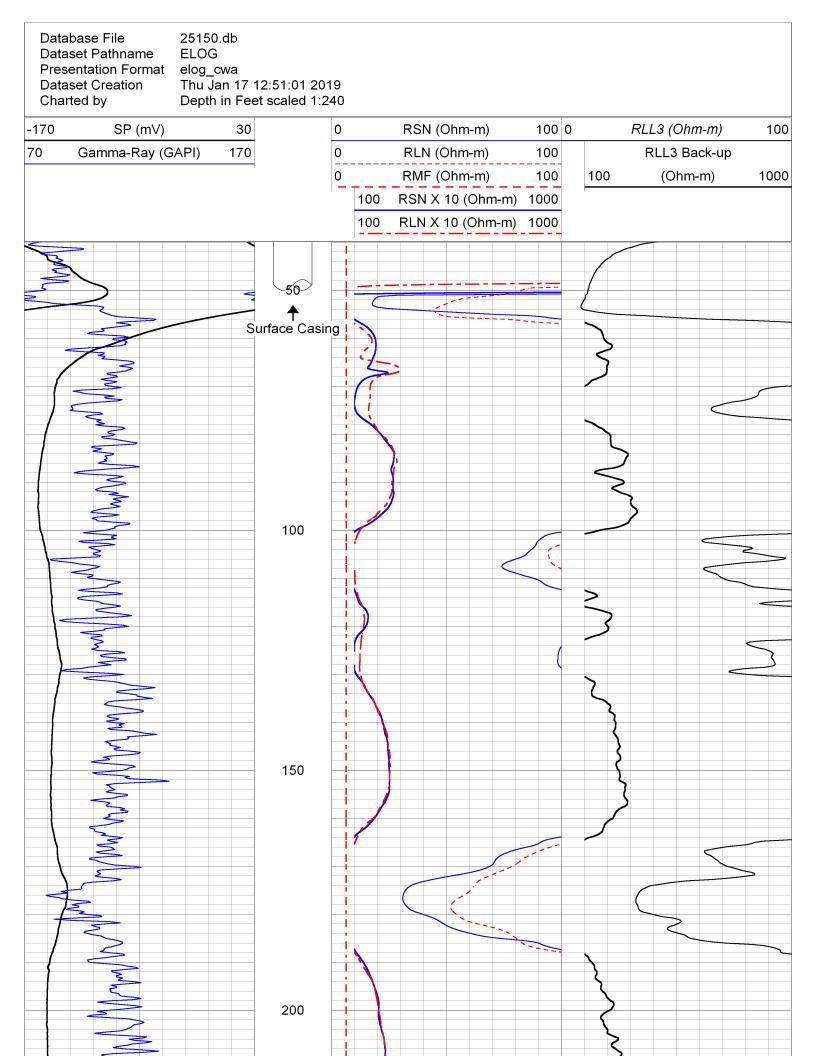
	Readings			References			Resu	sults	
	Zero	Cal		Zero	Cal		Gain	Offset	
Short	0.000	101.067		0.000	101.105	Ohm-m	1.000	0.000	
Long	0.000	102.216		0.000	102.475	Ohm-m	1.003	0.000	
IEE	0.000	3483.240	counts	0.000	3.812	Α			
VSN	86.720	3955.200	counts	1.654	75.441	V			
VLN	77.260	1000.040	counts	1.474	19.075	V			

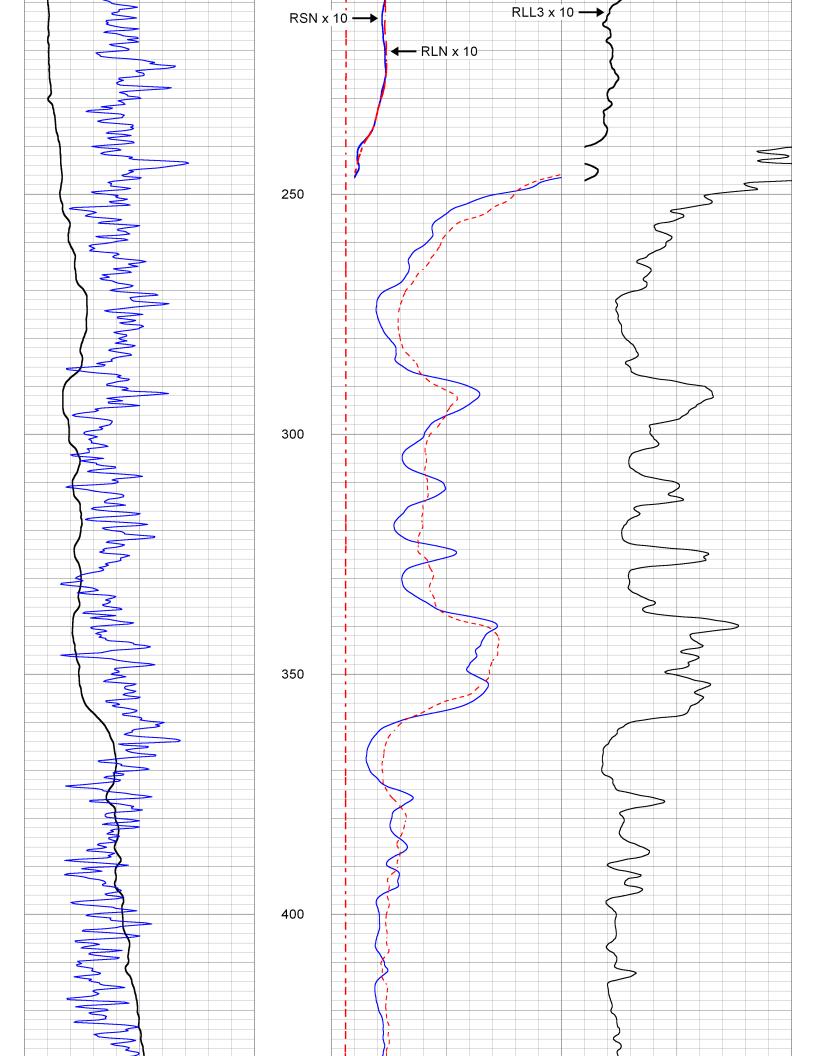
#### After Survey Verification compared to Before Survey Calibration

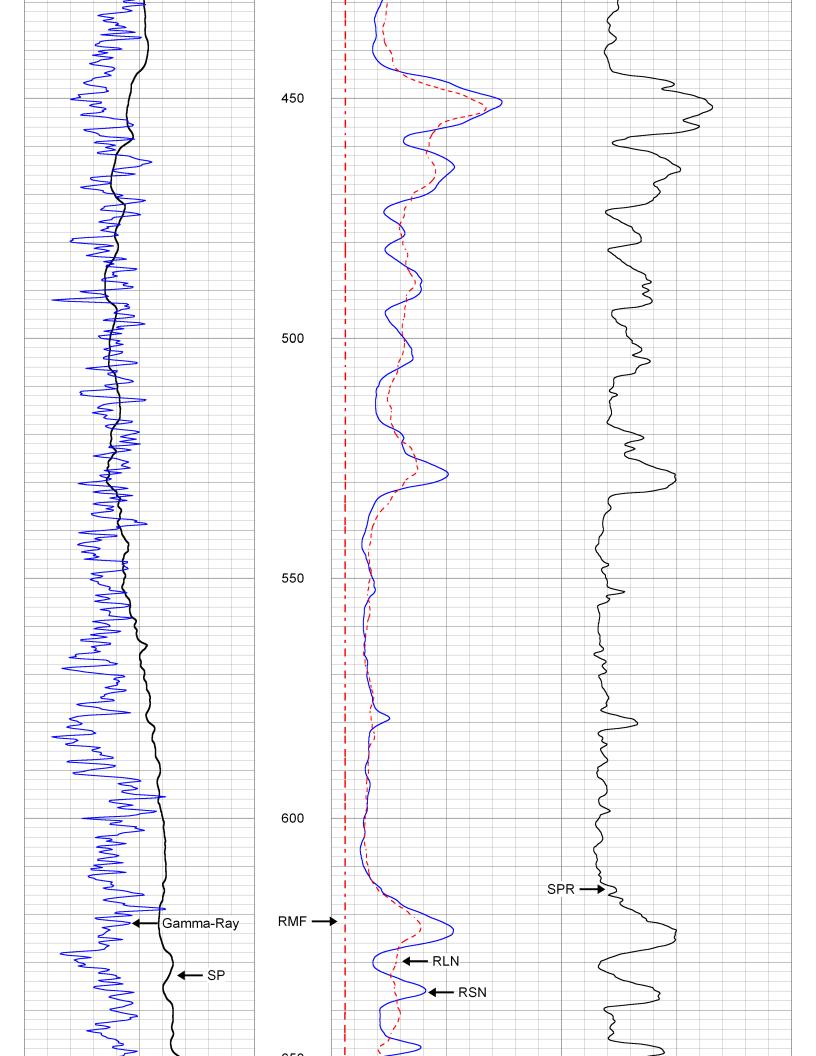
	Zer	0		Ca	İ	
	Before	After		Before	After	
Short	0.000	0.000	Ohm-m	101.038	101.105	Ohm-m
Long	0.000	0.000	Ohm-m	102.112	102.475	Ohm-m

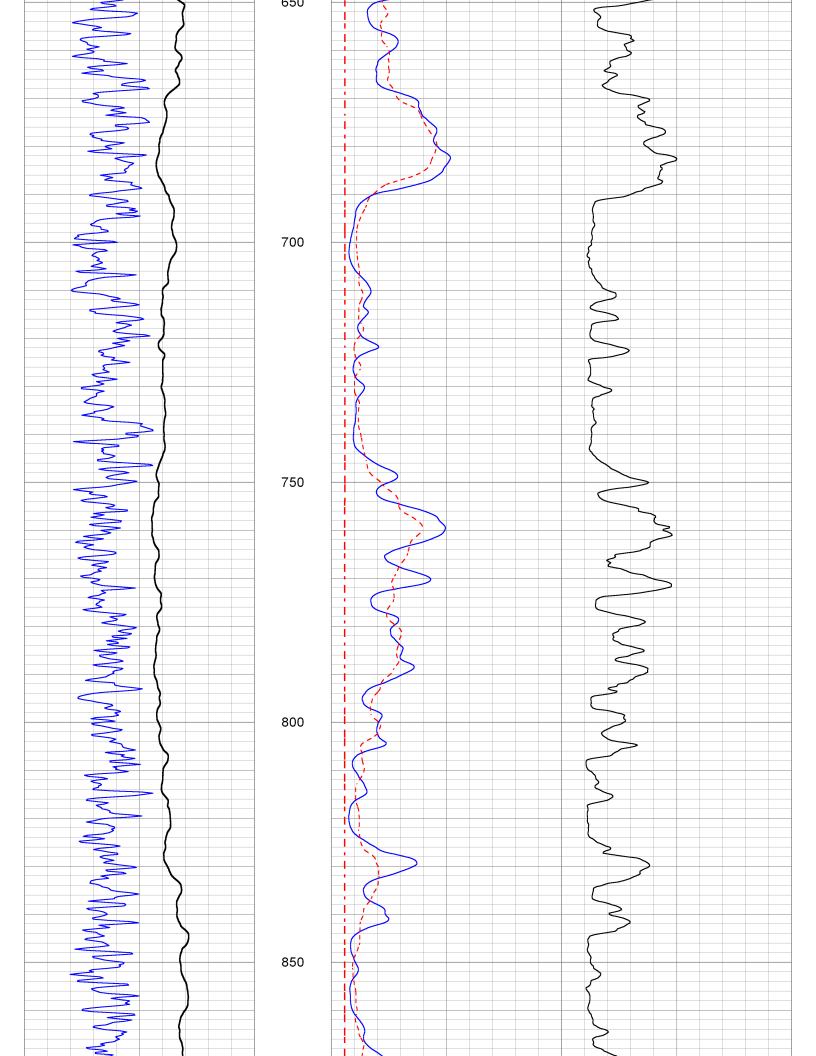
#### Gamma Ray Calibration Report

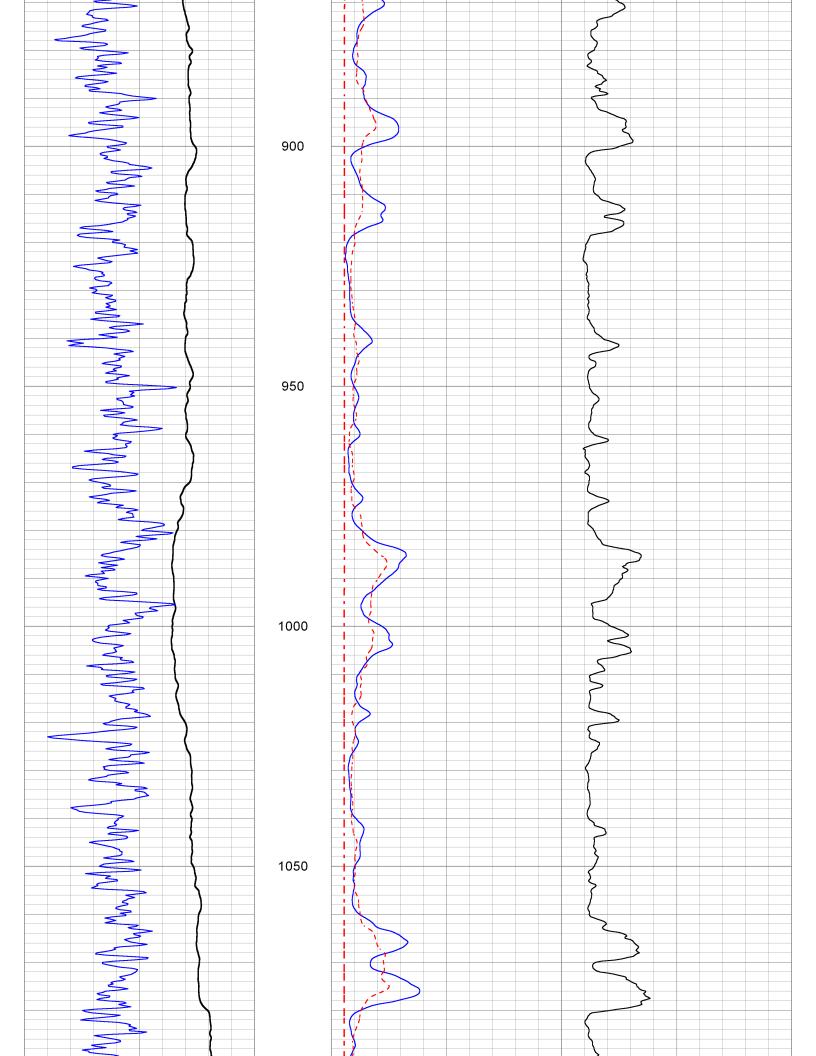
Serial Number: Tool Model: Performed:	D4 ELOG Fri Dec 07 11:42:	17 2018
Calibrator Value:	162.0	GAPI
Background Reading: Calibrator Reading:	101.7 326.7	cps cps
Sensitivity:	0.7200	GAPI/cps

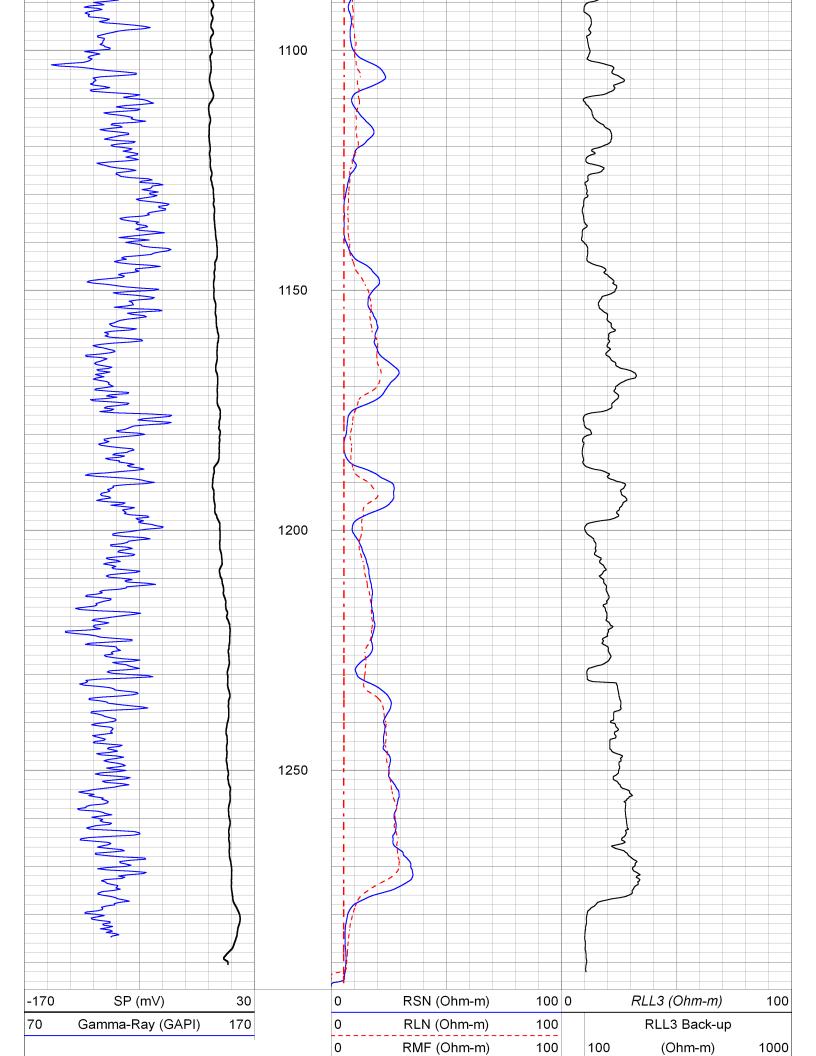












100	RSN X 10 (Ohm-m)	1000
100	RLN X 10 (Ohm-m)	1000

# Log Variables

DatabaseC:\ProgramData\Warrior\Data\25150.db Dataset field/well/run1/ELOG/\_vars\_

Top - Bottom

			<u>-</u>			
BOREID	BOTTEMP	CASEOD	CASETHCK	PERFS	RM_MEAS_R	RM_MEAS_T
in	degF	in	in		Ohm-m	degF
17.5	79.3	5.5	0	0	6.2	71.2
RMF	RSH	SPSHIFT	SRFTEMP	TDEPTH	TempGrad	
Ohm-m	Ohm-m	mV	degF	ft	DegF/ft	
5.96	20	7	63.5	1295	0.01235	

# ima Ray Calibration Report



# LATEROLOG 3 GAMMA-RAY

Job No.
25150 Company CASCADE DRILLING

Well IEUA PX2

Field POMONA

County LOS ANGELES State CA

Location: Other Services:

WEST SIDE OF MONTVUE PARK: 1634 CORDOVA ST

Twp.

ELOG/GR SONIC TMP CALIPER

GPS: 34.0747462 -117.214596

File No.

Sec.

TMP DEVIATION

Permanent Datum G.L. Elevation
Log Measured From G.L. 0' above perm. datum
Drilling Measured From G.L.

Date 01-17-2019
Run Number ONE

Rge.

-•	G.L.
01-17-2019	
ONE	
1295'	
1295'	
1296.1'	
40'	
20" @ 50'	
50'	
17.5"	
BENTONITE	
9.2 / 37	
/ 7	
MUD TANK	
6.2 @ 71.2 F	
5.96 @ 71.2 F	
N/A	
MEASURED	
N/A	
0745	
1340	
72.69 F	
PS-5	
VENTURA	
CALEB VILLALOBOS	_
ROBERT THACKER	
	01-17-2019  ONE  1295' 1296.1' 40' 20" @ 50' 50' 17.5"  BENTONITE  9.2 / 37 / 7  MUD TANK  6.2 @ 71.2 F  N/A  MEASURED  N/A  0745  1340  72.69 F  PS-5  VENTURA  CALEB VILLALOBOS

or correctness of All interpretations are opinions based on inferences from electrical or other measurements and we cannot and do not guarantee the accuracy or correctness o any interpretation, and we shall not, except in the case of gross or willful negligence on our part, be liable or responsible for any loss, costs, damages, or expenses incurred or sustained by anyone resulting from any interpretation made by any of our officers, agents or employees. These interpretations are also subject to our general terms and conditions set out in our current Price Schedule.

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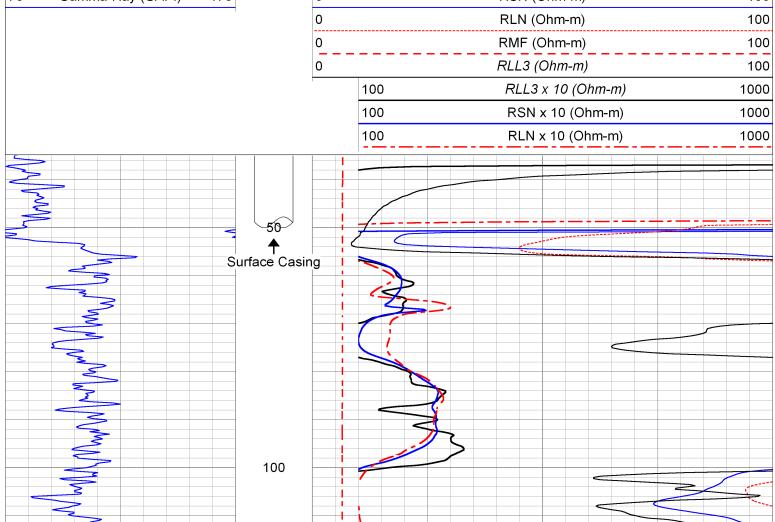
Comments

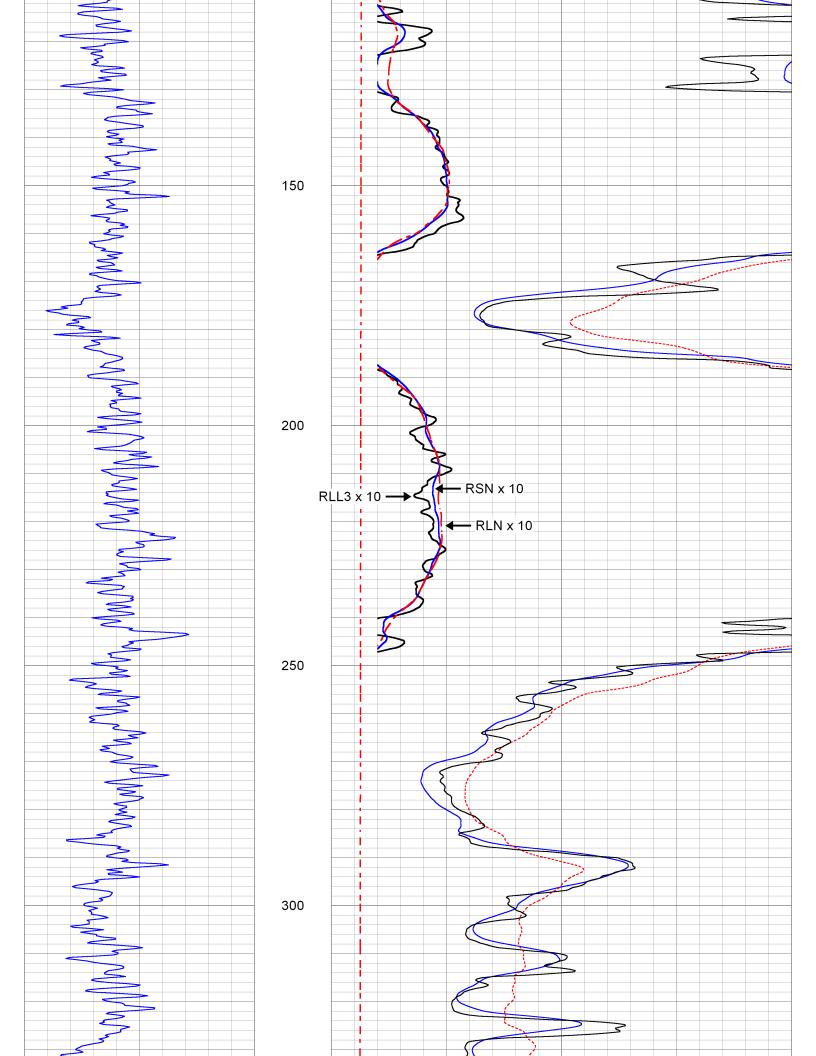
Calibration Report

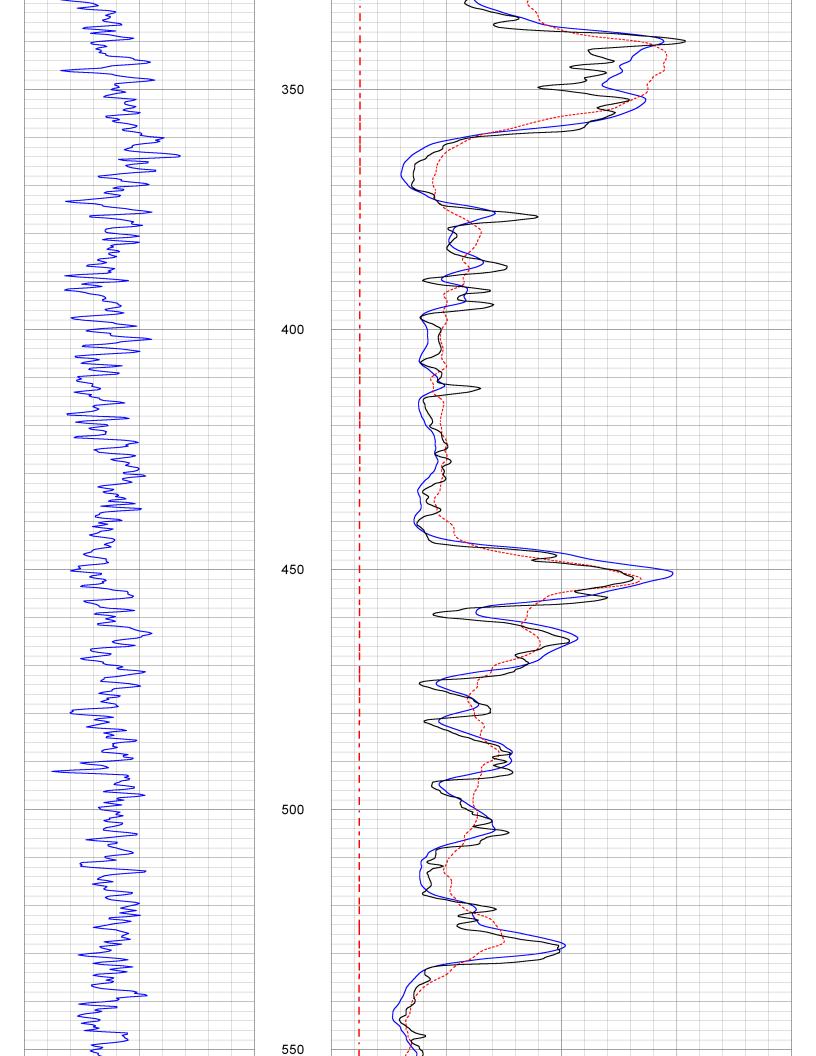
25150.db le GUARD1 Thu Jan 17 13:50:05 2019

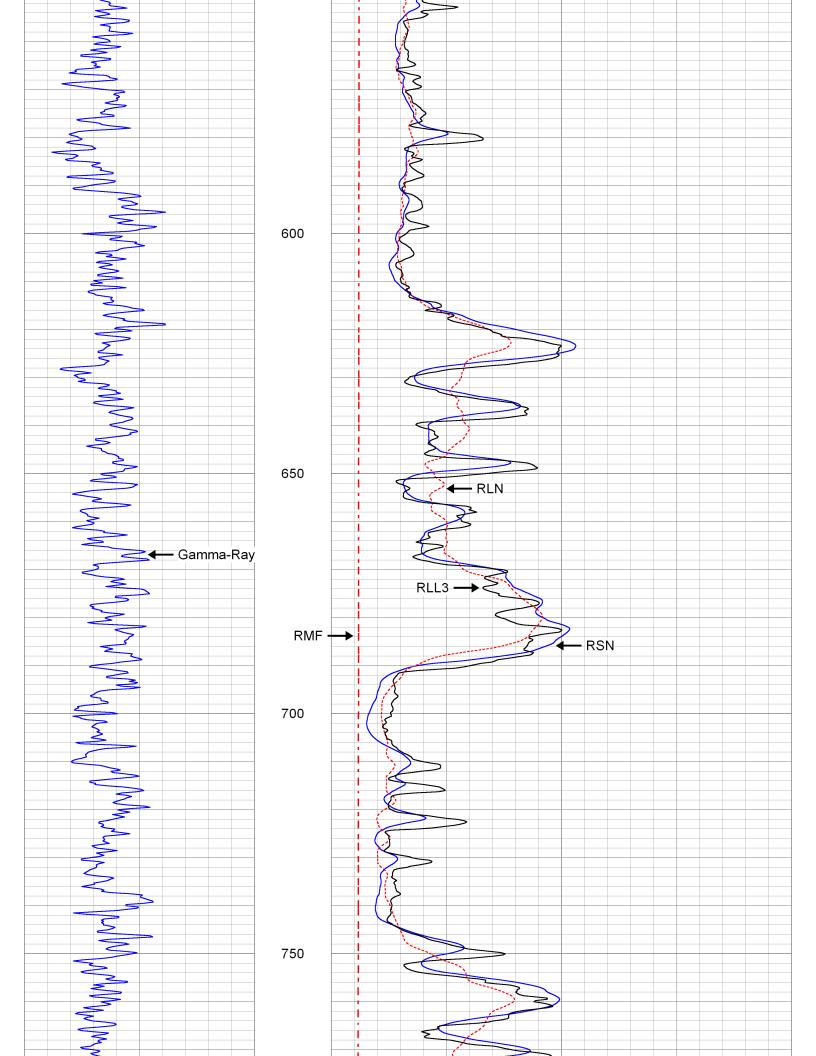
Database File 25150 Dataset Pathname GUAR Dataset Creation Thu Ja

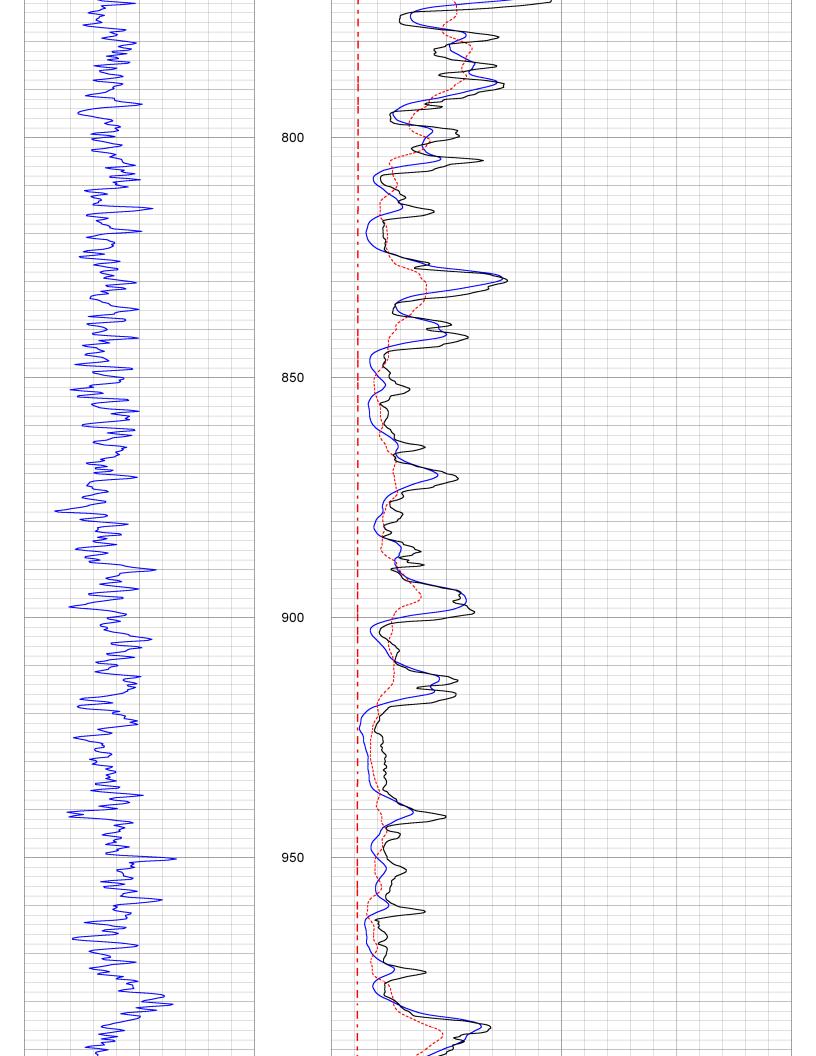
12 Serial Number: **GROH** Tool Model: Performed: Thu Nov 16 12:19:03 2017 Calibrator Value: 162.0 **GAPI** Background Reading: 54.1 Calibrator Reading: 193.3 Sensitivity: GAPI/ 1.1641 RLL3 (Resistivity Laterolog 3) Calibration Report: Serial Number: 128 Tool Model: M&W Performed: Thu Nov 16 12:18:00 2017 System Reading Calibration Reference 800.0 2.500 Ohm-m 0.015 5.000 50.000 0.154 0.787 250.000 1.646 500.000 Database File 25150.db **GUARD1 Dataset Pathname** Presentation Format guard **Dataset Creation** Thu Jan 17 13:50:05 2019 Charted by Depth in Feet scaled 1:240 70 Gamma-Ray (GAPI) 170 0 RSN (Ohm-m) 100 0 RLN (Ohm-m) 100 0 100 RMF (Ohm-m) 0 RLL3 (Ohm-m) 100 100 1000

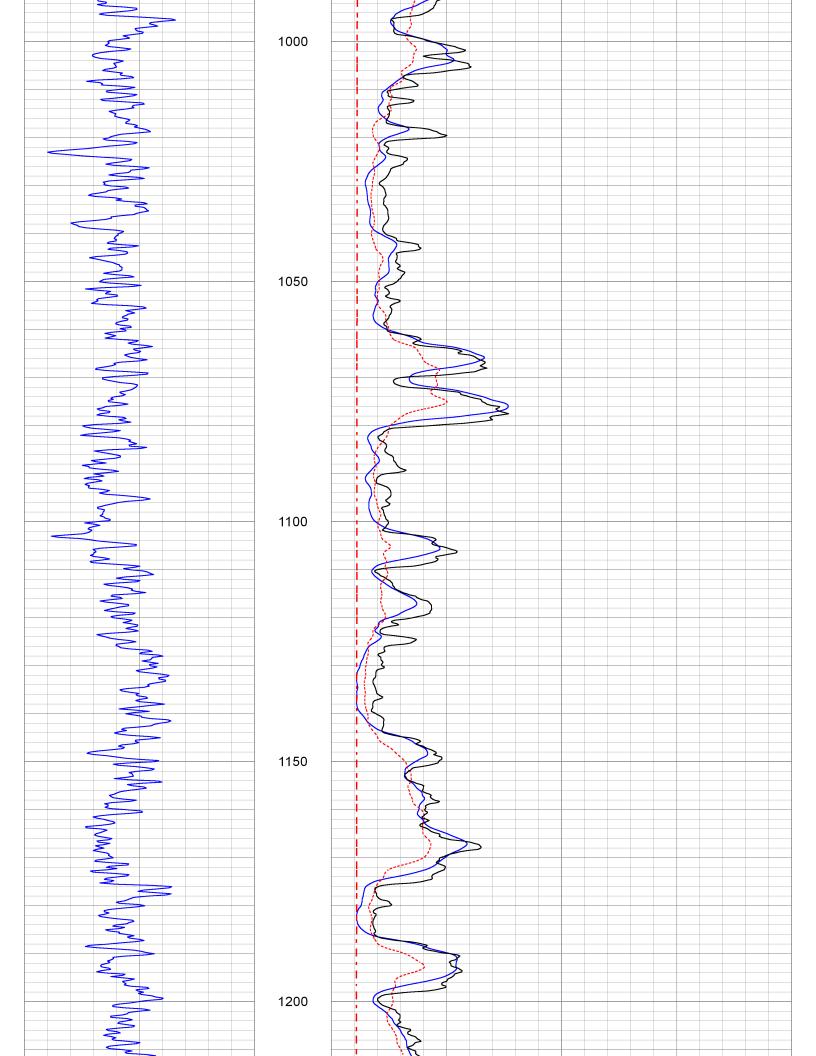


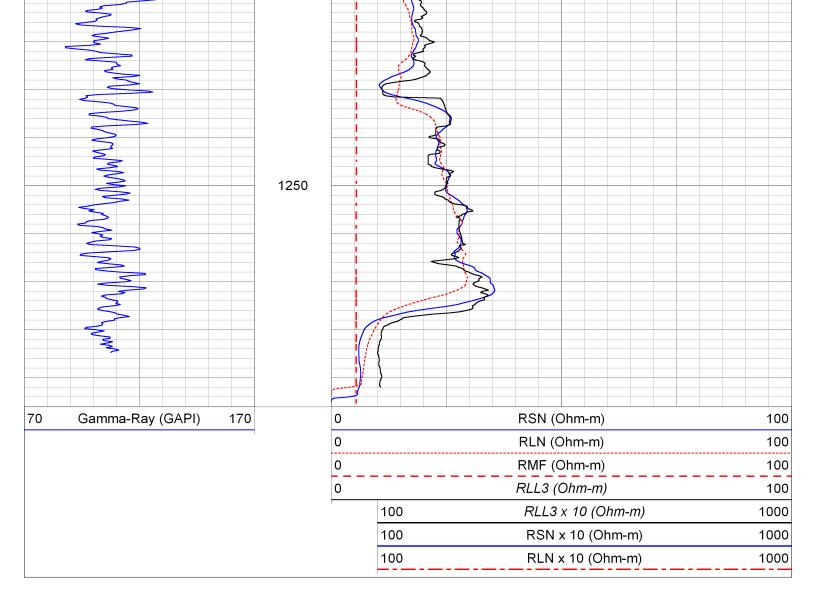












₋og Vari	Og Variables DatabaseC:\ProgramData\Warrior\Data\25150.db Dataset field/well/run1/GUARD1/_vars_								
Top - Bottom									
BOREID in	BOTTEMP degF	CASEOD in	CASETHCK in	PERFS	RM_MEAS_R Ohm-m	RM_MEAS_T degF			
17.5	79.3	5.5	0	0	6.2	71.2			
RMF Ohm-m 5.96	RSH Ohm-m 20	SPSHIFT mV 7	SRFTEMP degF 63.5	TDEPTH ft 1295	TempGrad DegF/ft 0.01235				

# PACIFIC SURVEYS

# **SONIC VELOCITY VARIABLE DENSITY**

Job No. **CASCADE DRILLING** Company 25150

> Well **IEUA PX2**

**POMONA** Field File No.

LOS ANGELES CA County State

Other Services: Location:

WEST SIDE OF MONTVUE PARK: 1634 CORDOVA ST GPS: 34.0747462 -117.214596

Twp.

LL3 TEMP DEVIATION

ELOG

**CALIPER** 

Sec.

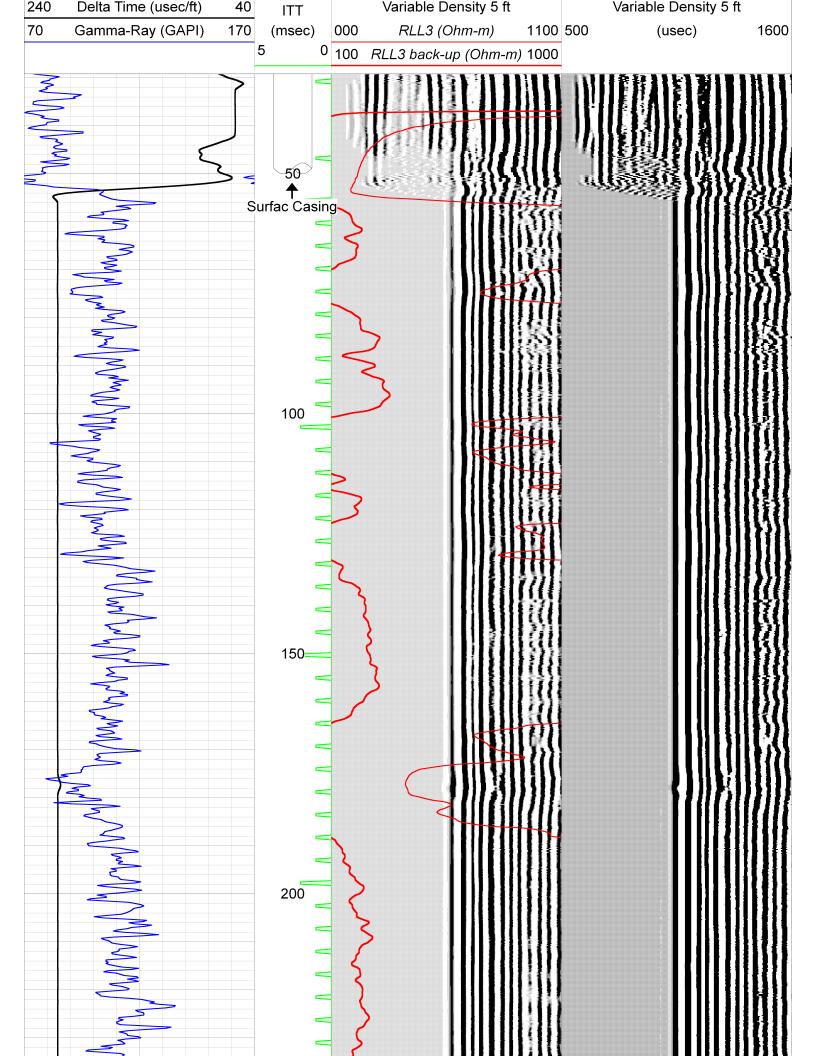
Rge. G.L. Elevation Permanent Datum Elevation above perm. datum G.L. 0' K.B Log Measured From

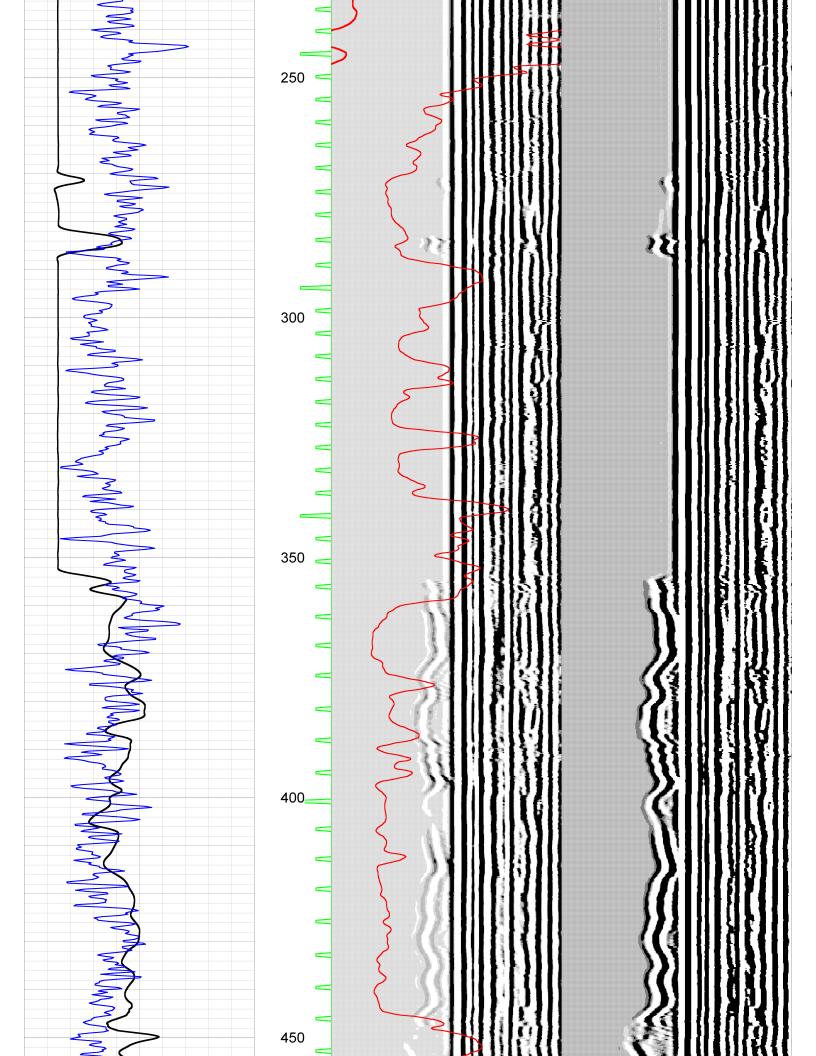
Drilling Measured From G.	L.	and the period duction	D.F. G.L.	
Date	01-17-2019			
Run Number	ONE			
Depth Driller	1295'			
Depth Logger	1296.8 F			
Bottom Logged Interval	1296.8 F			
Top Log Interval	30'			
Casing Driller	20" @ 50'			
Casing Logger	50'			
Bit Size	17.5"			
Type Fluid in Hole	BENTONITE			
Density / Viscosity	9.2 / 37			
pH / Fluid Loss	/ 7			
Source of Sample	MUD TANK			
Rm @ Meas. Temp	6.2 @ 71.2 F			
Rmf @ Meas. Temp	5.96 @ 71.2 F			
Rmc @ Meas. Temp	N/A			
Source of Rmf / Rmc	MEASURED			
Rm @ BHT	N/A			
Time Circulation Stopped	0745			
Time Logger on Bottom	1645			
Max. Recorded Temperature	72.69 F			
Equipment Number	PS-5			3
Location	VENTURA			
Recorded By	CALEB VILLALOBOS			,
Witnessed By	ROBERT THACKER			

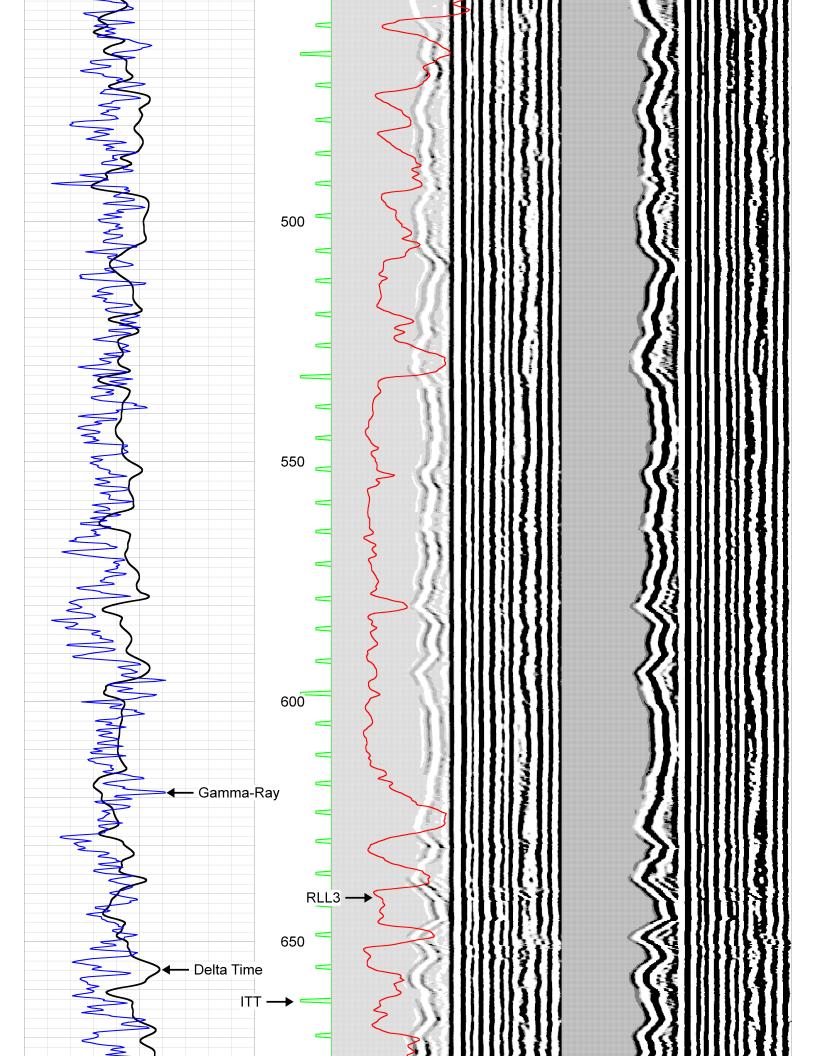
etations are opinions based on inferences from electrical or other measurements and we cannot and do not guarantee the accuracy or correctness of any tation, and we shall not, except in the case of gross or willful negligence on our part, be liable or responsible for any loss, costs, damages, or expenses or sustained by anyone resulting from any interpretation made by any of our officers, agents or employees. These interpretations are also subject to our general terms and conditions set out in our current Price Schedule. All interpretations a interpretation, an

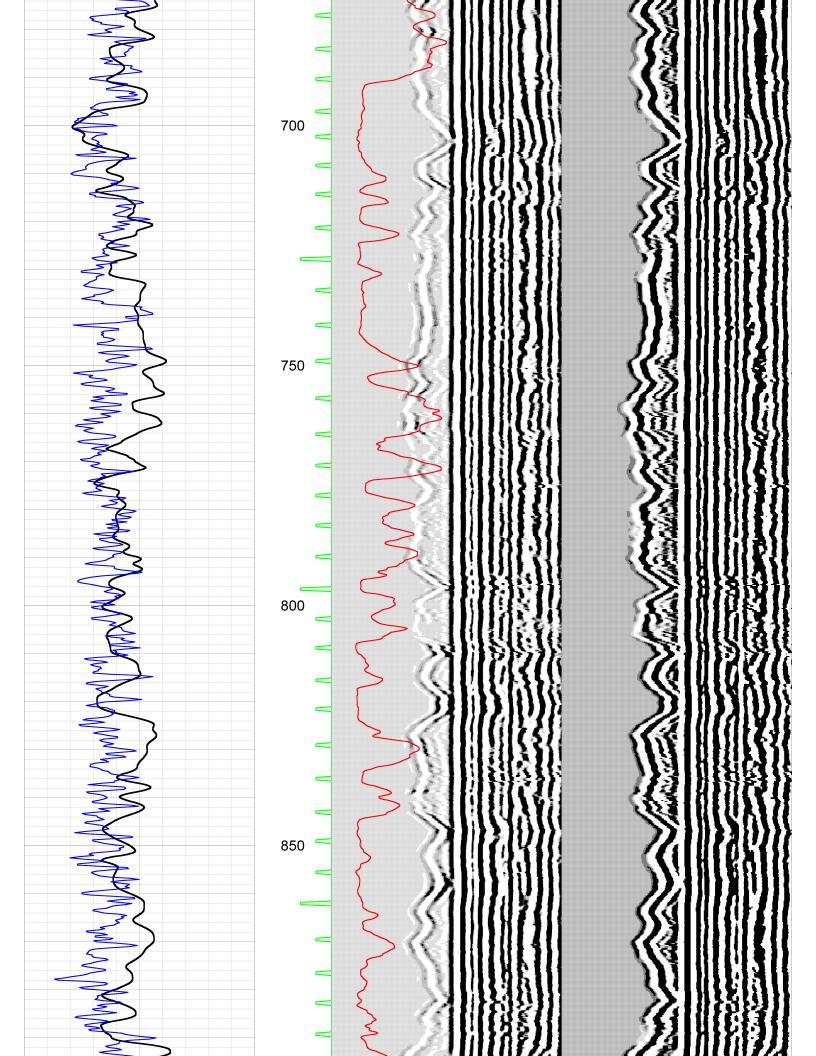
Comments

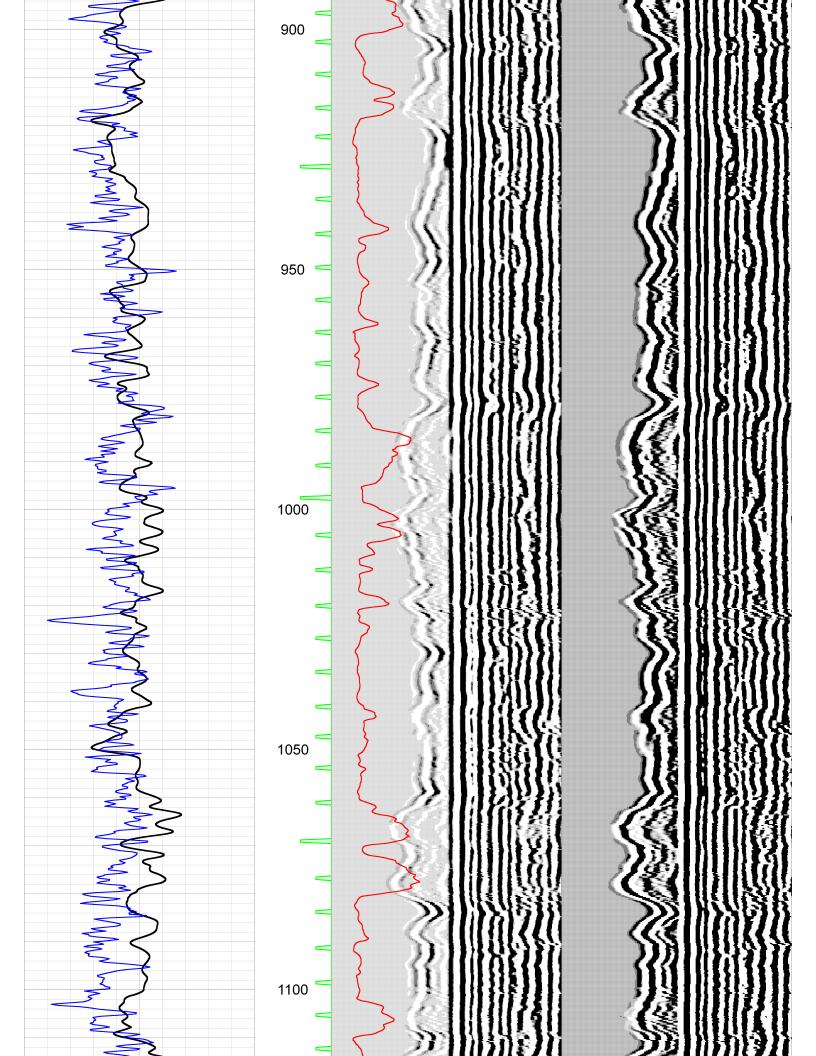
25150.db SONIC2 slt Thu Jan 17 16:43:12 2019 Depth in Feet scaled 1:240 Presentation Format Database File Dataset Pathname Dataset Creation Charted by

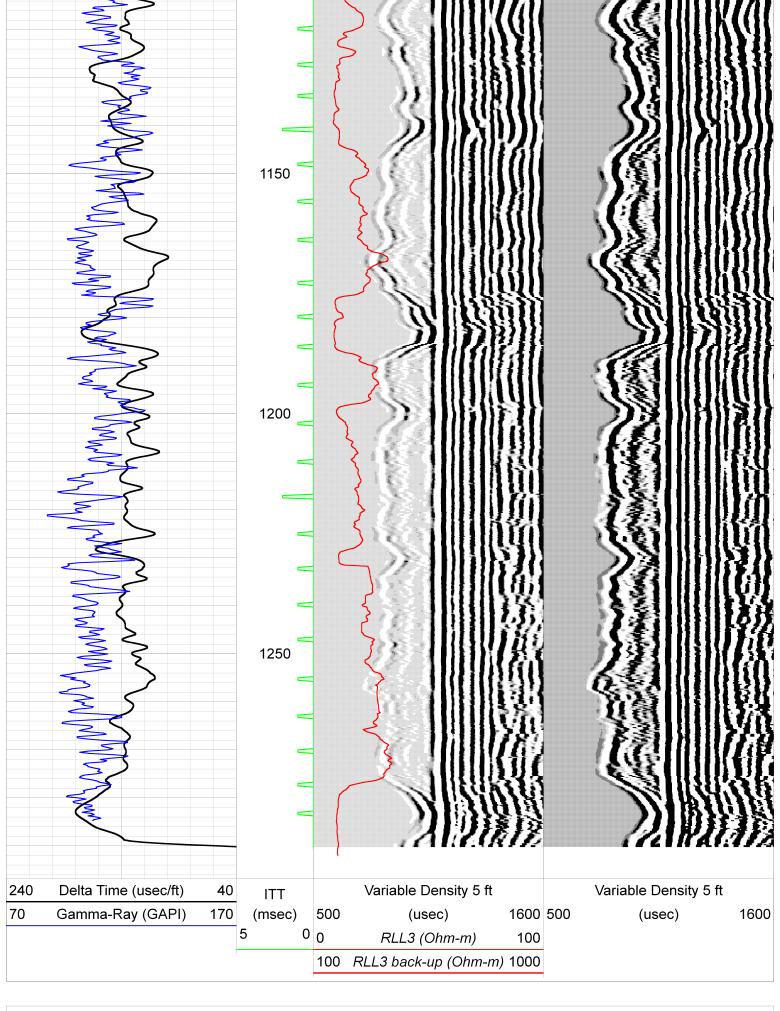












### Top - Bottom

BHTEMP_Src	BOREID in	BOTTEMP degF	CASEOD in	CASETHCK in	COMPACT	FloatGate
TEMP	17.5	79.3	5.5	0	1	0
PERFS	RM_MEAS_R Ohm-m	RM_MEAS_T degF	RMF Ohm-m	RSH Ohm-m	SPSHIFT mV	SRFTEMP degF
0	6.2	71.2	5.96	20	7	63.5
SVFLUID usec/ft 189	SVMATRIX usec/ft 47.6	TDEPTH ft 1295	TempGrad DegF/ft 0.01235			

# Inclinometer Calibration Report



### **TEMPERATURE DIFFERENTIAL TEMP**

Job No. **CASCADE DRILLING** Company 25150

> Well **IEUA PX2**

**POMONA** Field File No.

LOS ANGELES State CA County

Other Services: Location:

WEST SIDE OF MONTVUE PARK: 1634 CORDOVA ST GPS: 34.0747462 -117.214596

LL3 SONIC DEVIATION **CALIPER** 

ELOG

Sec. Twp. Rge. G.L. Elevation Permanent Datum Elevation Log Measured From G.L. 0' above perm. datum K.B.

Drilling Measured From G.L.	U	above perm. datam	D.F. G.L.
•	04.47.0040	T	G.L.
Date	01-17-2019		
Run Number	ONE		
Depth Driller	1295'		
Depth Logger	1290.8'		
Bottom Logged Interval	1290.8'		
Top Log Interval	0'		
Casing Driller	20" @ 50'		
Casing Logger	50'		
Bit Size	17.5"		
Type Fluid in Hole	BENTONITE		
Density / Viscosity	9.2 / 37		
pH / Fluid Loss	/ 7		
Source of Sample	MUD TANK		
Rm @ Meas. Temp	6.2 @ 71.2 F		
Rmf @ Meas. Temp	5.96 @ 71.2 F		
Rmc @ Meas. Temp	N/A		
Source of Rmf / Rmc	MEASURED		
Rm @ BHT	N/A		
Time Circulation Stopped	0745		
Time Logger on Bottom	1515		
Max. Recorded Temperature	72.69 F		
Equipment Number	PS-5		
Location	VENTURA		
Recorded By	CALEB VILLALOBOS		
Witnessed By	ROBERT THACKER		

or correctness of All interpretations are opinions based on inferences from electrical or other measurements and we cannot and do not guarantee the accuracy or correctness o any interpretation, and we shall not, except in the case of gross or willful negligence on our part, be liable or responsible for any loss, costs, damages, or expenses incurred or sustained by anyone resulting from any interpretation made by any of our officers, agents or employees. These interpretations are also subject to our general terms and conditions set out in our current Price Schedule.

<<< Fold Here >>>

Comments

Calibration Report

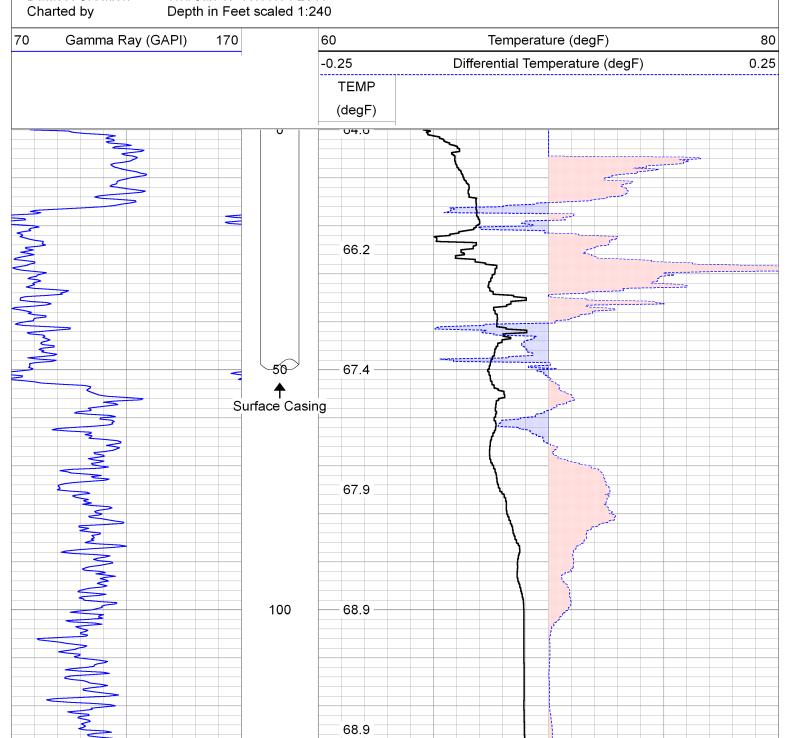
25150.db TEMP

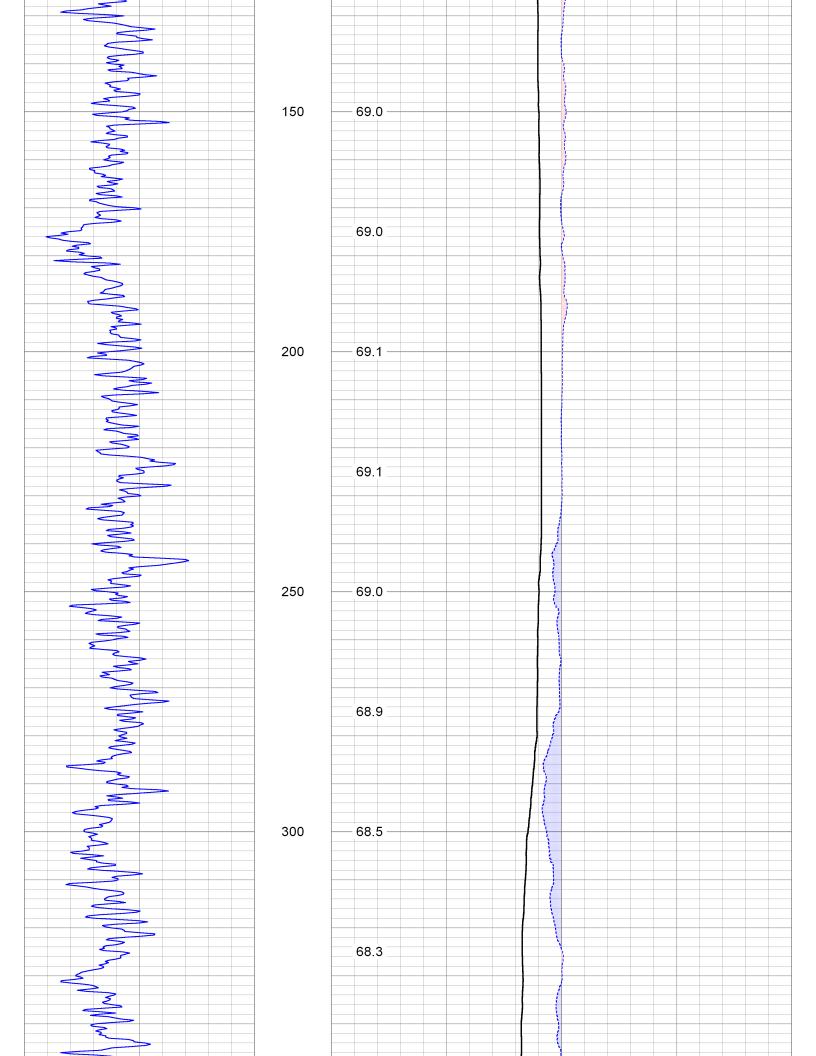
Thu Jan 17 15:39:54 2019 Dataset Pathname Dataset Creation Database File

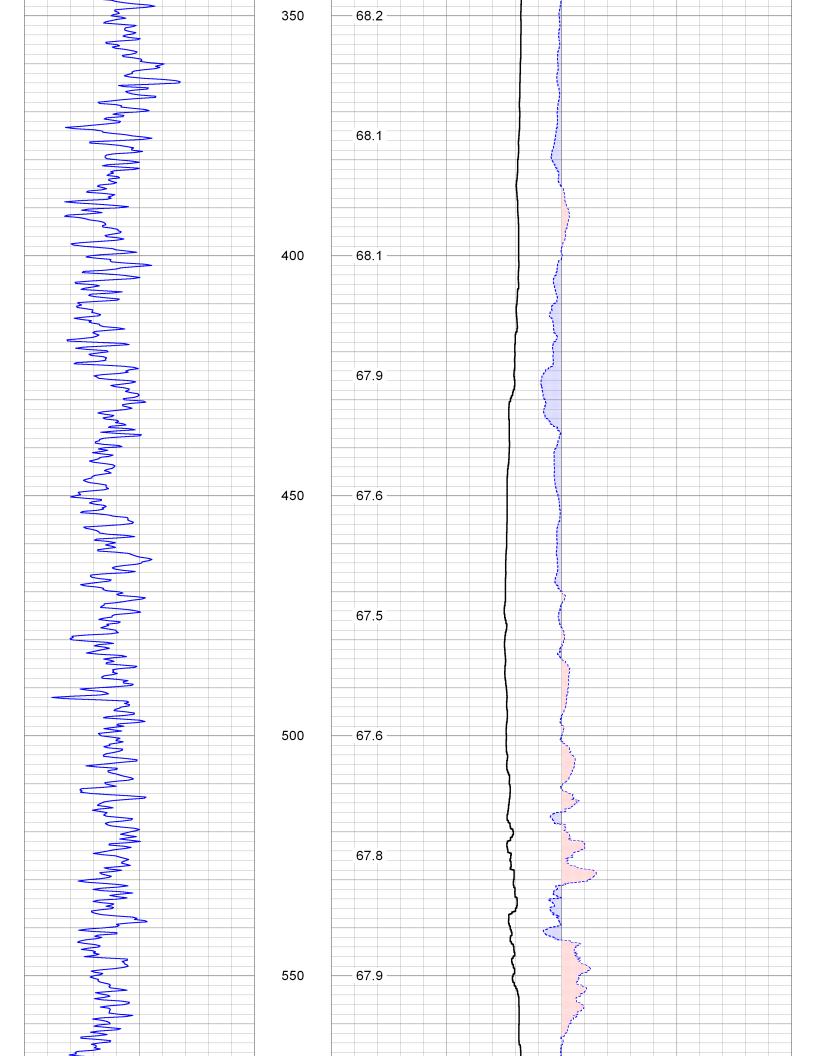
Performed:	Tue Oct 08	14:21:34 20	13			
	Low Read.	High Read.		Low Ref.	High Ref.	
X Accelerometer	-90.00	90.00	deg	-1.00	1.00	gee
Y Accelerometer	-90.00	90.00	deg	-1.00	1.00	gee
Z Accelerometer			deg			gee

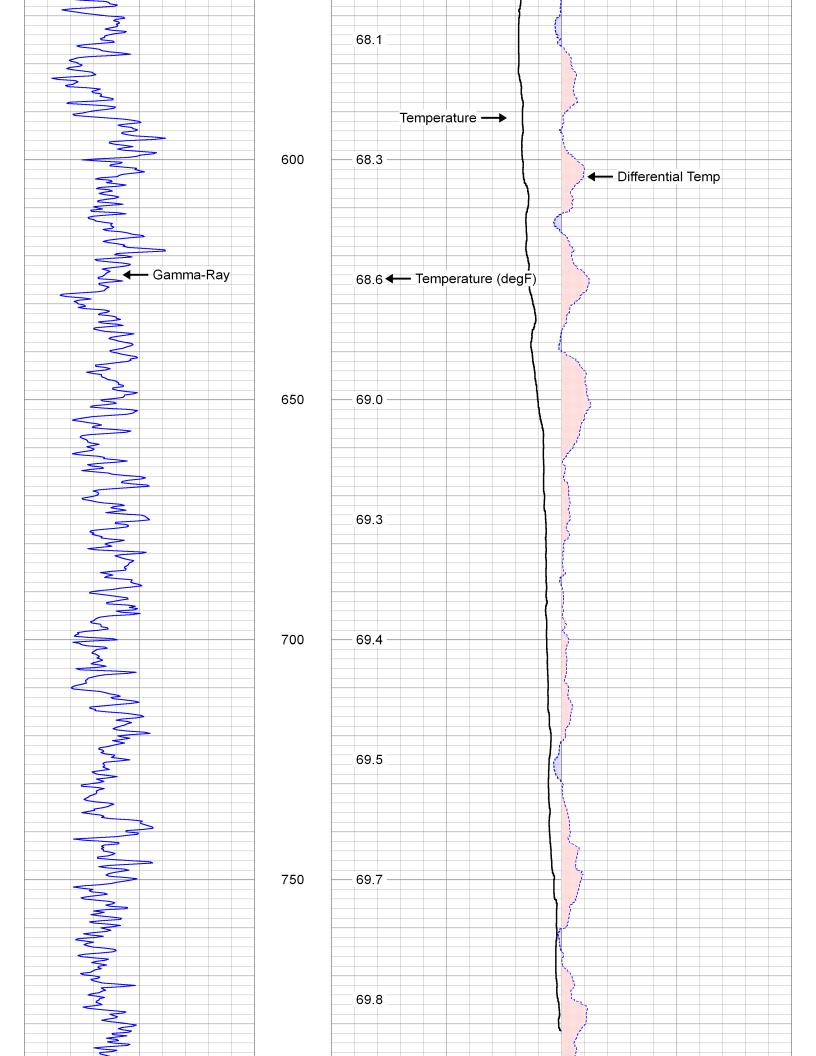


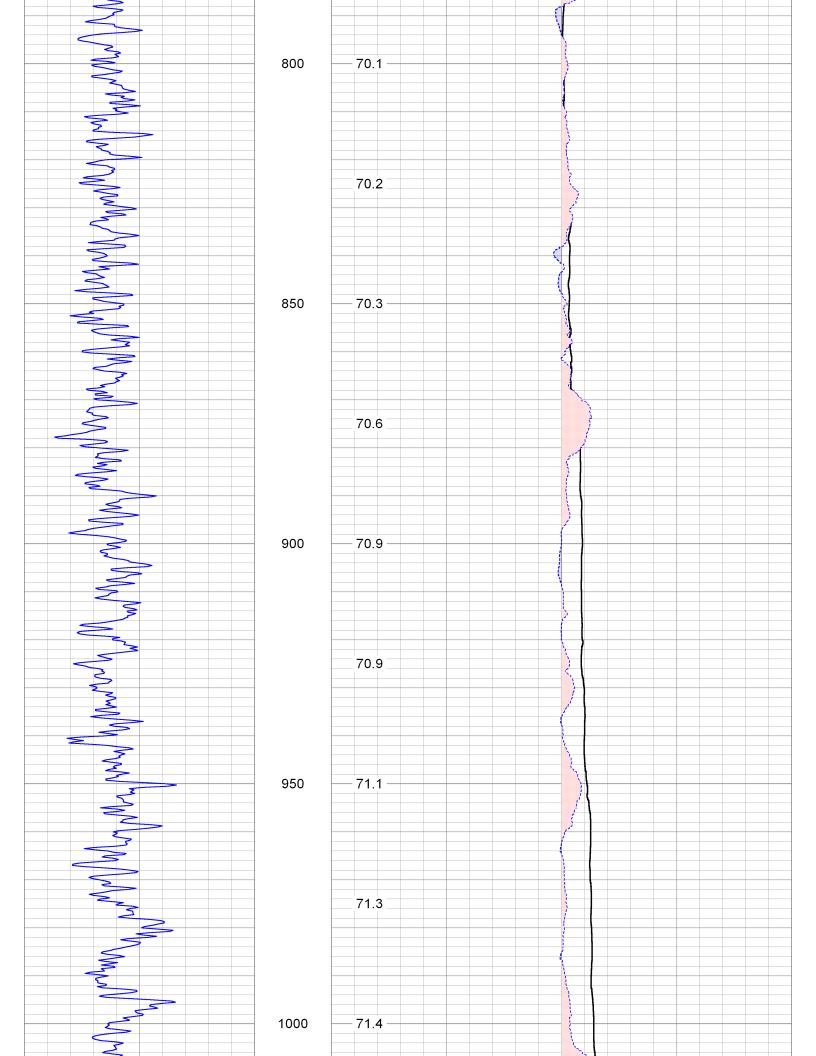
**Dataset Creation** Thu Jan 17 15:39:54 2019

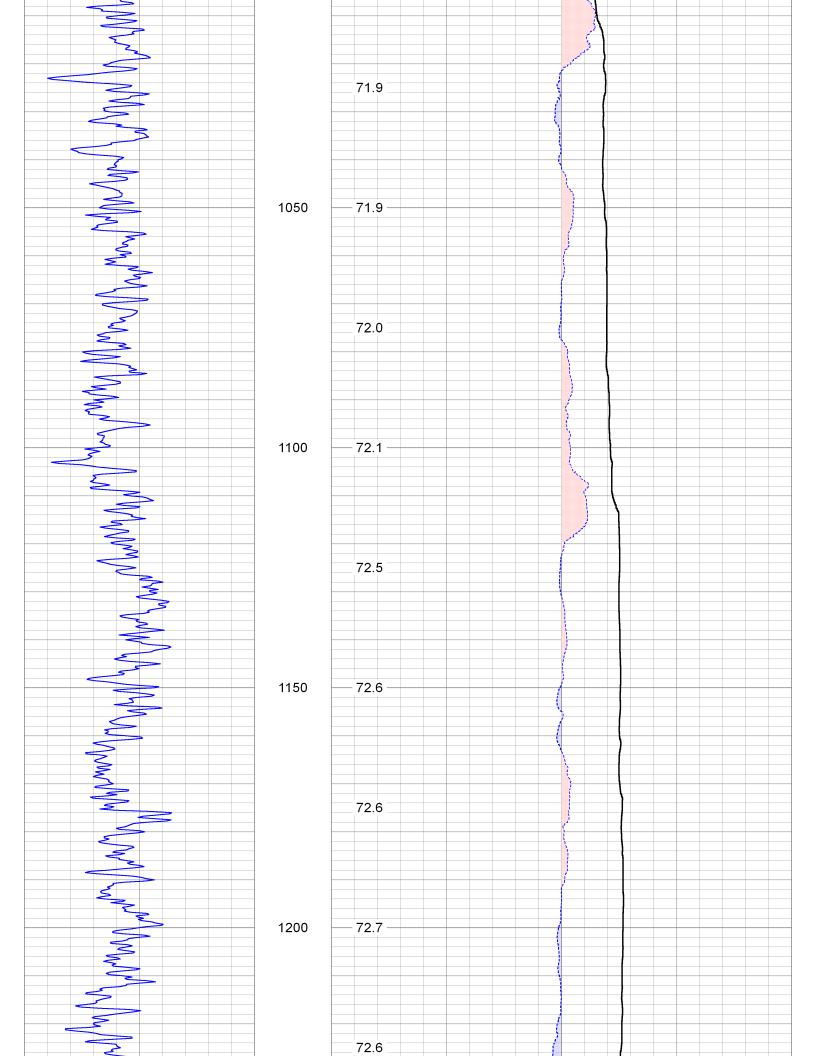


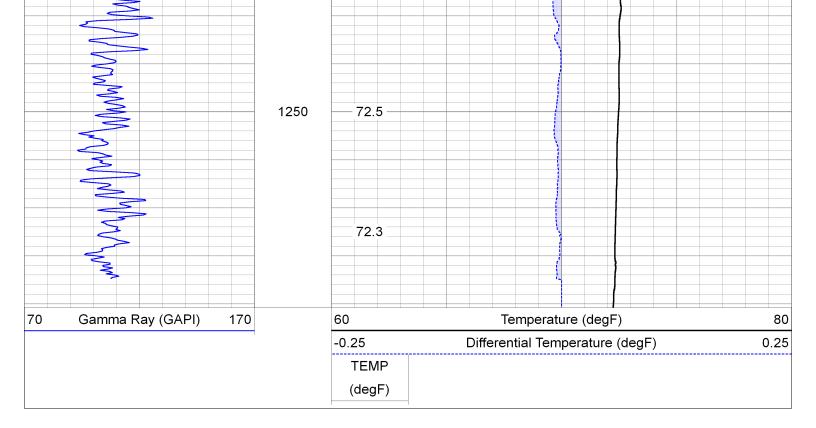












## Log Variables DatabaseC:\ProgramData\Warrior\Data\25150.db Dataset field/well/run1/TEMP/\_vars\_

### Top - Bottom

BHTEMP_Src TEMP	BOREID in 17.5	BOTTEMP degF 79.3	CASEOD in 5.5	CASETHCK in 0	PERFS 0	RM_MEAS_R Ohm-m 6.2
RM_MEAS_T	RMF	RSH	SPSHIFT	SRFTEMP	TDEPTH	TempGrad
degF	Ohm-m	Ohm-m	mV	degF	ft	DegF/ft
71.2	5.96	20	7	63.5	1295	0.01235

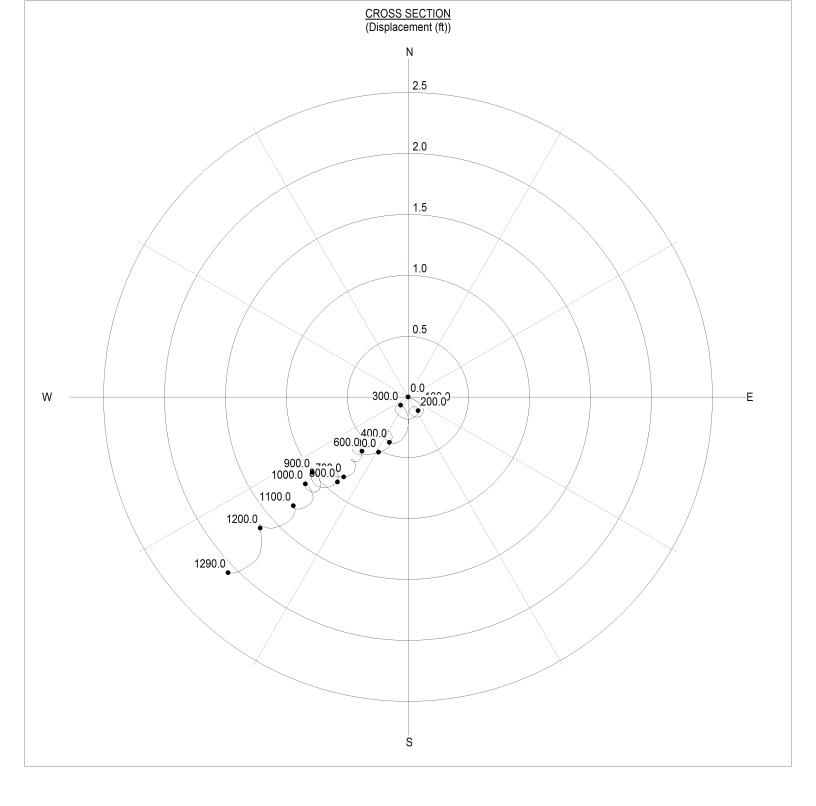


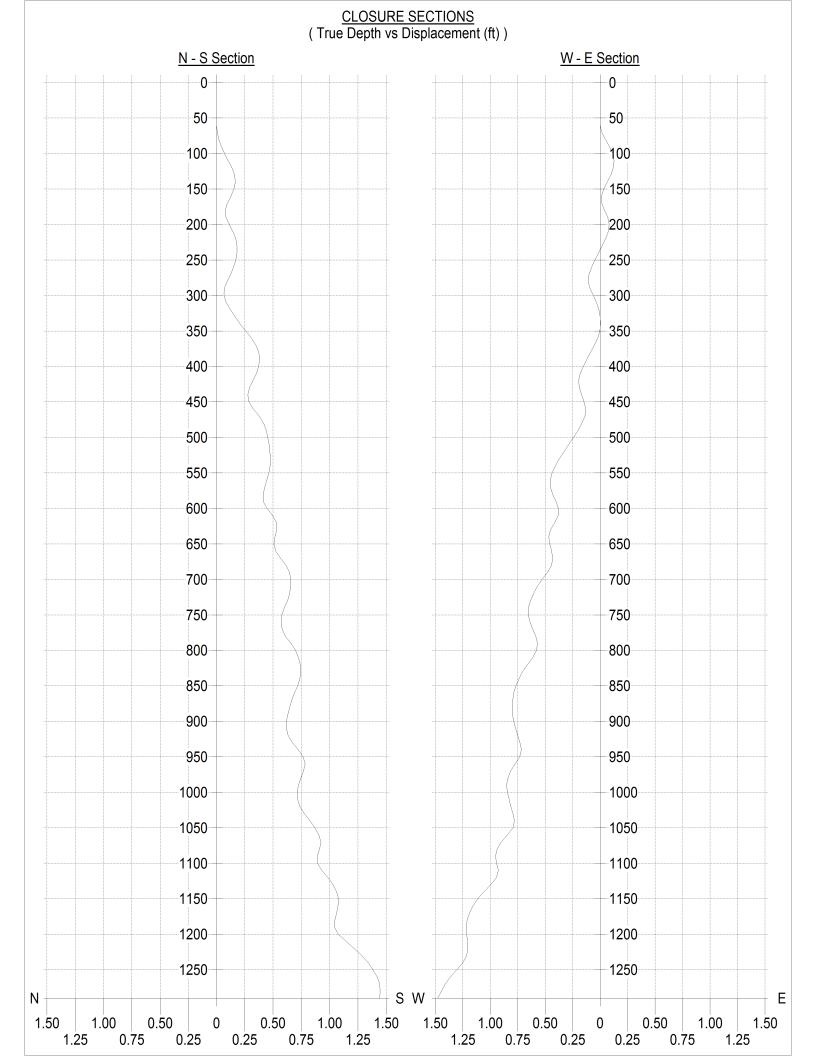
### **DEVIATION SURVEY**

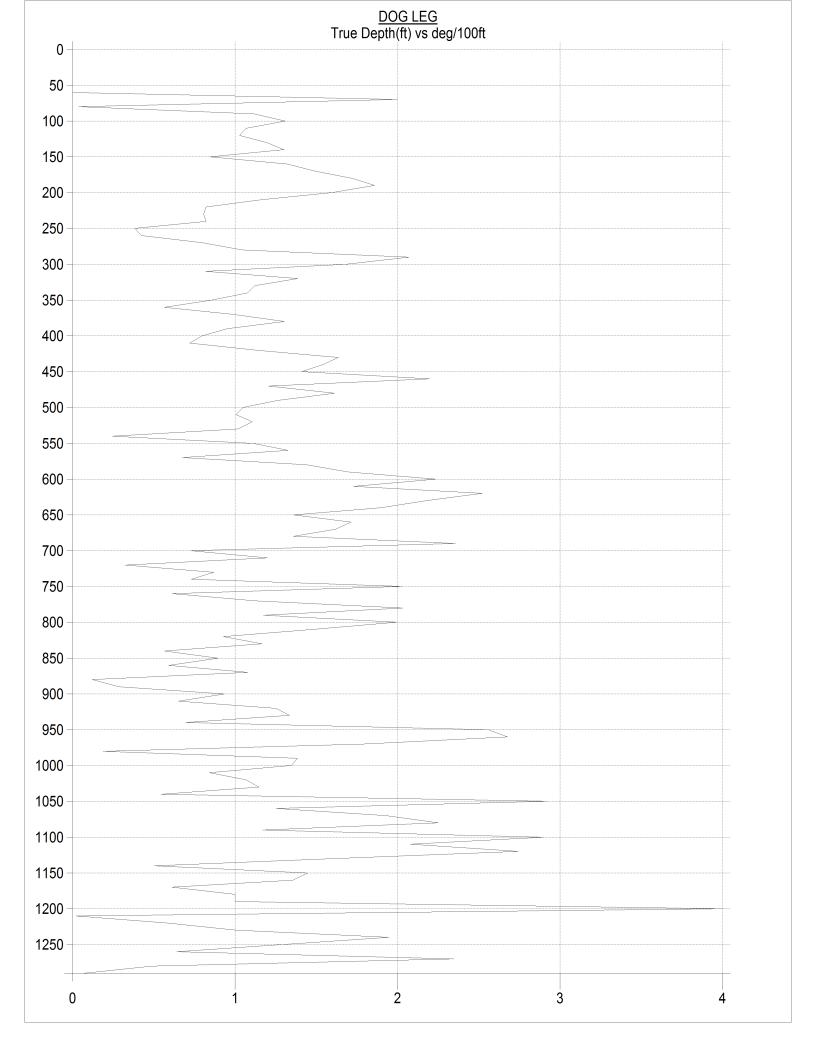
Job No.						$\dashv$
25150	Company	CASCADE DRILL	_ING			
	Well	IEUA PX2				
	vveii	IEUA PAZ				
File No.	Field	POMONA				
THE NO.	County	LOS ANGELES	State	CA		
Location:	1			Other Ser	vices:	
GPS: 34.07474	62 -117.214596	RK: 1634 CORDOVA ST		ELOG LL3 SONIC TMP	CALIPER	
Sec.	Twp.	Rge.			Florestion	_
Permanent Datu	• • • • • • • • • • • • • • • • • • • •		Elevation	. 4	Elevation	
Log Measured F			above perm. da	atum	K.B. D.F. G.L.	
Drilling Measure	ed From G.			I	G.L.	4
Date		01-17-2019				4
Run Number		ONE				$\dashv$
Depth Driller		1295'				-
Depth Logger	Intonual	1295' 1295.6'				$\dashv$
Bottom Logged Top Log Interva		0'				$\dashv$
Casing Driller	11	20" @ 50'				$\dashv$
Casing Driller Casing Logger		50'				$\dashv$
Bit Size		17.5"				$\dashv$
Type Fluid in He	ole	BENTONITE				$\dashv$
Density / Viscos		9.2 / 37				$\dashv$
pH / Fluid Loss		/ 7				$\dashv$
Source of Samp	ole	MUD TANK				┪
Rm @ Meas. T		6.2 @ 71.2 F				$\exists$
Rmf @ Meas. T		5.96 @ 71.2 F				7
Rmc @ Meas.	<u> </u>	N/A				1
Source of Rmf	/ Rmc	MEASURED				7
Rm @ BHT		N/A				1
Time Circulation		0745				
Time Logger on		1230				
Max. Recorded	<u> </u>	72.69 F				
Equipment Num	nber	PS-5				
Location		VENTURA				
Recorded By		CALEB VILLALOBOS				
Witnessed By		ROBERT THACKER				

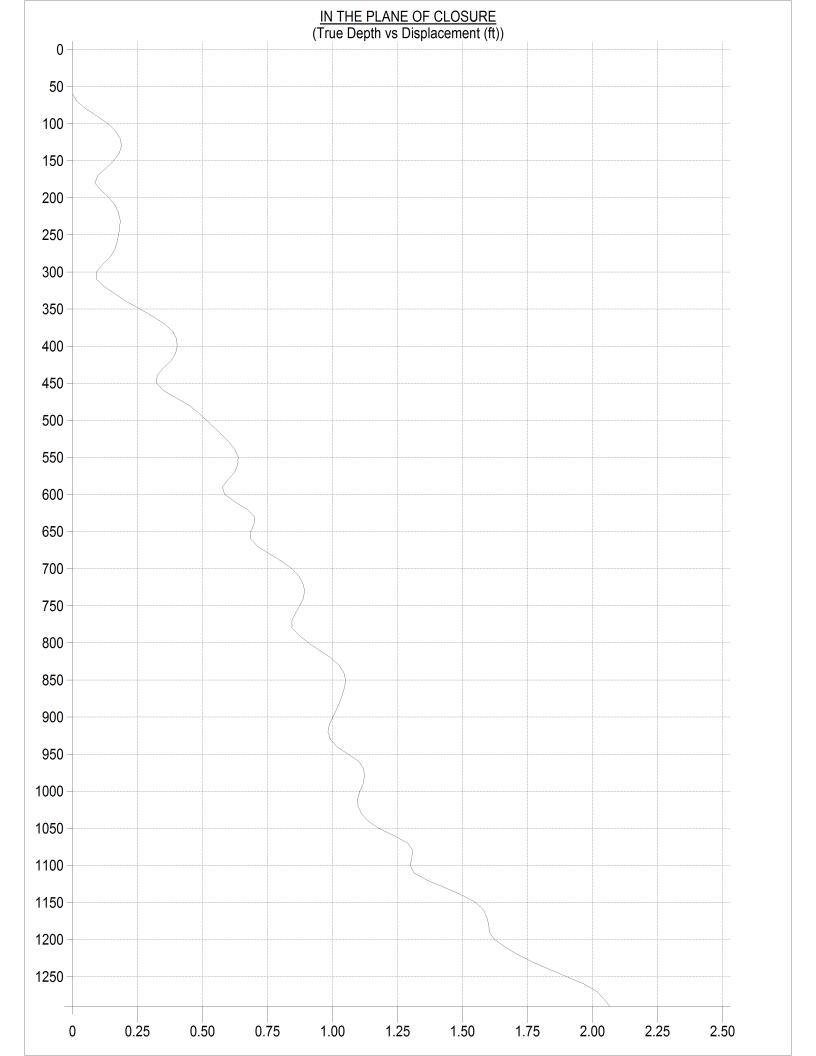
All interpretations are opinions based on inferences from electrical or other measurements and we cannot and do not guarantee the accuracy or correctness of any interpretation, and we shall not, except in the case of gross or willful negligence on our part, be liable or responsible for any loss, costs, damages, or expenses incurred or sustained by anyone resulting from any interpretation made by any of our officers, agents or employees. These interpretations are also subject to our general terms and conditions set our tin our current Price Schedule.

Comments









### TVD Report (Minimum Curvature Method)

Database File 25150.db
Dataset Pathname ./././\_tvd\_\_/1

510.0

520.0

530.0 540.0 0.20

0.30

0.20

0.20

253.00

264.10

268.50

275.50

510.00

520.00

530.00

540.00

Dataset Creation Thu Jan 17 14:58:05 2019

Meas. Depth	Incline	Azimuth	TVD	North	East	Dog Leg	Closure Dis	Closure Dir	Vert. Sec.
(ft)	(deg)	(deg)	(ft)	(ft)	(ft)	(deg/100ft)	(ft)	(deg)	(ft)
		Vertical Sect							
0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10.0	0.00	67.60	10.00	0.00	0.00	0.00	0.00	0.00	0.00
20.0	0.00	179.00	20.00	0.00	0.00	0.00	0.00	0.00	0.00
30.0	0.00	228.50	30.00	0.00	0.00	0.00	0.00	0.00	0.00
40.0	0.00	224.20	40.00	0.00	0.00	0.00	0.00	0.00	0.00
50.0	0.00	279.80	50.00	0.00	0.00	0.00	0.00	0.00	0.00
60.0	0.00	90.40	60.00	0.00	0.00	0.00	0.00	0.00	0.00
70.0	0.20	112.50	70.00	-0.01	0.02	2.00	0.02	-67.50	-0.01
80.0	0.20	113.60	80.00	-0.02	0.05	0.04	0.05	-67.13	-0.02
90.0	0.30	125.30	90.00	-0.04	0.09	1.12	0.10	-63.62	-0.04
100.0	0.20	145.20	100.00	-0.07	0.12	1.31	0.14	-58.41	-0.07
110.0	0.20	176.20	110.00	-0.10	0.13	1.07	0.16	-51.01	-0.10
120.0	0.20	206.00	120.00	-0.14	0.12	1.03	0.18	-41.63	-0.14
130.0	0.20	240.70	130.00	-0.16	0.10	1.19	0.19	-31.51	-0.16
140.0	0.20	278.70	140.00	-0.17	0.07	1.30	0.18	-21.64	-0.17
150.0	0.20	303.10	150.00	-0.15	0.03	0.85	0.16	-12.51	-0.15
160.0	0.20	341.70	160.00	-0.13	0.01	1.32	0.13	-6.31	-0.13
170.0	0.20	25.60	170.00	-0.10	0.02	1.50	0.10	-9.60	-0.10
180.0	0.20	76.70	180.00	-0.08	0.04	1.73	0.09	-28.07	-0.08
190.0	0.20	132.10	190.00	-0.08	0.07	1.86	0.11	-40.03	-0.08
200.0	0.20	179.20	200.00	-0.11	0.08	1.60	0.14	-36.51	-0.11
210.0	0.20	212.90	210.00	-0.15	0.07	1.16	0.16	-27.18	-0.15
220.0	0.20	236.60	220.00	-0.17	0.05	0.82	0.18	-16.62	-0.17
230.0	0.20	259.90	230.00	-0.18	0.02	0.81	0.18	-5.92	-0.18
240.0	0.20	283.60	240.00	-0.18	-0.02	0.82	0.18	4.80	-0.18
250.0	0.20	294.60	250.00	-0.17	-0.05	0.38	0.18	15.79	-0.17
260.0	0.20	306.80	260.00	-0.15	-0.08	0.43	0.17	27.09	-0.15
270.0	0.20	329.90	270.00	-0.13	-0.10	0.80	0.16	38.45	-0.13
280.0	0.20	0.20	280.00	-0.09	-0.11	1.05	0.14	49.25	-0.09
290.0	0.20	62.60	290.00	-0.07	-0.09	2.07	0.12	53.77	-0.07
300.0	0.20	112.20	300.00	-0.07	-0.06	1.68	0.09	42.72	-0.07
310.0	0.20	135.80	310.00	-0.09	-0.03	0.82	0.09	21.37	-0.09
320.0	0.30	158.40	320.00	-0.12	-0.01	1.39	0.12	5.56	-0.12
330.0	0.20	170.30	330.00	-0.16	0.00	1.12	0.16	-0.20	-0.16
340.0	0.30	179.70	340.00	-0.21	0.00	1.08	0.21	-1.01	-0.21
350.0	0.30	196.10	350.00	-0.26	-0.00	0.86	0.26	0.76	-0.26
360.0	0.30	206.90	360.00	-0.31	-0.02	0.56	0.31	4.19	-0.31
370.0	0.30	225.80	370.00	-0.35	-0.05	0.99	0.35	8.65	-0.35
380.0	0.20	245.50	380.00	-0.38	-0.09	1.30	0.39	13.18	-0.38
390.0	0.20	273.10	390.00	-0.38	-0.12	0.95	0.40	17.62	-0.38
400.0	0.20	296.10	400.00	-0.37	-0.15	0.80	0.40	22.48	-0.37
410.0	0.20	316.90	410.00	-0.35	-0.18	0.72	0.40	27.30	-0.35
420.0	0.20	349.90	420.00	-0.32	-0.20	1.14	0.38	31.40	-0.32
430.0	0.20	38.20	430.00	-0.29	-0.19	1.64	0.35	32.97	-0.29
440.0	0.10	87.40	440.00	-0.28	-0.17	1.54	0.33	31.44	-0.28
450.0	0.20	128.50	450.00	-0.29	-0.15	1.41	0.32	27.08	-0.29
460.0	0.30	175.60	460.00	-0.32	-0.13	2.20	0.35	22.04	-0.32
470.0	0.30	198.80	470.00	-0.38	-0.14	1.21	0.40	20.16	-0.38
480.0	0.30	230.00	480.00	-0.42	-0.17	1.61	0.45	21.75	-0.42
490.0	0.20	248.10	490.00	-0.44	-0.20	1.26	0.49	24.70	-0.44
Meas. Depth	Incline	Azimuth	TVD	North	East	Dog Leg	Closure Dis	Closure Dir	Vert. Sec.
(ft)	(deg)	(deg)	(ft)	(ft)	(ft)	(deg/100ft)	(ft)	(deg)	(ft)
		Vertical Sect							
500.0	0.30	255.70	500.00	-0.45	-0.24	1.05	0.52	28.30	-0.45
E10 0	0.20	252.00	E10 00	0.47	0.20	1 01	0.55	21 61	0.47

-0.29

-0.33

-0.37

-0.41

1.01

1.11

1.02

0.24

0.55

0.58

0.60

0.63

31.61

34.83

38.04

40.62

-0.47

-0.47

-0.48

-0.47

-0.47

-0.47

-0.48

-0.47

550.0	0.20	307.80	550.00	-0.46	-0.44	1.11	0.64	43.47	-0.46
560.0	0.10	343.70	560.00	-0.44	-0.45	1.33	0.64	45.72	-0.44
570.0	0.10	23.20	570.00	-0.43	-0.45	0.68	0.62	46.74	-0.43
580.0	0.20	66.20	580.00	-0.41	-0.43	1.44	0.60	46.51	-0.41
590.0	0.20	116.40	590.00	-0.41	-0.40	1.70	0.58	44.30	-0.41
600.0	0.30	164.60	600.00	-0.45	-0.38	2.24	0.59	40.46	-0.45
610.0	0.30	198.10	610.00	-0.50	-0.38	1.73	0.63	37.56	-0.50
620.0	0.30	247.80	620.00	-0.53	-0.41	2.52	0.67	37.94	-0.53
630.0	0.20	294.50	630.00	-0.53	-0.45	2.18	0.70	40.40	-0.53
640.0	0.10	4.10	640.00	-0.52	-0.47	1.90	0.70	42.20	-0.52
650.0	0.10	89.80	650.00	-0.51	-0.46	1.36	0.69	42.11	-0.51
660.0	0.20	148.80	660.00	-0.52	-0.44	1.71	0.69	40.17	-0.52
670.0	0.30	178.90	670.00	-0.56	-0.43	1.62	0.71	37.45	-0.56
680.0	0.30	205.10	680.00	-0.61	-0.44	1.36	0.76	35.79	-0.61
690.0	0.30	251.40	690.00	-0.65	-0.48	2.36	0.80	36.53	-0.65
700.0	0.30	265.30	700.00	-0.66	-0.53	0.73	0.84	38.88	-0.66
710.0	0.20	280.90	710.00	-0.66	-0.57	1.20	0.87	41.15	-0.66
720.0	0.20	290.20	720.00	-0.65	-0.61	0.32	0.89	43.17	-0.65
730.0	0.20	315.30	730.00	-0.63	-0.64	0.87	0.89	45.32	-0.63
740.0	0.20	336.40	740.00	-0.60	-0.65	0.73	0.89	47.50	-0.60
750.0	0.10	53.80	750.00	-0.58	-0.65	2.03	0.87	48.52	-0.58
760.0	0.10	89.50	760.00	-0.57	-0.64	0.61	0.86	48.09	-0.57
770.0	0.20	110.50	769.99	-0.58	-0.61	1.13	0.84	46.64	-0.58
780.0	0.30	152.90	779.99	-0.61	-0.59	2.03	0.84	43.88	-0.61
790.0	0.30	175.50	789.99	-0.66	-0.57	1.18	0.87	40.96	-0.66
800.0	0.20	216.80	799.99	-0.70	-0.58	2.00	0.91	39.70	-0.70
810.0	0.30	242.50	809.99	-0.72	-0.61	1.48	0.95	40.26	-0.72
820.0	0.30	260.30	819.99	-0.74	-0.66	0.93	0.99	41.80	-0.74
830.0	0.20	274.40	829.99	-0.74	-0.71	1.17	1.03	43.49	-0.74
840.0	0.20	290.70	839.99	-0.74	-0.74	0.57	1.04	45.12	-0.74
850.0	0.20	316.60	849.99	-0.72	-0.77	0.90	1.05	46.93	-0.72
860.0	0.20	333.60	859.99	-0.69	-0.79	0.59	1.05	48.81	-0.69
870.0	0.10	350.20	869.99	-0.67	-0.80	1.08	1.04	50.15	-0.67
880.0	0.10	357.20	879.99	-0.65	-0.80	0.12	1.03	50.96	-0.65
890.0	0.10	13.60	889.99	-0.63	-0.80	0.29	1.02	51.65	-0.63
900.0	0.10	69.40 107.50	899.99	-0.62	-0.79	0.94	1.00	51.81 51.24	-0.62
910.0 920.0	0.10		909.99	-0.62	-0.77	0.65 1.25	0.99	51.24	-0.62
920.0	0.20 0.30	138.50 159.30	919.99 929.99	-0.63 -0.67	-0.75	1.25	0.98 0.99	49.80 47.36	-0.63 -0.67
940.0	0.30	172.60	939.99	-0.87 -0.72	-0.73 -0.72	0.69	1.02	47.36 44.79	-0.67
950.0	0.30	223.10	949.99	-0.72 -0.77	-0.72	2.56	1.02	43.63	-0.72
960.0	0.30	276.10	959.99	-0.77 -0.78	-0.73 -0.78	2.68	1.10	44.70	-0.77
970.0	0.30	311.10	969.99	-0.77	-0.76	1.78	1.12	46.64	-0.77
980.0	0.20	316.50	979.99	-0.75	-0.84	0.19	1.12	48.41	-0.75
990.0	0.10	356.10	989.99	-0.72	-0.85	1.38	1.12	49.66	-0.72
000.0	0.10			0.12		1.00	1.12		0.72
Meas. Depth	Incline	Azimuth	TVD	North	East	Dog Leg	Closure Dis	Closure Dir	Vert. Sec.
(ft)	(deg)	(deg)	(ft)	(ft)	(ft)	(deg/100ft)	(ft)	(deg)	(ft)
		Vertical Sect	ion Direction	0.00					
1000.0	0.10	80.80	999.99	-0.71	-0.84	1.35	1.11	49.79	-0.71
1010.0	0.10	130.60	1009.99	-0.72	-0.83	0.84	1.10	49.11	-0.72
1020.0	0.20	145.90	1019.99	-0.74	-0.81	1.07	1.10	47.75	-0.74
1030.0	0.30	159.10	1029.99	-0.78	-0.79	1.15	1.11	45.60	-0.78
1040.0	0.30	169.50	1039.99	-0.83	-0.78	0.54	1.14	43.30	-0.83
1050.0	0.30	227.90	1049.99	-0.87	-0.79	2.93	1.18	42.37	-0.87
1060.0	0.40	240.40	1059.99	-0.91	-0.84	1.25	1.24	42.99	-0.91
1070.0	0.30	268.00	1069.99	-0.92	-0.90	1.93	1.29	44.27	-0.92
1080.0	0.20	316.60	1079.99	-0.91	-0.94	2.25	1.31	45.83	-0.91
1090.0	0.10	341.50	1089.99	-0.89	-0.95	1.17	1.30	46.94	-0.89

1100.0

1110.0

1120.0

1130.0

1140.0

1150.0

1160.0

1170.0

1180.0

0.20

0.30

0.40

0.40

0.40

0.30

0.20

0.20

0.10

129.60

173.30

216.60

239.80

247.00

264.40

285.90

303.50

303.30

1099.99

1109.99

1119.99

1129.99

1139.99

1149.99

1159.99

1169.99

1179.99

-0.89

-0.93

-0.98

-1.03

-1.06

-1.08

-1.08

-1.06

-1.05

-0.94

-0.93

-0.94

-0.99

-1.06

-1.12

-1.16

-1.19

-1.21

2.90

2.08

2.74

1.61

0.50

1.45

1.35

0.61

1.00

1.30

1.31

1.36

1.43

1.50

1.55

1.58

1.59

1.60

46.53

44.86

43.78

44.00

44.88

45.98

47.12

48.27

49.17

-0.89

-0.93

-0.98

-1.03

-1.06

-1.08

-1.08

-1.06

-1.05

1190.0	0.00	55.50	1189.99	-1.04	-1.22	1.00	1.60	49.47	-1.04
1200.0	0.40	173.70	1199.99	-1.08	-1.21	4.00	1.62	48.45	-1.08
1210.0	0.40	173.40	1209.99	-1.15	-1.21	0.02	1.66	46.49	-1.15
1220.0	0.40	181.90	1219.99	-1.22	-1.20	0.59	1.71	44.73	-1.22
1230.0	0.40	196.30	1229.99	-1.28	-1.22	1.00	1.77	43.42	-1.28
1240.0	0.40	224.50	1239.99	-1.34	-1.25	1.95	1.83	42.95	-1.34
1250.0	0.40	243.10	1249.99	-1.38	-1.30	1.29	1.90	43.34	-1.38
1260.0	0.40	233.90	1259.99	-1.42	-1.36	0.64	1.97	43.87	-1.42
1270.0	0.20	259.00	1269.99	-1.44	-1.41	2.35	2.02	44.32	-1.44
1280.0	0.20	273.10	1279.99	-1.45	-1.44	0.49	2.04	44.97	-1.45
1290.0	0.20	275.00	1289.99	-1.44	-1.48	0.07	2.07	45.70	-1.44

# Caliper Calibration Report

# PACIFIC SURVEYS

File No.

Sec.

### CALIPER BOREHOLE VOLUME

Job No.
25150 Company CASCADE DRILLING
Well IEUA PX2

Field POMONA

Twp.

County LOS ANGELES State CA

Location: Other Services:

WEST SIDE OF MONTVUE PARK: 1634 CORDOVA ST
GPS: 34.0747462 -117.214596

ELOG/GR
SONIC

Rge.

TMP DEVIATION

Permanent Datum G.L. Elevation Elevation
Log Measured From G.L. 0' above perm. datum
Drilling Measured From G.L.

Elevation
K.B.
D.F.
G.I.

209 1110404110111	·	 D F	
Drilling Measured From G	.L.	 D.F. G.L.	
Date	01-17-2019		
Run Number	ONE		
Depth Driller	1295'		
Depth Logger	1296.1'		
Bottom Logged Interval	1296.1'		
Top Log Interval	0'		
Casing Driller	20" @ 50'		
Casing Logger	50'		
Bit Size	17.5"		
Type Fluid in Hole	BENTONITE		
Density / Viscosity	9.2 / 37		
pH / Fluid Loss	/ 7		
Source of Sample	MUD TANK		
Rm @ Meas. Temp	6.2 @ 71.2 F		
Rmf @ Meas. Temp	5.96 @ 71.2 F		
Rmc @ Meas. Temp	N/A		
Source of Rmf / Rmc	MEASURED		
Rm @ BHT	N/A		
Time Circulation Stopped	0745		^
Time Logger on Bottom	1415		^ و
Max. Recorded Temperature	72.69 F		1 1
Equipment Number	PS-5		Д С
Location	VENTURA		F
Recorded By	CALEB VILLALOBOS		\v
Witnessed By	ROBERT THACKER		

or correctness of All interpretations are opinions based on inferences from electrical or other measurements and we cannot and do not guarantee the accuracy or correctness o any interpretation, and we shall not, except in the case of gross or willful negligence on our part, be liable or responsible for any loss, costs, damages, or expenses incurred or sustained by anyone resulting from any interpretation made by any of our officers, agents or employees. These interpretations are also subject to our general terms and conditions set out in our current Price Schedule.

Comments

Calibration Report

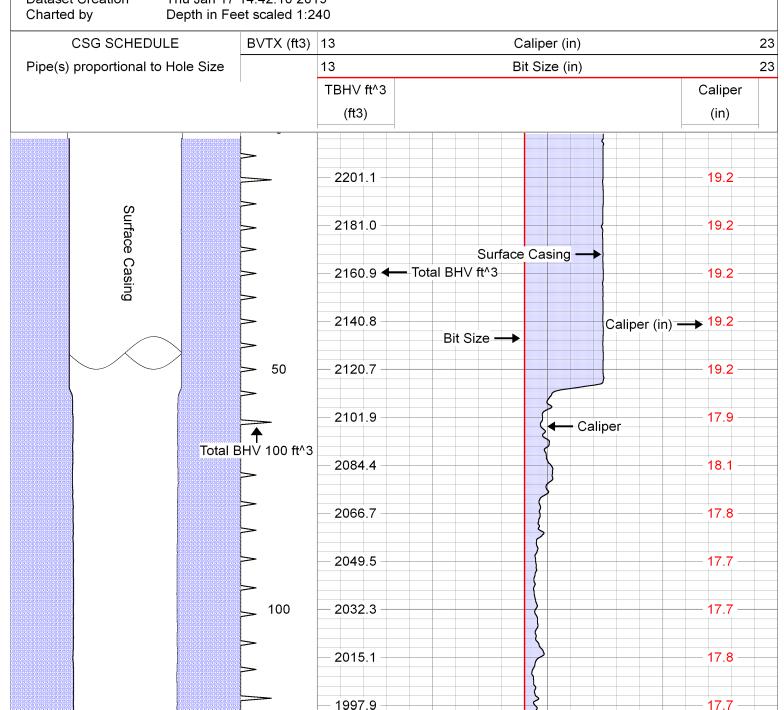
25150.db me CALIPER n Thu Jan 17 14:42:10 2019

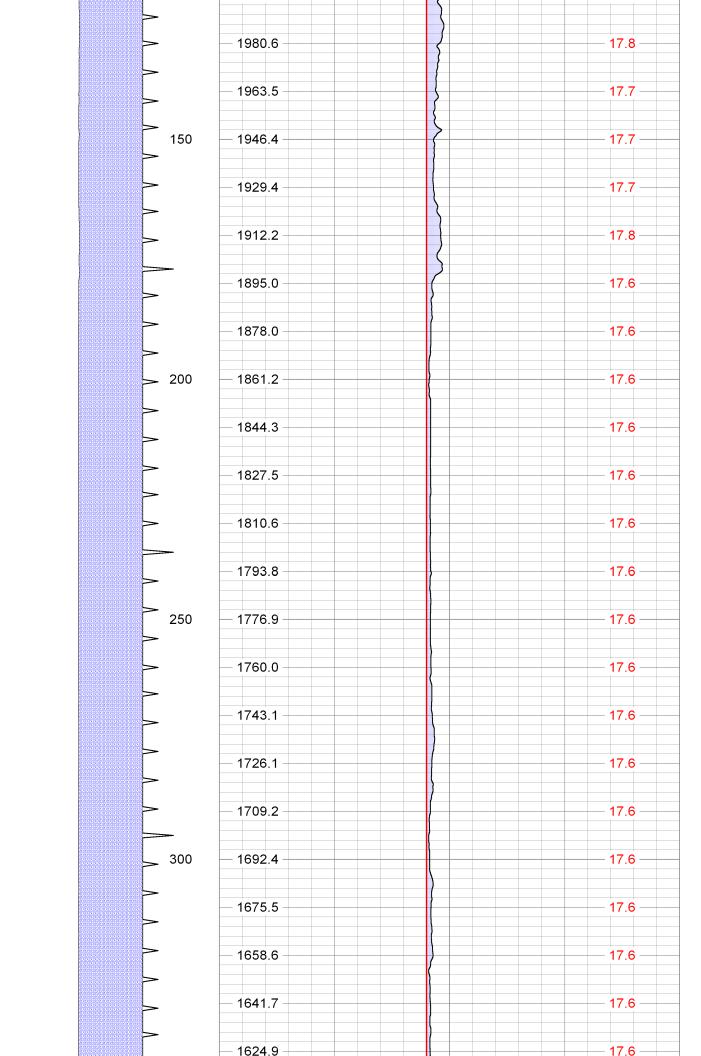
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Dataset Pathname CALIPER
Dataset Creation Thu Jan

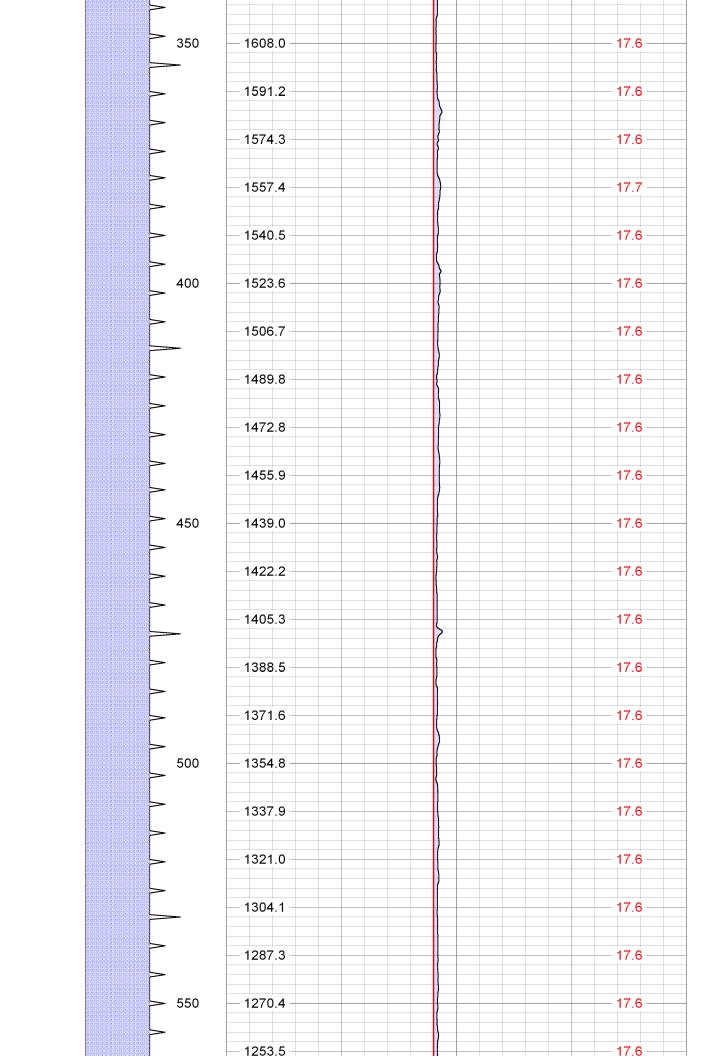
Serial Perfo	Number rmed:	/Model:	CAL-10_MEDIUI Wed Jan 24 09:3		3	
	Ring		X Caliper		Y Caliper	
1:	2.1	in	635.979	cps	635.979	cps
2:	8	in	1178.22	cps	1178.22	cps
3:	14	in	1593.37	cps	1593.37	cps
4:	20	in	1985.65	cps	1985.65	cps
5:	26	in	2350.5	cps	2350.5	cps
6:	32	in	2768.67	cps	2768.67	cps
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8:		in		cps		cps
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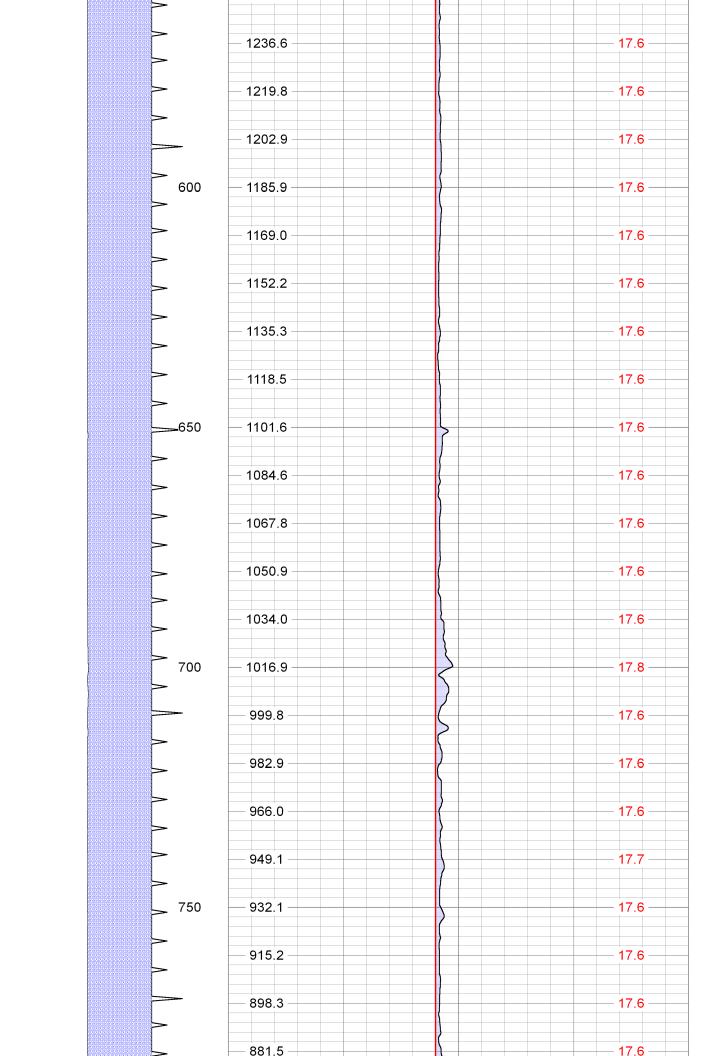
Database File 25150.db **Dataset Pathname CALIPER** Presentation Format xyc\_gph\_final

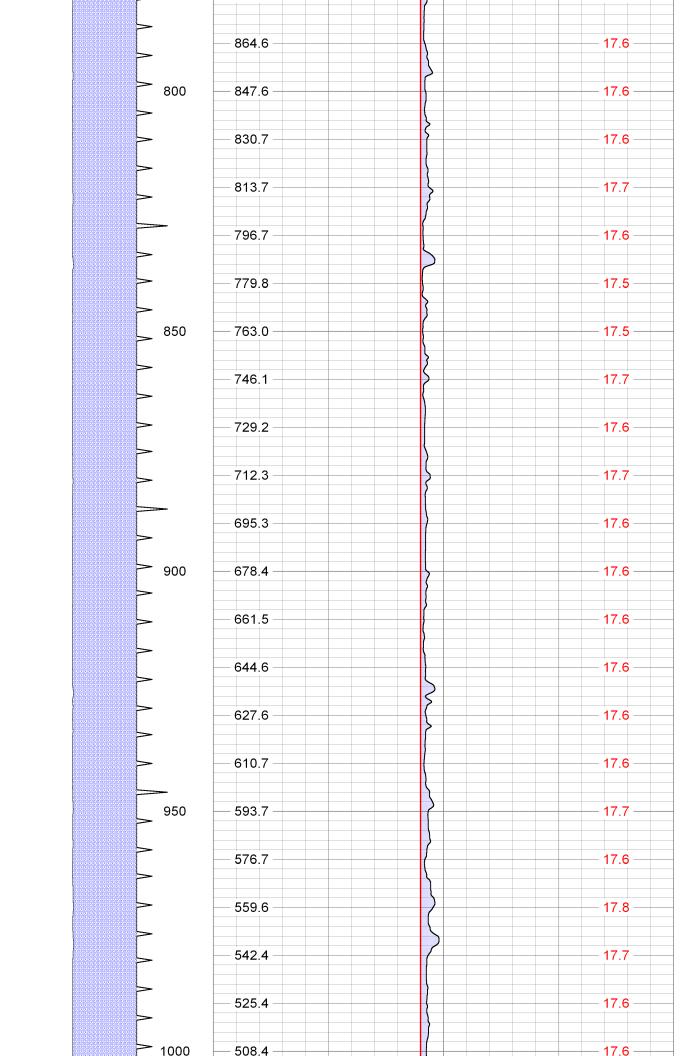
Thu Jan 17 14:42:10 2019 **Dataset Creation** 

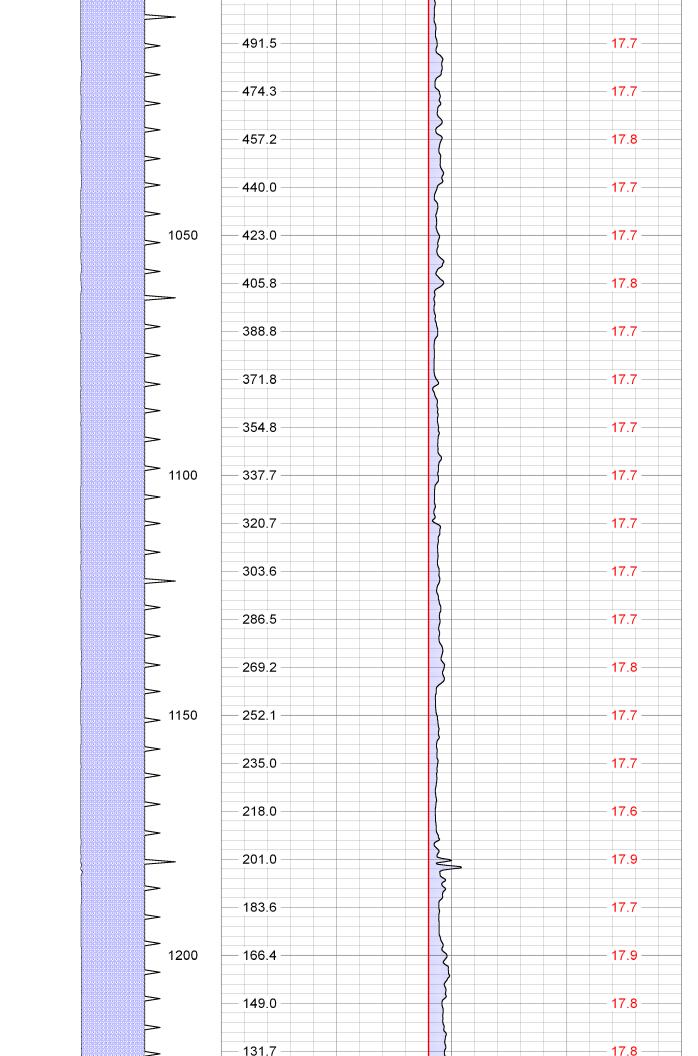


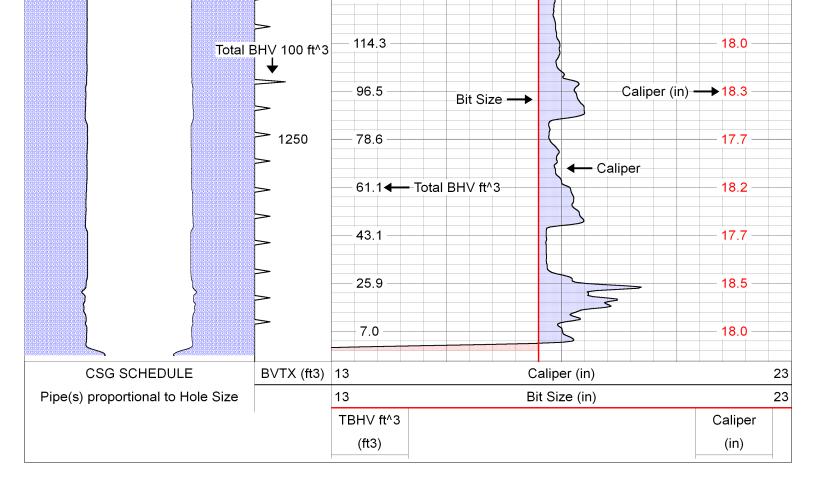




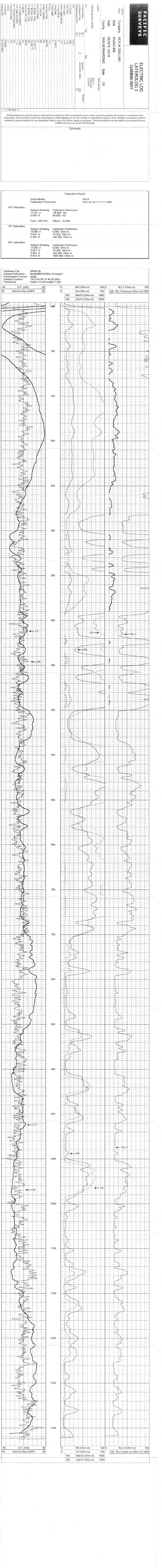








### Log Variables DatabaseC:\ProgramData\Warrior\Data\25150.db Dataset field/well/run1/CALIPER/\_vars\_ **Top - Bottom** CASEOD CASETHCK RM\_MEAS\_T **BOREID BOTTEMP PERFS** RM\_MEAS\_R in degF in in Ohm-m degF 5.5 0 17.5 79.3 0 6.2 71.2 **RMF** RSH **SPSHIFT SRFTEMP** TDEPTH TempGrad Ohm-m Ohm-m mV degF ft DegF/ft 5.96 20 7 63.5 1295 0.01235



# Appendix B

## Response to GLMC Comments



# State of California Department/John Wood Group PLC (Richard Rees, PG, CHG)

### **Comment 1 – Global Comment**

We make the following comment on behalf of the State of California/California Department of Corrections and Rehabilitation, a member of the Agricultural Pool. We agree that the one-dimensional models appear to be sufficiently calibrated to use for estimation of potential future subsidence at the locations they represent, subject to the limitations identified in the technical memorandum.

B-1

### **Response:**

Thank you for your comment.



### City of Chino/Geopentech (Eric Fordham, PG, CEG, CHG)

### Comment 1 - Background and Objectives

The first paragraph should identify that in addition to ground fissuring as the primary threat to infrastructure, permanent ground subsidence can also change hydraulic grade in gravity flow systems such as storm drains and sewers and differential subsidence over short distances could also pose significant threats to rigid infrastructure.

### Response:

Thank you for your comments and suggestions. The text was updated, where appropriate, to address this comment.

### **Comment 2 – Boundary Conditions**

The last sentence of page 8 should read "...deeper pumping caused head declines in the deeper confined CVM layers, which in turn resulted in *upward* vertical hydraulic gradients." *Upward* should be *downward* vertical hydraulic gradients.

### Response:

Thank you for your comment and suggestions. The text was updated, where appropriate, to address this comment.

### **Comment 3 – Global Comment**

We concur that the 1D compaction models that have been developed for this study are sufficiently calibrated to provide a useful tool for evaluating potential future subsidence under the Baseline Management Alternative.

### Response:

Thank you for your comment.



### Monte Vista Water District/Geoscience (Christofer Coppinger, PG, CHG)

### Comment 1 - Calibration of the 1D Models

Can a figure showing residual and calibration statistics for water levels at the wells be included? Or some brief discussion of the residual and calibration statistics compared to adjusted heads from the CVM? Something to document that the sensitivity run included conditions outside the observed data.

### Response:

Excerpts from the 2020 Safe Yield Recalculation Final Report<sup>1</sup> are attached to Appendix B and document the calibration statistics and the residuals for the heads in the Chino Valley Model (CVM):

Figure 6-6. Location of Calibration Wells

Figure 6-7a. Comparison of Simulated and Measured Water Levels in the Wells of Chino Basin

Figure 6-9. Residual Relative Frequency Histogram in Chino Basin

Figure 6-11. Mean Residual Error of Calibration Wells

Figure 6-6 shows the location of all the wells used in the model calibration and Figure 6-7a plots the simulated vs measured heads for the calibration wells plotted in Figure 6-6. The coefficient of determination R2 is 0.932 and the points are distributed closely around the diagonal line, indicating "good inverse modeling performance and a robust calibration" (WEI, 2020). As shown in Figure 6-9, the mean of the hydraulic head residuals is around 0.06, which is near zero, with a standard deviation of about 21 feet. Figure 6-11 shows the spatial distribution of average residuals for each calibration well and shows that there was no spatial bias by the CVM in estimating heads in the Chino Basin.

Given the results from the calibration and residual analysis, the heads simulated by the CVM were assigned to the Sand cells in the 1D Models. During the sensitivity analysis of the 1D Models, the heads in Layers 1 and 5 were adjusted from 1978-2018 to better match recent heads measured at the PX1-1 piezometer (Layer 1) in 2020 and at the PX2-3 piezometer (Layer 5) in 2020. Historical measured heads at several wells located in the vicinity of the 1D Models were also used to adjust heads in the model layers.

### Comment 2 - Appendix A

Can geologist's lithlogs be included as attachment?

### **Response:**

The PX2 and MVWD-28 borehole lithologic and geophysical logs are provided in Appendix A.

<sup>&</sup>lt;sup>1</sup> Wildermuth Environmental Inc. (2020). *2020 Safe Yield Recalculation Final Report*. Prepared for Chino Basin Watermaster.



### **Appendix B**

### **Response to GLMC Comments**



### Comment 3 – Figures 13 and 14

There was some discussion of the Compaction and Critical head columns during one of the meetings last year – I think Eric was explaining the critical head in upper vs lower systems. If any of that was captured, it would be a great addition to the figure.

### Response:

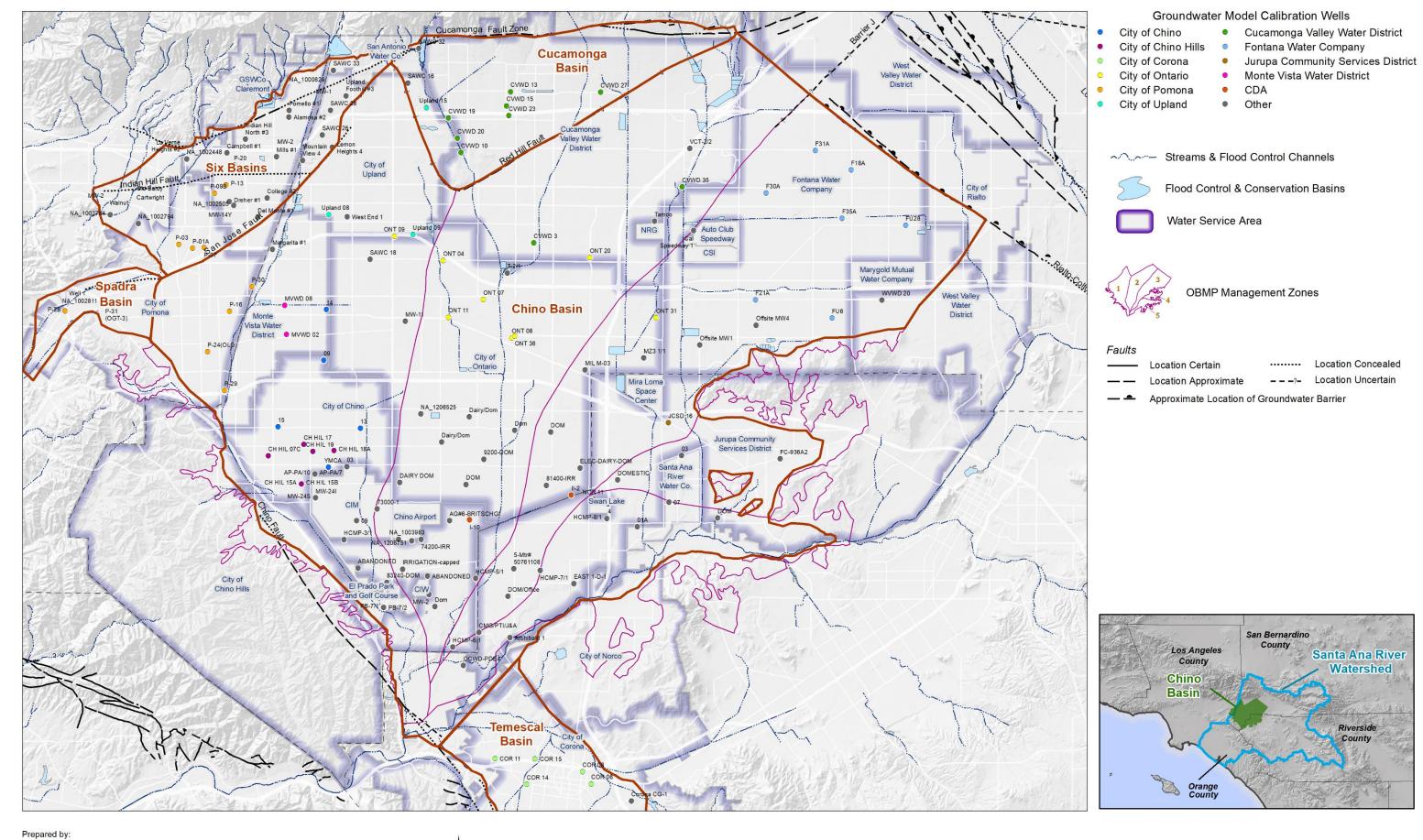
We are uncertain of the exact discussion that this comment is referring. Compaction and critical head are inversely related. In Layer 1, compaction has been relatively great in the Clay layers and hence, critical head is relatively low. In Layers 2, 3, 4, and 5, compaction has been relatively minor in the Clay layers (particularly the thick clay layers) and hence, critical head is relatively high. This model result indicates that the greatest potential for future compaction is within the thick Clay layers in Layers 2, 3, 4, and 5.

### Comment 4 – Global Comment

Overall – the 1D sensitivity run results are very interesting – maybe the sensitivity to the clay layers explains the subsidence at whispering lakes away from the pumping center.

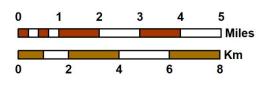
### Response:

The Whispering Lake Subsidence Feature is located somewhat distant from Northwest MZ1. These 1D Model results in Northwest MZ1 should not be interpreted to represent the aquifer system processes underlying the Whispering Lake Subsidence Feature.



WILDERMUTH ENVIRONMENTALING.

Author: LS Date: 4/1/2020 File: Figure 6-6 Calibration Wells.mxd



2020 Safe Yield Recalculation

Location of Calibration Wells Chino Valley Model

Figure 6-7a Comparison of Simulated and Measured Water Levels in the Wells of Chino Basin

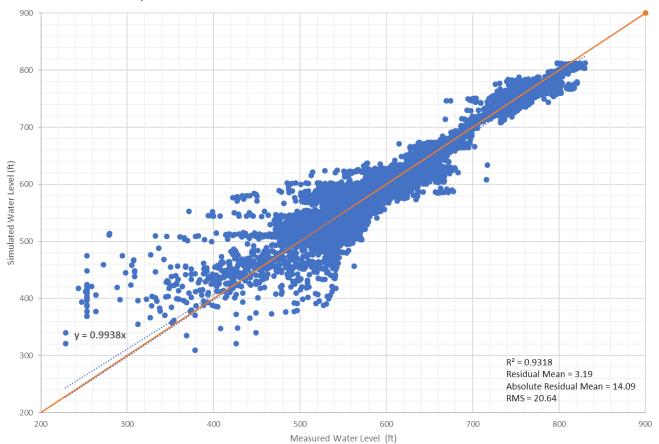


Figure 6-7c
Comparison of Simulated and Measured Water Levels in the Wells of Six Basin

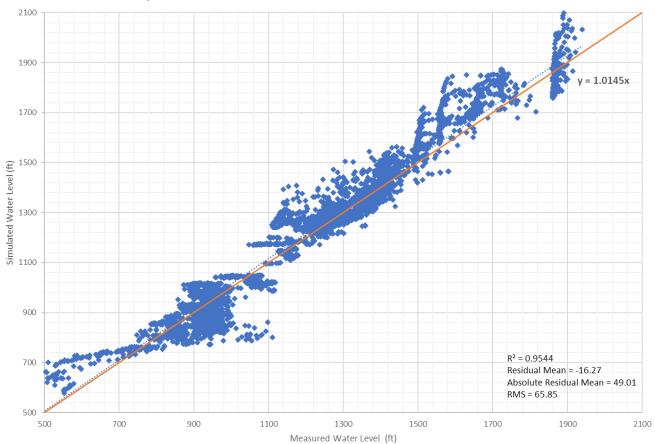


Figure 6-7b Comparison of Simulated and Measured Water Levels in the Wells of Cucamonga Basin

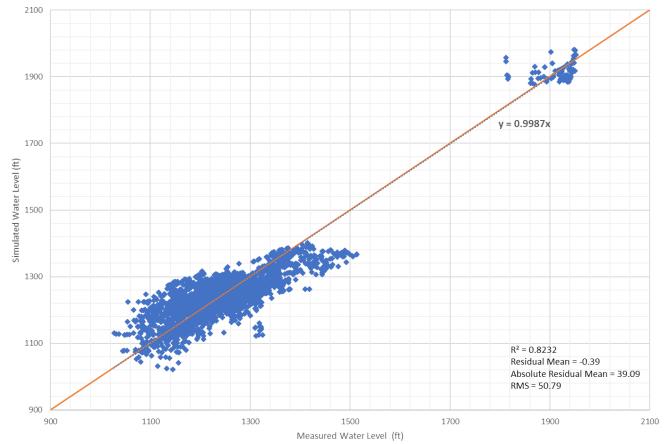


Figure 6-7d Comparison of Simulated and Measured Water Levels in the Selected Chino Hills Wells with the other Wells of Chino Basin

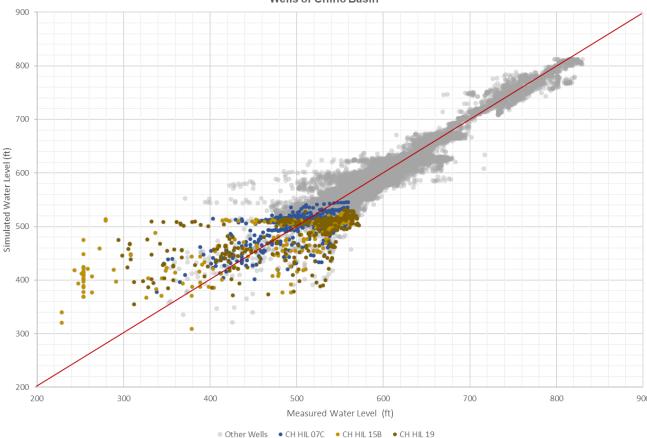
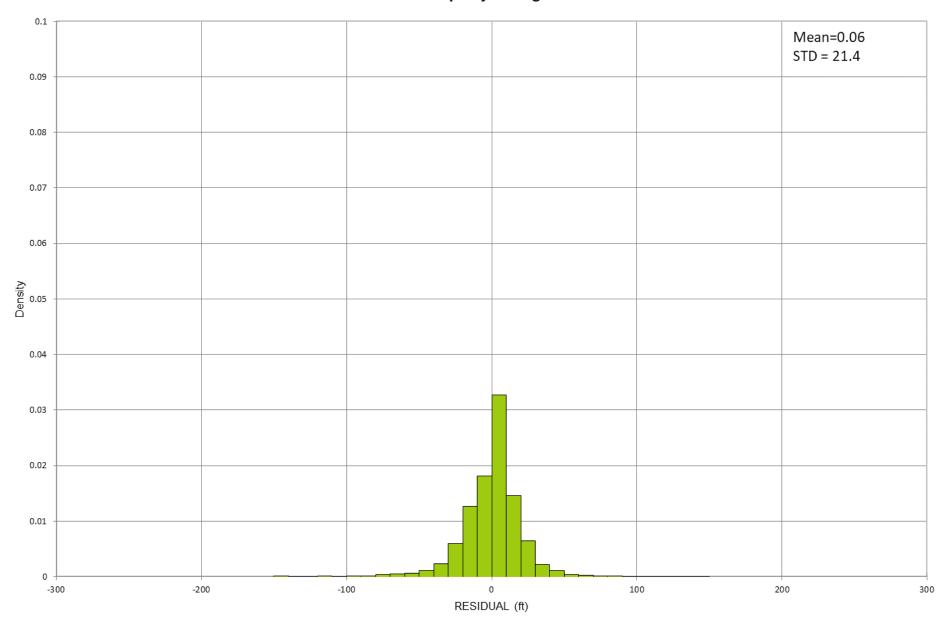
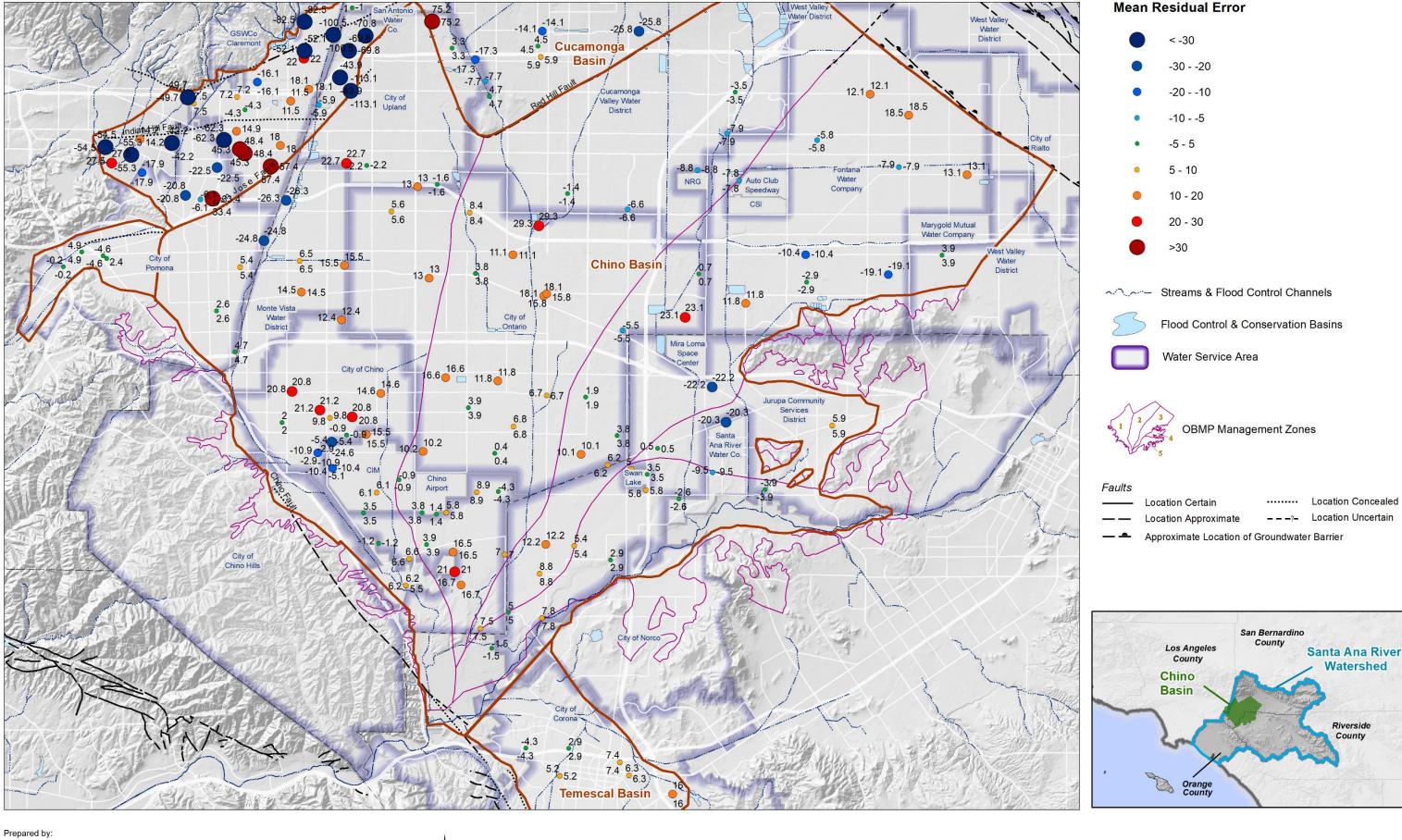




Figure 6-9 Residual Relative Freqency Histogram in Chino Basin

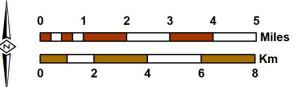






WEI WEI

Author: LS
Date: 5/11/2020
File: Figure 6-11 Mean Residual.mxd



Prepared for:
2020 Safe Yield Recalculation



Mean Residual Error of Calibration Wells